# Phase diagram of the two-fluid Lipkin model: A "butterfly" catastrophe 

J. E. García-Ramos, ${ }^{1}$ P. Pérez-Fernández, ${ }^{2}$ J. M. Arias, ${ }^{3}$ and E. Freire ${ }^{4}$<br>${ }^{1}$ Departamento de Física Aplicada, Universidad de Huelva, 21071 Huelva, Spain<br>${ }^{2}$ Departamento de Física Aplicada III, Escuela Técnica Superior de Ingeniería, Universidad de Sevilla, Sevilla, Spain<br>${ }^{3}$ Departamento de Física Atómica, Molecular y Nuclear, Facultad de Física, Universidad de Sevilla, Apartado 1065, 41080 Sevilla, Spain<br>${ }^{4}$ Departamento de Matemática Aplicada II, Escuela Técnica Superior de Ingeniería, Universidad de Sevilla, Sevilla, Spain

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#### Abstract

Background: In the past few decades quantum phase transitions have been of great interest in nuclear physics. In this context, two-fluid algebraic models are ideal systems to study how the concept of quantum phase transition evolves when moving into more complex systems, but the number of publications along this line has been scarce up to now. Purpose: We intend to determine the phase diagram of a two-fluid Lipkin model that resembles the nuclear protonneutron interacting boson model Hamiltonian using both numerical results and analytic tools, i.e., catastrophe theory, and compare the mean-field results with exact diagonalizations for large systems. Method: The mean-field energy surface of a consistent- $Q$-like two-fluid Lipkin Hamiltonian is studied and compared with exact results coming from a direct diagonalization. The mean-field results are analyzed using the framework of catastrophe theory. Results: The phase diagram of the model is obtained and the order of the different phase-transition lines and surfaces is determined using a catastrophe theory analysis. Conclusions: There are two first-order surfaces in the phase diagram, one separating the spherical and the deformed shapes, while the other separates two different deformed phases. A second-order line, where the later surfaces merge, is found. This line finishes in a transition point with a divergence in the second-order derivative of the energy that corresponds to a tricritical point in the language of the Ginzburg-Landau theory for phase transitions.


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## I. INTRODUCTION

The study of quantum phase transitions (QPTs) is a hot topic in different areas of quantum many-body physics. In nuclear physics many aspects of QPTs have been studied [1-3], both theoretically and experimentally. Also, in other fields such as molecular physics [4,5], quantum optics [6,7], or solid-state physics [8] studies related to relevant QPTs have been recently presented.

QPTs are phase transitions analogous to the classical ones but occurring at zero temperature. QPTs appear when the Hamiltonian has two (or more) parts with different structures (symmetries) and there is one (or several) control parameter that drives the system from one structure to the other. The phase transition is characterized by an abrupt change in an observable (called order parameter) that is zero in one phase and different from zero in the other. The value of the control parameter for which the structural change appears is known as critical value. Schematically, a Hamiltonian undergoing a QPT is written as

$$
\begin{equation*}
H(\xi)=\xi H\left(\text { symmetry }_{1}\right)+(1-\xi) H\left(\text { symmetry }_{2}\right) \tag{1}
\end{equation*}
$$

For a particular value of the control parameter, $\xi_{c}$, which is the critical value, the system undergoes a structural QPT from symmetry 1 to symmetry 2 .

One interesting extension of the QPT concept appears when treating with composed systems, as in the case of lattice systems [9]. The simplest case is a quantum two-fluid system in which there are two kind of particles (bosons in the case
presented here) with creation (and annihilation) operators that commute among them. Some pioneering studies on two-fluid systems [10-12] were carried out for the proton-neutron interacting boson model, IBM-2, and the authors managed to construct the phase diagram for a restricted Hamiltonian and classified the different phase transitions that the system undergoes. Other models that can be considered as two-fluid systems are the Dicke [13] and the Jaynes-Cumming [14] models for which the two fluids correspond to photons and atoms. Note that in this case the role of both fluids is not symmetric, photons fulfill a hw(1) (Heisenberg-Weyl) algebra while atoms are governed by a su(2) algebra. In the case of IBM-2, both fluids are connected with a $u(6)$ algebra.

The aim of this work is to study a simple two-fluid Lipkin model, which corresponds to a $\mathrm{su}(2) \otimes \operatorname{su}(2)$ algebra. One of the main motivations for carrying out this study is to treat with a model somehow similar to IBM-2 (except for the $\gamma$ degree of freedom) but simpler. In Refs. [10,11], when discussing QPTs in IBM-2, because of the large dimensions involved, exact results (obtained from a direct diagonalization) were only obtained for small values of the boson number. Thus, a comparison with the corresponding mean-field results, valid for $N \rightarrow \infty$, was not possible. Therefore, it is of interest to carry out such a comparison for a model with similar physics content than IBM-2. In particular, it has been shown that the IBM-1 and the Lipkin energy surfaces are equal [15] and then their phase diagrams are fully equivalent. The advantage of the two-fluid Lipkin model with respect to IBM-2 is the smaller dimensions involved, which allows one to perform exact
calculations with much larger boson numbers. Consequently, this study allows us to establish a proper comparison with the mean-field results. Finally, it is worth noting that Dicke and Jaynes-Cumming models correspond to a given limit of the two-fluid Lipkin model, in which a contraction from $u(2)$ to $\mathrm{hw}(1)$ is performed [16].

The paper is organized as follows. In Sec. II the algebraic structure of the model is outlined and the particular case of the consistent- $Q$-like Hamiltonian is worked out. Section III is devoted to study the classical limit of the model (mean field). In Sec. IV a numerical study of the phase diagram is presented. Section V is devoted to the application of the catastrophe theory in the study of the phase diagram and the unambiguous determination of the order of the different phase transitions. Finally, Sec. VI contains the summary and the conclusions.

## II. THE LIPKIN MODEL AND ITS TWO-FLUID EXTENSION

The Lipkin model was proposed by Lipkin, Meshkov, and Glick in Ref. [17] as a toy model that is exactly solvable through a simple diagonalization and appropriated to check the validity and limitations of different approximation methods used in many-body physics (in particular in nuclear physics). Since then, a plethora of applications have appeared in the literature. Using a boson representation, the model is built in terms of scalar bosons that can occupy two nondegenerated energy levels labeled by $s$ and $t$. In the simplest case, the building blocks are the creation- $s^{\dagger}, t^{\dagger}$ - and annihilation- $s$, $t$-boson operators. The four possible bilinear products of one creation and one annihilation boson generate the $u(2)$ algebra. If one combines two coupled Lipkin structures, one
obtains the two-fluid Lipkin model. In this model, there are two boson families identified by a subindex $-s_{1}^{\dagger}, t_{1}^{\dagger}$ and $s_{2}^{\dagger}$, $t_{2}^{\dagger}$-and the corresponding dynamical algebra is $\mathrm{u}_{1}(2) \otimes \mathrm{u}_{2}(2)$, whose generators are $s_{i}^{\dagger} s_{i}, s_{i}^{\dagger} t_{i}, t_{i}^{\dagger} s_{i}$, and $t_{i}^{\dagger} t_{i}$, for $i=1,2$. If the boson number in each fluid is conserved, it is also of interest to consider the dynamical subalgebra $\mathrm{su}_{1}(2) \otimes \mathrm{su}_{2}(2)$ with generators

$$
\begin{equation*}
J_{i}^{+}=t_{i}^{\dagger} s_{i}, \quad J_{i}^{-}=s_{i}^{\dagger} t_{i}, \quad J_{i}^{0}=\frac{1}{2}\left(t_{i}^{\dagger} t_{i}-s_{i}^{\dagger} s_{i}\right) \tag{2}
\end{equation*}
$$

which verify the angular momentum commutation relations,

$$
\begin{equation*}
\left[J_{i}^{+}, J_{i}^{-}\right]=2 J_{i}^{0}, \quad\left[J_{i}^{0}, J_{i}^{ \pm}\right]= \pm J_{i}^{ \pm} \tag{3}
\end{equation*}
$$

Adding the operators $N_{i}=s_{i}^{\dagger} s_{i}+t_{i}^{\dagger} t_{i}$, one recovers the $\mathrm{u}_{1}(2) \otimes \mathrm{u}_{2}(2)$ algebra.

We consider that $s$ and $t$ present a different behavior with respect to the parity operator,

$$
\begin{align*}
& P t_{i}^{\dagger} P^{-1}=-t_{i}^{\dagger}, \quad P t_{i} P^{-1}=-t_{i} \\
& P s_{i}^{\dagger} P^{-1}=s_{i}^{\dagger}, \quad P s_{i} P^{-1}=s_{i} \tag{4}
\end{align*}
$$

Therefore, $s$ bosons preserve the parity while $t$ bosons do not; i.e., $s$ has positive parity while $t$ has negative. In $\mathrm{u}(2)$ this assignment is arbitrary, but in higher-dimensional models it appears from physical considerations.

A detailed description of the $u_{1}(2) \otimes u_{2}(2)$ algebraic structure can be found in Ref. [18]. Here we present just an abridged version of that analysis. Starting from the dynamical algebra $u_{1}(2) \otimes u_{2}(2)$, the possible subalgebra chains are four: two of them correspond to an early coupling of the dynamical algebras into the direct-sum subalgebra $\mathrm{u}_{12}(2)$ [or $\mathrm{su}_{12}(2)$ ],

$$
\begin{array}{ccccc}
\hline \mathrm{u}_{1}(2) \otimes \mathrm{u}_{2}(2) & \supset & \mathrm{u}_{12}(2) & \supset & \mathrm{u}_{12}(1)  \tag{5}\\
\downarrow & & \downarrow & & \downarrow \\
N_{1} \otimes N_{2} & & {\left[h, h^{\prime}\right]} & & n_{t} \rightarrow \text { basis }\left|N_{1} N_{2} h n_{t}\right\rangle
\end{array}
$$

where the labels of the irreps verify the following branching rules: $h+h^{\prime}=N_{1}+N_{2}, h \geqslant h^{\prime}, 1 / 2\left(N_{1}+N_{2}+h^{\prime}-h\right) \leqslant n_{t} \leqslant$ $1 / 2\left(N_{1}+N_{2}-h^{\prime}+h\right)$, and

where $j_{i}=N_{i} / 2, j=1 / 2\left(N_{1}+N_{2}\right), 1 / 2\left(N_{1}+N_{2}\right)-1, \ldots, 1 / 2\left|N_{1}-N_{2}\right|,-j \leqslant \mu \leqslant j$, and $j=1 / 2\left(h-h^{\prime}\right) .|\cdots\rangle$ stands for the basis state in the corresponding dynamical symmetry.

The second two algebras correspond to a late coupling into a direct-sum subalgebra,

where $n_{t_{i}} \leqslant N_{i}$, and
where $-j_{i} \leqslant \mu_{i} \leqslant j_{i}$.

Concerning the Hamiltonian, the most general up to two-body interaction Hamiltonian can be written as

$$
\begin{equation*}
H=H_{1}+H_{2}+H_{12} \tag{9}
\end{equation*}
$$

where

$$
\begin{align*}
H_{i} & =a_{i} J_{i}^{\prime 0}+b_{i}\left(J^{+}+J^{-}\right)+c_{i}\left(J_{i}^{+} J_{i}^{-}\right)+d_{i}\left[\left(J_{i}^{+}\right)^{2}+\left(J_{i}^{-}\right)^{2}\right]+e_{i}\left(J_{i}^{+} J_{i}^{\prime 0}+J_{i}^{\prime 0} J_{i}^{-}\right)+f_{i}\left(J_{i}^{\prime 0}\right)^{2}  \tag{10}\\
H_{12} & =w_{1}\left(J_{1}^{+} J_{2}^{+}+J_{1}^{-} J_{2}^{-}\right)+w_{2}\left(J_{1}^{+} J_{2}^{-}+J_{1}^{-} J_{2}^{+}\right)+w_{3}\left(J_{1}^{+} J_{2}^{\prime 0}+J_{1}^{-} J_{2}^{\prime 0}\right)+w_{4}\left(J_{1}^{\prime 0} J_{2}^{+}+J_{1}^{\prime 0} J_{2}^{-}\right)+w_{5} J_{1}^{\prime 0} J_{2}^{\prime 0} \tag{11}
\end{align*}
$$

where

$$
\begin{equation*}
J_{i}^{\prime 0}=J_{i}^{0}+\frac{N_{i}}{2} \tag{12}
\end{equation*}
$$

In an equivalent way the Hamiltonian can be expressed as

$$
\begin{align*}
H_{i} & =a_{i} t_{i}^{\dagger} t_{i}+b_{i}\left(t_{i}^{\dagger} s_{i}+s_{i}^{\dagger} t_{i}\right)+c_{i}\left(t_{i}^{\dagger} s_{i} s_{i}^{\dagger} t_{i}\right)+d_{i}\left(t_{i}^{\dagger} s_{i} t_{i}^{\dagger} s_{i}+s_{i}^{\dagger} t_{i} s_{i}^{\dagger} t_{i}\right)+e_{i}\left(t_{i}^{\dagger} s_{i} t_{i}^{\dagger} t_{i}+t_{i}^{\dagger} t_{i} s_{i}^{\dagger} t_{i}\right)+f_{i} t_{i}^{\dagger} t_{i} t_{i}^{\dagger} t_{i}  \tag{13}\\
H_{12} & =w_{1}\left(t_{1}^{\dagger} s_{1} t_{2}^{\dagger} s_{2}+s_{1}^{\dagger} t_{1} s_{2}^{\dagger} t_{2}\right)+w_{2}\left(t_{1}^{\dagger} s_{1} s_{2}^{\dagger} t_{2}+s_{1}^{\dagger} t_{1} t_{2}^{\dagger} s_{2}\right)+w_{3}\left(t_{1}^{\dagger} s_{1} t_{2}^{\dagger} t_{2}+s_{1}^{\dagger} t_{1} t_{2}^{\dagger} t_{2}\right)+w_{4}\left(t_{1}^{\dagger} t_{1} t_{2}^{\dagger} s_{2}+t_{1}^{\dagger} t_{1} s_{2}^{\dagger} t_{2}\right)+w_{5} t_{1}^{\dagger} t_{1} t_{2}^{\dagger} t_{2} \tag{14}
\end{align*}
$$

## The consistent- $Q$-like Hamiltonian

A more restricted Hamiltonian, which is inspired in the consistent- $Q$ formalism of the IBM [19], is used throughout the rest of the paper. This Hamiltonian resembles the schematic one used in many IBM-2 calculations; it was studied in detail in Refs. $[10,20]$ and is the reference Hamiltonian in this work. The Hamiltonian can be written as

$$
\begin{equation*}
H=x\left(n_{t_{1}}+n_{t_{2}}\right)-\frac{1-x}{N_{1}+N_{2}} Q^{\left(y_{1}, y_{2}\right)} Q^{\left(y_{1}, y_{2}\right)} \tag{15}
\end{equation*}
$$

where

$$
\begin{align*}
n_{t_{i}} & =t_{i}^{\dagger} t_{i}  \tag{16}\\
Q^{\left(y_{1}, y_{2}\right)} & =\left(Q_{1}^{y_{1}}+Q_{2}^{y_{2}}\right)  \tag{17}\\
Q_{i}^{y_{i}} & =s_{i}^{\dagger} t_{i}+t_{i}^{\dagger} s_{i}+y_{i}\left(t_{i}^{\dagger} t_{i}\right) \tag{18}
\end{align*}
$$

Owing to the behavior of the bosons under parity (4), the Hamiltonian (15) is, in general, non-parity-conserving, except for $y_{1}=y_{2}=0$. This Hamiltonian (15) can be obtained from the general one (9), (13), (14) with the relations among parameters

$$
\begin{align*}
a_{i} & =x-2 \frac{x-1}{N_{1}+N_{2}}, \quad b_{i}=\frac{x-1}{N_{1}+N_{2}} y_{i} \\
c_{i} & =2 \frac{x-1}{N_{1}+N_{2}}, \quad d_{i}=\frac{x-1}{N_{1}+N_{2}}  \tag{19}\\
e_{i} & =2 y_{i} \frac{x-1}{N_{1}+N_{2}}, \quad f_{i}=y_{i}^{2} \frac{x-1}{N_{1}+N_{2}}, \quad \Delta_{i}=x-1 \\
w_{1} & =w_{2}=2 \frac{x-1}{N_{1}+N_{2}}, \quad w_{3}=2 y_{1} \frac{x-1}{N_{1}+N_{2}}  \tag{20}\\
w_{4} & =2 y_{2} \frac{x-1}{N_{1}+N_{2}}, \quad w_{5}=2 y_{1} y_{2} \frac{x-1}{N_{1}+N_{2}} \tag{21}
\end{align*}
$$

(please note that $\Delta_{i}$ correspond to a shift in the energy origins), leading to the compact form,

$$
\begin{align*}
H= & x\left(J_{1}^{\prime 0}+J_{2}^{\prime 0}\right)-\frac{1-x}{N_{1}+N_{2}} \\
& \times\left(J_{1}^{+}+J_{1}^{-}+J_{2}^{+}+J_{2}^{-}+y_{1} J_{1}^{\prime 0}+y_{2} J_{2}^{\prime 0}\right) \\
& \times\left(J_{1}^{+}+J_{1}^{-}+J_{2}^{+}+J_{2}^{-}+y_{1} J_{1}^{\prime 0}+y_{2} J_{2}^{\prime 0}\right) \tag{22}
\end{align*}
$$

This Hamiltonian is a mixture of dynamical symmetries of the problem, particularly $\mathrm{u}_{1}(1) \otimes \mathrm{u}_{2}(1)$ for $x=1$, and $\mathrm{su}_{1}(2) \otimes \mathrm{su}_{2}(2)$ for $x=0$ and $y_{1}=y_{2}=0$. This form is especially suitable to study QPTs, because one can associate a symmetric (spherical) phase to the first term of the Hamiltonian and a nonsymmetric (deformed) shape to the second term. Moreover, depending on the values of $y_{1}$ and $y_{2}$ different kinds of deformation are produced.

## III. THE CLASSICAL LIMIT

The study of QPTs should be strictly done in the thermodynamic limit, i.e., for an infinity number of particles. Fortunately, this kind of calculation can be easily performed through the use of the mean-field approximation, which, indeed, coincides with the exact result in the large particle number limit [21]. The mean-field analysis of the model starts considering the product of two boson condensates, one for each fluid,

$$
\begin{equation*}
|g\rangle=\frac{1}{\sqrt{N_{1}!N_{2}!}}\left(\Gamma_{1}^{\dagger}\right)^{N_{1}}\left(\Gamma_{2}^{\dagger}\right)^{N_{2}}|0\rangle \tag{23}
\end{equation*}
$$

where $|0\rangle$ is the boson vacuum and $\Gamma_{i}^{\dagger}$ the boson creation operator for the $i$ fluid defined as

$$
\begin{equation*}
\Gamma_{i}^{\dagger}=\frac{1}{\sqrt{1+\beta_{i}^{2}}}\left(s_{i}^{\dagger}+\beta_{i} t_{i}^{\dagger}\right) \tag{24}
\end{equation*}
$$

The coefficients $\beta_{1}$ and $\beta_{2}$ are variational parameters associated with each fluid that, in turn, become order parameters.

The mean-field energy for the consistent- $Q$-like Hamiltonian for a symmetric system, i.e., a system with $N_{1}=N_{2}$, in the large- $N\left(N=N_{1}+N_{2}\right)$ limit can be written as

$$
\begin{equation*}
\frac{E\left(\beta_{1}, \beta_{2}, x, y_{1}, y_{2}\right)}{N}=\frac{x}{2}\left(\frac{\beta_{1}^{2}}{1+\beta_{1}^{2}}+\frac{\beta_{2}^{2}}{1+\beta_{2}^{2}}\right)-\frac{1-x}{4}\left[\left(Q_{1}\right)^{2}+\left(Q_{2}\right)^{2}+2 Q_{1} Q_{2}\right] \tag{25}
\end{equation*}
$$

with

$$
\begin{equation*}
Q_{i}=\frac{1}{1+\beta_{i}^{2}}\left(2 \beta_{i}+y_{i} \beta_{i}^{2}\right) \tag{26}
\end{equation*}
$$

Inserting these expressions for $Q_{i}$ in Eq. (25), we get

$$
\begin{align*}
\frac{E\left(\beta_{1}, \beta_{2}, x, y_{1}, y_{2}\right)}{N}= & \frac{x}{2}\left(\frac{\beta_{1}^{2}}{1+\beta_{1}^{2}}+\frac{\beta_{2}^{2}}{1+\beta_{2}^{2}}\right)-\frac{1-x}{4}\left[\frac{1}{\left(1+\beta_{1}^{2}\right)^{2}}\left(2 \beta_{1}+y_{1} \beta_{1}^{2}\right)^{2}+\frac{1}{\left(1+\beta_{2}^{2}\right)^{2}}\left(2 \beta_{2}+y_{2} \beta_{2}^{2}\right)^{2}\right. \\
& \left.+2 \frac{1}{\left(1+\beta_{1}^{2}\right)} \frac{1}{\left(1+\beta_{2}^{2}\right)}\left(2 \beta_{1}+y_{1} \beta_{1}^{2}\right)\left(2 \beta_{2}+y_{2} \beta_{2}^{2}\right)\right] \tag{27}
\end{align*}
$$

Please note that, contrary to the IBM-2 case where for $\chi_{\pi}=-\chi_{\nu}$ the energy surface is invariant under the transformation $\beta_{\pi} \leftrightarrow \beta_{v}$, the double Lipkin model with $y_{1}=-y_{2}$ is symmetric under the interchange $\beta_{1} \leftrightarrow-\beta_{2}$.

It could be also of interest to write the energy for the nonsymmetric case for analyzing how the difference in the relative number of bosons affects the mean-field energy,

$$
\begin{align*}
\frac{E\left(\beta_{1}, \beta_{2}, x, y_{1}, y_{2}\right)}{N}= & x\left[F_{1} \frac{\beta_{1}^{2}}{1+\beta_{1}^{2}}+\left(1-F_{1}\right) \frac{\beta_{2}^{2}}{1+\beta_{2}^{2}}\right]-(1-x)\left[\frac{F_{1}^{2}}{\left(1+\beta_{1}^{2}\right)^{2}}\left(2 \beta_{1}+y_{1} \beta_{1}^{2}\right)^{2}+\frac{\left(1-F_{1}\right)^{2}}{\left(1+\beta_{2}^{2}\right)^{2}}\left(2 \beta_{2}+y_{2} \beta_{2}^{2}\right)^{2}\right. \\
& \left.+2 \frac{F_{1}}{\left(1+\beta_{1}^{2}\right)} \frac{\left(1-F_{1}\right)}{\left(1+\beta_{2}^{2}\right)}\left(2 \beta_{1}+y_{1} \beta_{1}^{2}\right)\left(2 \beta_{2}+y_{2} \beta_{2}^{2}\right)\right] \tag{28}
\end{align*}
$$

where $F_{1}=\frac{N_{1}}{N_{1}+N_{2}}$. Throughout this paper we only consider the symmetric case.

## IV. NUMERICAL ANALYSIS OF THE PHASE DIAGRAM

To study the structure of the two-fluid Lipkin model phase diagram as a function of the control parameters, $\left(x, y_{1}, y_{2}\right)$, we have found it appropriate to introduce alternative control parameters $\left(y, y^{\prime}\right)$, defined by

$$
\begin{equation*}
y=\frac{y_{1}+y_{2}}{2}, \quad y^{\prime}=\frac{y_{1}-y_{2}}{2} \tag{29}
\end{equation*}
$$

With this change, we can study the phase diagram in terms of the coordinates

$$
\begin{align*}
& \rho=1-x, \quad \theta=\frac{\pi}{24}\left(y_{1}-y_{2}\right)=\frac{\pi}{12} y^{\prime}, \\
& \phi=\frac{\pi}{24}\left(y_{1}+y_{2}\right)=\frac{\pi}{12} y \tag{30}
\end{align*}
$$

where we have assumed a maximum value for $\left|y_{1}\right|$ and $\left|y_{2}\right|$ equal to 2 so as the angles $\theta$ and $\phi$ are defined between $-\pi / 6$ and $\pi / 6$ (see Fig. 1).

The geometric representation of the two-fluid consistent-$Q$-like Lipkin Hamiltonian will be, therefore, a pyramid in this phase space. One vertex corresponds to the $u_{12}(1)$ limit of the model $(x=1)$. The bottom plane, $y_{1}=y_{2} \Rightarrow y^{\prime}=0$, corresponds to the $u_{12}(2)$ dynamical algebra [both fluid are combined symmetrically into a single $u(2)]$ algebra, which is equivalent at the mean-field level to the single Lipkin model (in the IBM-2 case, the equivalent horizontal plane represents the

IBM-1, i.e., a symmetric combination of the two boson fluids). In this plane, the line $y_{1}=y_{2}=0\left(y=y^{\prime}=0\right)$ goes from the $\mathrm{so}_{12}(2)$ to the $\mathrm{u}_{12}(1)$ limit. As soon as one considers $y_{1} \neq y_{2}$ $\left(y^{\prime} \neq 0\right)$ one moves in the vertical direction of the pyramid and any present symmetry will become broken. Of special interest is the vertical plane $y_{1}=-y_{2}\left(y=0, y^{\prime} \neq 0\right)$ because,


FIG. 1. Representation of the two-Lipkin model parameter space. For completeness, the symmetries of the model are also indicated in the diagram.


FIG. 2. Transition line for $y=0$ and $y^{\prime}=0$ changing the control parameter $x$. In the different panels we plot as a function of $x$ : panel (a) the energy per boson (in arbitrary units), panel (b) the order parameter $\beta_{1}$ (dimensionless), panel (c) the order parameter $\beta_{2}$ (dimensionless), panel (d) $d E / d x$ in arbitrary units, and panel (e) representation of the trajectory in the control parameter space. Full thin black lines correspond to the mean-field results while dashed thick red lines are the exact calculation with $N_{1}=N_{2}=500$.
for this combination of parameters, the mean-field energy is invariant under the transformation $\beta_{1} \rightarrow-\beta_{2}$. Note that the two remaining vertexes do not correspond to any symmetry of the model [in the case of IBM-2 they correspond to the su(3) and su(3)* symmetries].

As a first step to establish the phase diagram of the model, in the remainder of this section we present numerical studies of different trajectories within the phase space of the model ( $\rho, y, y^{\prime}$ ) to identify the different phases and phase-transition surfaces or lines.

To get a geometrical idea about system shapes in the different regions of the phase space, we note that the region around the $u_{12}(1)$ vertex corresponds to values of the variational parameters $\beta_{1}$ and $\beta_{2}$ equal to zero. Because $\beta$ parameters give the weight of the $t$ bosons in the boson condensate, $\beta=0$ implies a condensate of spherical $s$ bosons. Consequently, the phase around the $u_{12}(1)$ vertex is called symmetric or spherical. The corresponding spectrum will become nearly harmonic. When the system goes far from the $u_{12}(1)$ vertex, both variational parameters, $\beta_{1}$ and $\beta_{2}$ become different from zero. This makes that the boson condensate in both fluids has a fraction of $t$ bosons. Thus, this phase is called nonsymmetric or deformed. The horizontal plane corresponds to $\beta_{1}=\beta_{2}$, which implies equal deformations for both fluids, which brings us back to the single Lipkin model.

To study the possible phase transitions that occur in the phase diagram, we have performed numerical analysis through selected straight trajectories in the phase space. For each of them the equilibrium energy, the derivatives of the energy functional, and also the equilibrium values of the variational parameters have been analyzed. All exact calculations
presented in this section correspond to $N_{1}=N_{2}=500$, but similar studies can be done for $N_{1} \neq N_{2}$ and other boson numbers.

## A. Plane $\boldsymbol{y}^{\prime}=0$

First, we start analyzing the bottom plane that corresponds to $y_{1}=y_{2}=y$ and $y^{\prime}=0$; therefore, an energy surface fully equivalent to the single Linkin case is reproduced. In Fig. 2 the line $y_{1}=y_{2}=y=0$ and $y^{\prime}=0$ is studied [see panel (e)]; in the figure the energy per particle [panel (a)], as well as the deformation parameters [panels (b) and (c)], as functions of the control parameter $x$ are plotted. We have also included the function $d E / d x$ in panel (d). One can clearly see how a phase transition sets up around $x=4 / 5$. At the mean-field level the phase transition is established as second order because a discontinuity appears in the second derivative of the energy [see panel (d), where $d E / d x$ is continuous but not its derivative] and in the first derivative of the order parameters. Note that, owing to symmetry arguments, $\beta_{1}=\beta_{2}$ over the whole plane. In Fig. 2 the mean-field results (black solid line) are shown together with the exact result coming from direct diagonalization (red dashed line) for $N_{1}=N_{2}=500$. In the exact calculation, the values of the order parameters are extracted using this relationship,

$$
\begin{equation*}
\beta_{i}=\sqrt{\frac{\left\langle n_{t_{i}}\right\rangle}{N_{i}-\left\langle n_{t_{i}}\right\rangle}} . \tag{31}
\end{equation*}
$$

Excellent agreement is found between mean-field and exact results because the number of bosons considered in the exact diagonalization is large enough.


FIG. 3. Same as Fig. 2, but with $y_{1}=y_{2}=y=1$ and $y^{\prime}=0$.

In Fig. 3 we repeat the same calculation but for the line $y_{1}=$ $y_{2}=y=1$ and $y^{\prime}=0$ [see panel (e)]. In this case, a first-order phase transition is observed for $x_{c}=5 / 6=0.833$. The order of the phase transition is clear from the discontinuity in the value of the order parameter at the mentioned phase-transition point, as well as for the discontinuity in $d E / d x$ [see panel (d)]. In general, for $y_{1}=y_{2}=y \neq 0$ the phase transition is of first order and the critical point is located at [15]

$$
\begin{equation*}
x_{c}=\frac{4+y^{2}}{5+y^{2}} . \tag{32}
\end{equation*}
$$

Consequently, the location of the critical point is shifted to slightly larger values of $x$ as $y$ increases, while the jump of the order parameter at the phase-transition point becomes larger.

## B. Volume region inside the pyramid: $\boldsymbol{y} \neq 0$ and $\boldsymbol{y}^{\prime} \neq 0$

Now a trajectory going through the inner part of the pyramid is analyzed. In particular, the case $y_{1}=1$ and $y_{2}=-1 / 2$, i.e., $y=1 / 4$ and $y^{\prime}=3 / 4$, is presented in Fig. 4(e). From this figure, it is clear that a first-order phase transition is observed at around $x_{c}=0.805$. Several trajectories inside the pyramid have been studied with similar results (the dependence on $y$ and $y^{\prime}$ of $x_{c}$ is involved and cannot be obtained in a closed form). The size of the discontinuity depends on how far the values of $y$ and $y^{\prime}$ are from $y=0$ and $y^{\prime}=0$.

## C. The vertical plane: $\boldsymbol{y}=\mathbf{0}$

The vertical plane corresponds to $y_{1}=-y_{2}$, which means $y=0$ and $y^{\prime}=y_{1}=-y_{2}$ and, as we show below, is the most interesting case. Several trajectories inside this plane are presented, with one crossing the plane from positive to negative $\beta$ values.

The first trajectory is the line $y_{1}=-y_{2}=y^{\prime}=1 / 2$, and the results are depicted in Fig. 5. A second-order phase transition at $x_{c}=0.8$ is observed. The order parameters, coming from the exact diagonalization, show an oscillatory pattern owing to the degeneracy of two states that are related with the two minima present in the $\beta_{1}-\beta_{2}$ plane of the mean-field energy (see Fig. 9). The degeneracy of two states with different deformation makes that the order parameter obtained from the diagonalization may jump from one minimum to the other (between the two degenerate mean-field values). Indeed, for a given value of $x$ the equilibrium value of one of the order parameters will correspond to $\beta_{1}=\beta_{x}$ and $\beta_{2}=\beta_{x}^{\prime}$, while the other will correspond to $\beta_{1}=-\beta_{x}^{\prime}$ and $\beta_{2}=-\beta_{x}$. Note that we have taken the absolute value of $\beta_{i}$ for a better comparison with the exact results, which are, by definition, positive.

In Fig. 6 a calculation along the line $y_{1}=-y_{2}=y^{\prime}=1$ and $y=0$ is presented. In this case it is difficult to disentangle the order of the phase transition just looking at the energy and the order parameters; however, in the inset panel it is clear that a discontinuity in the second derivative of the energy exists, which, once more, happens at around $x_{c}=0.8$. In Sec. V B we see in detail that, indeed, a divergence in $d^{2} E / d x^{2}$ exists and we try to understand the reason why there is a divergence in the second derivative. Note that $d E / d x$ becomes vertical at $x=4 / 5$ from the left side.

Finally, in Fig. 7 the calculation along the line $y_{1}=-y_{2}=$ $y^{\prime}=3 / 2$ and $y=0$ is shown. In this calculation, the onset of a first-order phase transition at around $x_{c}=0.81$ is easily appreciated, i.e., discontinuity in the first derivative of the energy and in the value of the order parameters.

After the analysis of the different paths in the plane $y=0$, corresponding to different $y^{\prime}$ values, one is tempted to conclude


FIG. 4. Same as Fig. 2, but with $y_{1}=1$ and $y_{2}=-1 / 2\left(y=1 / 4\right.$ and $\left.y^{\prime}=3 / 4\right)$.
that there is a line of phase transition for values of $x$ around $x_{c}=0.8$. However, the value $y^{\prime}=1$ separates this line into two parts: For values $y^{\prime} \leqslant 1$ the line corresponds to a second-order phase transition, while for values $y^{\prime}>1$ the line is of first order. This weak conclusion, based on numerical calculations, is confirmed in Sec. V B through an analytic study.

It is worth noting that the vertical plane $y=0$ for $x<$ $4 / 5$ separates two deformed regions. To study the transition between both deformed regions, finally, a line crossing this
vertical surface is analyzed. Here, because of the presence of two degenerated minima, a first-order phase transition for the whole vertical surface in the deformed phase is expected. This is fully confirmed in Fig. 8 (parameters $x=0.5, y=1$ ), where the first-order phase transition appears for $y_{2}=-1$. Please note that in Fig. 8 we have changed by hand the value of $\beta$ coming from the exact calculation (it is, by definition, always positive) for a better comparison with the mean-field results.


FIG. 5. Same as Fig. 2, but with $y_{1}=-y_{2}=y^{\prime}=1 / 2$ and $y=0$.


FIG. 6. Same as Fig. 2, but with $y_{1}=-y_{2}=y^{\prime}=1$ and $y=0$.

Combining all the preceding evidence one gets the phase diagram depicted in Fig. 9, where one can appreciate a first-order phase transition surface separating the symmetric (spherical) and nonsymmetric (deformed) phases and the firstorder phase-transition vertical surface separating two different deformed phases. We see in next section that the intersection line between both surfaces, from $y^{\prime}=0$ up to $y^{\prime}=1$, is a
second-order phase-transition line, while for larger values of $y^{\prime}$ it becomes first order. Note that the phase diagram can be extended to negative values of $y$ and $y^{\prime}$, with the first-order phase transition surface separating spherical and deformed phase extended to four quadrants and the vertical first-order phase transition surface and the second-order phase-transition line extended to negative values of $y^{\prime}$.

(e)

FIG. 7. Same as Fig. 2, but with $y_{1}=-y_{2}=y^{\prime}=3 / 2$ and $y=0$.


FIG. 8. Transition for $x=0$ and $y_{1}=1$ as functions of $y_{2}$. In panel (a) the energy per boson is plotted in arbitrary units, in panel (b) the order parameter $\beta_{1}$ (dimensionless) is shown, in panel (c) the order parameter $\beta_{2}$ (dimensionless) is represented, in panel (d) $d E / d x$ in arbitrary units is plotted, and in panel (e) the representation of the trajectory in the control parameter space is shown. Solid thin black lines correspond to the mean-field results, while dashed thick red lines are the exact calculation with $N_{1}=N_{2}=500$.


FIG. 9. Phase diagram of the consistent- $Q$-like two-fluid Lipkin model. In the diagram the different phases are represented: spherical and deformed, the first-order QPT surfaces, and the second-order QPT line. Moreover, the relevant control parameters and dynamical symmetries also are shown.

## V. LOCAL TAYLOR EXPANSION AND CATASTROPHE THEORY

## A. Fundamentals

Once the main structure of the phase diagram of the model is known numerically, it is necessary to perform an analytic study to determine unambiguously the order of the phase transitions of surfaces and lines appearing in the phase diagram and to understand why the QPT areas are precisely located there. To carry out this task we will make use of catastrophe theory (CT) [22], which is an ideal tool for such an end.

In general, the aim of CT is to study a given potential, $V(\vec{x}, \vec{\lambda}) \in \Re$ (in our case, the mean-field energy surface of the model), or a family of potentials that are the function of a set of order parameters, $\vec{x} \in \mathfrak{R}^{n}$, that depend on a set of control parameters, $\vec{\lambda} \in \mathfrak{R}^{r}$, and to study the qualitative behavior of the potential, e.g., number of minima and maxima, as a function of the control parameters. To proceed, one should start looking for the stationary points (also known as critical points), i.e., those whose gradients vanish, and classify them according to their stability: (i) points where the determinant of the Hessian matrix is different from zero, called isolated, nondegenerated or Morse points and (ii) points where the determinant of the Hessian matrix is zero, called nonisolated, degenerated or non-Morse points. In summary, points of a family of smooth potentials can be classified according to their gradient and Hessian matrix $\mathcal{H}$ as
(i) regular points, $\nabla V \neq 0$;
(ii) Morse points (isolated critical points), $\nabla V=0$ and $|\mathcal{H}| \neq 0 ;$
(iii) non-Morse points (degenerated critical points), $\nabla V=$ 0 and $|\mathcal{H}|=0$.

The Morse theorem [23,24] guarantees that around a Morse point, a smooth potential is equivalent to a quadratic form, performing a smooth nonlinear change of variables. Therefore, the potential is stable under small perturbations around Morse points. At non-Morse points the potential cannot be written as a quadratic form because the Hessian matrix has at least one zero eigenvalue. Around non-Morse points CT will provide useful information on how the qualitative shape of the potential will evolve under small variations of the order parameters.

In the case of several order parameters, Thom's splitting lemma [22] guarantees that a smooth potential at non-Morse points can be written as a sum of a quadratic form, associated with the subspace with nonzero eigenvalues, plus a function containing the variables associated to the zero eigenvalues of the Hessian matrix.

The first step in the CT program is to find out the critical points of the energy surface $(\nabla E=0)$. Among them, the most important is the most degenerate one, i.e., the point where most successive derivatives vanish. This point is the fundamental root taking place at definite values of the control parameters, which we call critical values. We next proceed to make use of a Taylor expansion of the energy surface around the fundamental root. A Taylor expansion around such a point is also valid for the critical points that arise from the fundamental root when the degeneracy is broken. Depending on the degeneracy of the fundamental root, the number of extremes that can be analyzed
simultaneously will change. It is worth noting that the different minima related with the appearance of a critical phenomenon arise from a degenerated non-Morse point.

When the potential depends on several variables, as the case for the two-fluid Lipkin model is, it is important to separate the variables into two sets, depending on how Hessian eigenvalues behave. On one hand, one has the variables associated with the subspace with vanishing Hessian eigenvalues, called bad or essential variables, while, however, there is a set of variables related to the nonvanishing Hessian eigenvalues, called good or nonessential variables. Therefore, as a consequence of the splitting lemma [22], the potential could be separated into a part depending on the essential variables and into another part depending on the nonessential ones by rewriting it in terms of the eigenvectors of the Hessian matrix [24]. The appearance of critical phenomena will be associated exclusively with the behavior of the essential variables, i.e., the variables that can be identified as order parameters of the system.

## B. Application to the two-fluid Lipkin model

According to Eqs. (27) and (28), the most degenerated critical point for the two-fluid Lipkin model (15) corresponds to $\beta_{1}=0$ and $\beta_{2}=0$ (all derivatives up to fourth order vanish for an appropriated set of parameters) and, taking into account the shape of the phase diagram, all the critical points that can eventually arise in the energy surface are born from this most degenerated critical point. Because there are two shape variables it is necessary to construct, first, the Hessian matrix associated to the energy surface (27),

$$
\mathcal{H}=\left(\begin{array}{cc}
\partial^{2} E / \partial \beta_{1}^{2} & \partial^{2} E / \partial \beta_{1} \partial \beta_{2}  \tag{33}\\
\partial^{2} E / \partial \beta_{2} \partial \beta_{1} & \partial^{2} E / \partial \beta_{2}^{2}
\end{array}\right)=\left(\begin{array}{cc}
3 x-2 & 2 x-2 \\
2 x-2 & 3 x-2
\end{array}\right) .
$$

The two eigenvalues are $5 x-4$ and $x$, and the corresponding eigenvectors are

$$
\begin{align*}
& \beta_{a}=\frac{1}{2}\left(\beta_{1}+\beta_{2}\right)  \tag{34}\\
& \beta_{b}=\frac{1}{2}\left(\beta_{1}-\beta_{2}\right) . \tag{35}
\end{align*}
$$

The eigenvalue associated with $\beta_{a}$ vanishes for $x=4 / 5$, while the one associated with $\beta_{b}$ only vanishes for the trivial case $x=0$. Therefore, the essential variable turns out to be $\beta_{a}$, while $\beta_{b}$ becomes the nonessential one; i.e., the origin in this variable behaves as a Morse point.

The next step is to carry out a Taylor expansion in $\beta_{a}$ and $\beta_{b}$ around zero. Because we use $\beta_{a}$ and $\beta_{b}$, the quadratic term $\beta_{a} \beta_{b}$ will not be present in the Taylor expansion. Note that we are considering the case $N_{1}=N_{2}$,

$$
\begin{aligned}
\frac{E\left(x, y, y^{\prime}, \beta_{a}, \beta_{b}\right)}{N}= & (5 x-4) \beta_{a}^{2}+4(x-1) y \beta_{a}^{3} \\
& +\left[8-9 x+y^{2}(x-1)\right] \beta_{a}^{4}+\Theta\left(\beta_{a}^{5}\right) \\
& +x \beta_{b}^{2}+\Theta\left(\beta_{a} \beta_{b}^{2}, \beta_{b} \beta_{a}^{2}\right)
\end{aligned}
$$

To cancel the higher-order terms ( $\beta_{a}^{i} \beta_{b}^{j}$ with $j>1$ ), we have to implement a nonlinear transformation in $\beta_{b}$

$$
\begin{equation*}
\tilde{\beta}_{b}=\beta_{b}+\sum_{i+j>1} a_{i j} \beta_{a}^{i} \beta_{b}^{j} \tag{36}
\end{equation*}
$$

$$
\begin{align*}
\frac{E\left(x, y, y^{\prime}, \beta_{a}, \beta_{b}\right)}{N}= & (5 x-4) \beta_{a}^{2}+4(x-1) y \beta_{a}^{3}+\left[8-9 x+y^{2}(x-1)-\frac{16 y^{\prime 2}}{x}(x-1)^{2}\right] \beta_{a}^{4} \\
& +\frac{8(x-1) y\left[\left(6 y^{\prime 2}-1\right) x^{2}-14 y^{\prime 2} x+8 y^{\prime 2}\right]}{x^{2}} \beta_{a}^{5} \\
& +\frac{1}{x^{3}}\left\{\left[64 y^{\prime 4}-384 y^{\prime 2}-2 y^{2}\left(82 y^{\prime 2}+1\right)+13\right) x^{4}+2\left(-96 y^{\prime 4}+576 y^{\prime 2}\right.\right. \\
& \left.+y^{2}\left(372 y^{\prime 2}+1\right)-6\right] x^{3}+4 y^{\prime 2}\left[48\left(y^{\prime 2}-6\right)-313 y^{2}\right] x^{2} \\
& \left.+32 y^{\prime 2}\left(29 y^{2}-2 y^{\prime 2}+12\right) x-256 y^{2} y^{\prime 2}\right\} \beta_{a}^{6}+O\left(\beta_{a}^{7}\right)+x \beta_{b}^{2} \tag{37}
\end{align*}
$$

The number of lower-order terms that are kept in the Taylor expansion without losing substantial information with respect to the original function (problem of determinacy) is determined studying the terms in the Taylor expansion that can be canceled out with appropriated particular values of the control parameters. For Eq. (37) the values of the control parameters, $x=4 / 5, y=0$, and $y^{\prime}=1$ cancel all terms up to $\beta_{a}^{5}$. Therefore, the dominant remaining term is $\beta_{a}^{6}$ and it is said that the function is $6-$ determined. Hence, the number of essential parameters will be 3 . Consequently, the relevant elementary catastrophe of this model is the butterfly $\left(A_{+5}\right)$ [24]. It is worth mentioning that the butterfly has a codimension equal to 4 ; i.e., the number of essential parameters is 4 . In our case, owing to the function symmetry, the number of parameters is only 3 . In general, depending on the values selected for the control parameters, the potential energy may have three, two, or one local minima. Please note that Eq. (37) does not correspond to the canonical form of the butterfly because it presents a fifth-order term instead of the first-order one. However, one always can perform a shift transformation in the $\beta_{a}$ variable to recover the canonical form.

To determine the order of the phase transitions, already studied numerically in the preceding section, we can take advantage of Eq. (37). In general, for any situation with $y \neq 0$ the cubic (and fifth) term always survives for any value of $y^{\prime}$ and, therefore, the phase transition will become first order. The reason is simple: The presence of a cubic (and fifth) term guarantees the possible appearance of several critical points (i.e., a region of coexistence), three critical points (two minima and one maximum) when the $\beta_{a}^{2}$ coefficient and the $\beta_{a}^{4}$ coefficient are positive and five critical points (three minima and two maxima) when the $\beta_{a}^{2}$ coefficient is positive and the $\beta_{a}^{4}$ coefficient is negative (see below for more details). Note that in our case the $\beta_{a}^{6}$ coefficient is always positive. Indeed, this particular situation is precisely the one necessary to develop a first-order phase transition. This happens in almost the whole surface separating the symmetric (spherical) and nonsymmetric (deformed) phases.

To know the character of the vertical surface, $y=0$ (with $x<4 / 5$ ), one can note that the lowest leading terms are $\beta_{a}^{2}$ with negative coefficient and $\beta_{a}^{4}$ with positive coefficient. This
potential gives rise to two degenerated minima symmetric with respect to the origin, $\beta_{a}=0$. As soon as one perturbs the system, changing $y$ (to either positive or negative values) the degeneracy is broken and one of the deformed minima is lower in energy. Therefore, this situation corresponds to a first-order phase transition because the order parameter will jump suddenly from one to the other minimum.

It is also of interest to see how one can recover the case corresponding to the single Lipkin, i.e., $y^{\prime}=0$. For this case (horizontal plane) the energy surface reads as

$$
\begin{align*}
& \frac{E\left(x, y, y^{\prime}, \beta_{a}, \beta_{b}\right)}{N} \\
& \quad=(5 x-4) \beta_{a}^{2}+4(x-1) y \beta_{a}^{3} \\
& \quad+\left[y^{2}(x-1)+8-9 x\right] \beta_{a}^{4}+O\left(\beta_{a}^{5}\right)+x \beta_{b}^{2} \tag{38}
\end{align*}
$$

where one can easily single out that for the line $x=4 / 5$, values $y \neq 0$ produce a first-order phase transition because the cubic term is present. For the particular value $y=0$ the cubic term vanishes and, therefore, the transition is no longer of first order, but of second order.

Finally, a most interesting case is the intersection line between the surfaces $y=0$ (vertical plane, separating two regions of different deformation) and $x \approx 4 / 5$ (spherical surface separating spherical from deformed shapes). For this situation, the energy functional is written as

$$
\begin{align*}
& \frac{E\left(x, y^{\prime}, \beta_{a}, \beta_{b}\right)}{N} \\
& =(5 x-4) \beta_{a}^{2}+\left[8-9 x-\frac{16(x-1)^{2} y^{\prime 2}}{x}\right] \beta_{a}^{4} \\
& \quad+\frac{1}{2}\left[26 x-24+\frac{128(x-1)^{3} y^{\prime 2}\left(y^{\prime 2}-6\right)}{x^{2}}\right] \beta_{a}^{6} \\
& \quad+O\left(\beta_{a}^{7}\right)+x \beta_{b}^{2} . \tag{39}
\end{align*}
$$

This situation looks like the case $y=y^{\prime}=0$, because no odd terms appear in the expansion and only the onset of a second-order phase transition is expected. However, there are fundamental differences. The key point to disentangle the
stability structure of the energy surface is the sign of the fourth-order coefficient. The phase transition at $x=4 / 5$ is indeed of second order if the fourth-order coefficient remains positive but will change to first order otherwise. There is a critical value for $y^{\prime}$ for which the fourth-order coefficient vanishes, i.e., $y^{\prime}=1$ and $x=4 / 5$. At this point, the only term that survives in the energy functional is the sixth-order term. The most important consequence is that at this point the energy surface is very flat (as $\beta_{a}^{6}$ ). Going to values with $y^{\prime}>1$, the fourth-order coefficient changes to negative sign, which implies that there is no longer a second-order phase transition, but a first-order one because, in this case, there is a sudden change in the order parameter when crossing the QPT point. To understand this fact, let us write in a more compact form the Taylor expansion (39) as

$$
\begin{equation*}
E=\frac{A}{2} \beta^{2}+\frac{B}{4} \beta^{4}+\frac{C}{6} \beta^{6} \tag{40}
\end{equation*}
$$

where $C>0$. According to Eq. (39): $A>0$ for $x>4 / 5, A<$ 0 for $x<4 / 5$, and $A=0$ for $x=4 / 5$; at $x=4 / 5, B>0$ for $y^{\prime}<1, B<0$ for $y^{\prime}>1$, and $B=0$ for $y^{\prime}=1$; for $x \approx$ $4 / 5, C$ is always positive. The equation $d E / d \beta=0$ has as solutions

$$
\begin{align*}
\beta & =0 \\
\beta^{2} & =\frac{-B \pm \sqrt{B^{2}-4 A C}}{2 C} \tag{41}
\end{align*}
$$

The spherical solution $(\beta=0)$ corresponds to a minimum if $A>0$, i.e., $x>4 / 5$ (to a maximum if $A<0$, i.e., $x<$ $4 / 5$ ), irrespective of the $B$ sign, i.e., independently of the $y^{\prime}$ value. For $A<0$ and $B>0$ (which occurs for $\left|y^{\prime}\right|<1$ ) two deformed critical points exist (symmetric with respect to the origin), which correspond to minima because, as discussed above, $\beta=0$ corresponds, in this case, to a maximum. Note that for $A=0$ the two deformed minima merge into a flat spherical one, never coexisting several minima. Therefore, the line $y=0$ and $A=0$ corresponds to a second-order phase transition while $\left|y^{\prime}\right|<1$.

For $A \gtrsim 0$ and $B<0$ (which occurs for $y^{\prime}>1$ and $x \gtrsim$ $4 / 5$ ) five critical points coexist for $B^{2}>4 A C$, one corresponds to the spherical minimum, and other two correspond to two deformed minima (symmetric with respect to the origin, $\beta_{a}=0$ ). The other two extremes correspond to maxima (symmetric with respect to the origin). The particular region $y=0, A=0(x=4 / 5)$, for values $y^{\prime}>1$, is a region of coexistence of three minima, one spherical and two deformed. At the critical point all three minima are degenerated. As a consequence, a first-order phase transition develops around this line. The first-order phase-transition line is defined then by

$$
\begin{equation*}
A=\frac{B^{2}}{4 C} \tag{42}
\end{equation*}
$$

and is bounded by the spinodal $\left[\left(\partial^{2} E / \partial \beta^{2}\right)_{\beta=0}=0\right]$ and the antispinodal $\left[\left(\partial^{2} E / \partial \beta^{2}\right)_{\beta=\beta_{c} \neq 0}=0\right]$ lines given by

$$
\begin{align*}
A & =0 \quad(\text { spinodal })  \tag{43}\\
A & =\frac{3 B^{2}}{16 C} \quad(\text { antispinodal }) \tag{44}
\end{align*}
$$

For the case $B^{2}<4 A C$ only the spherical minimum exists.

It is worth analyzing what happens at the special line $y=0$ and $y^{\prime}=1$. For this line $B=0$ and the energy surface presents three critical points when $A<0(x<4 / 5)$,

$$
\begin{align*}
& \beta=0  \tag{45}\\
& \beta= \pm\left(\frac{-A}{C}\right)^{1 / 4} \tag{46}
\end{align*}
$$

The first one, spherical, corresponds to a maximum and the second and the third, deformed and symmetric with respect to the origin, correspond to minima. For $A>0(x>4 / 5)$ only the minimum at $\beta=0$ survives. To study the QPT at $x=4 / 5$, one can write the energy at the equilibrium $\beta$ value (46), that is,

$$
\begin{align*}
& E=\frac{(-A)^{3 / 2}}{3 \sqrt{C}} \text { for } A<0  \tag{47}\\
& E=0 \quad \text { for } A>0 \tag{48}
\end{align*}
$$

Its first derivative with respect to $A$ is

$$
\begin{align*}
& \frac{d E}{d A}=\frac{-\sqrt{-A}}{2 \sqrt{C}} \quad \text { for } A<0  \tag{49}\\
& \frac{d E}{d A}=0 \quad \text { for } A>0 \tag{50}
\end{align*}
$$

Therefore, the transition is not of first order. Performing the second-order derivative,

$$
\begin{align*}
& \frac{d^{2} E}{d A^{2}}=\frac{-1}{4 \sqrt{-A C}}, \quad \text { for } A<0  \tag{51}\\
& \frac{d^{2} E}{d A^{2}}=0 \quad \text { for } A>0 \tag{52}
\end{align*}
$$

Therefore, a discontinuity appears in the second derivative with respect to the control parameter. Indeed, in the deformed side the second derivative diverges to $-\infty$.


FIG. 10. Same as Fig. 9, but including the corresponding energy curves as a function of the essential order parameter $\beta_{a}$.


FIG. 11. Representation of the butterfly catastrophe (without oddpower terms), Eq. (40), as a function of the control parameters $A$ and $B$. The energy curves that characterize every region are depicted as well as the curves corresponding to lines and points with degenerated critical points are also depicted.

In Fig. 10 we show, once more, the phase diagram, but in this case plotting the corresponding energy curves as a function of the value of the essential variable. In this figure one can appreciate in a cleaner way how the first-order vertical plane is related to two symmetric degenerated minima, symmetric with respect to $\beta_{a}=0$, while the first-order surface separating spherical and deformed phases corresponds also to two degenerated minima, spherical and deformed. The line $x=4 / 5, y=0, y^{\prime}<1$ corresponds to a $\beta_{1}^{4}$ energy curve, i.e., to a cusp line. The point $x=4 / 5, y=0, y^{\prime}=1$ corresponds to a $\beta_{1}^{6}$ energy curve and, finally, a first-order phase transition line appears for $x \approx 4 / 5, y=0, y^{\prime}>1$ with three degenerated minima. The behavior of this first-order phase-transition area is explained in detail in Fig. 11, where, as a function of the control parameters $A$ and $B$, is depicted the phase diagram, separating the areas corresponding to spherical (blue area), deformed shapes (red area), or coexistence area (yellow area). Also spinodal, antispinodal, and first-order lines are shown.

At the point $A=0, B=0$, i.e., $x=4 / 5, y=0$, and $y^{\prime}=1$, the second-order phase-transition line $(B>0)$ and the spinodal, antispinodal, and first-order phase transitions merge. This point is known as the tricritical point, while the first-order phase-transition line corresponds to a triple point curve where three minima are degenerated and coexist.

The inclusion of a third- (and a fifth-) order term in the potential (40) will break the symmetry of the function. The consequence will be the appearance of a coexistence region for
the cusp line and, therefore, its transformation in a first-order phase transition line. In the case of the coexistence area with $B<0$ the asymmetry generated in the energy curves will make impossible the degeneracy of three minima, but the degeneracy of the spherical and one of the deformed minima will continue to be possible. Moreover, the spinodal line is still at $A=0$ too, though the antispinodal one will be shifted. As a consequence, in this case, the phase transition is still of first order.

## VI. SUMMARY AND CONCLUSIONS

In this work the mean-field energy surface of the consistent-$Q$-like double Lipkin Hamiltonian has been studied. The analyzed Hamiltonian resembles the IBM-2 Hamiltonian of interest in nuclear physics. The phase diagram of the model has been established both numerical and analytically. The mean-field numerical calculations have been compared with direct diagonalizations and good agreement has been reached. The analytical study has been performed using the catastrophe theory and it has been found that the energy can be successfully described by the butterfly catastrophe.

Therefore, the phase diagram of the model has been obtained, including phases, locations of the QPT phase transitions, and their orders. In particular, there are three phases: spherical and two different deformed ones. The surface separating spherical and both deformed phases is of first order: two minima, one spherical and one deformed, which are degenerated at the phase transition point. Moreover, the vertical plane separating both deformed phases is also of first order: Two deformed minima with different deformations are degenerated and separated by a maximum at $\beta_{a}=0$. These two surfaces intersect in the line $(x=4 / 5, y=0)$, this is of second order for $0<y^{\prime} \leqslant 1$ and transforms to a first-order phase transition for $y^{\prime}>1$. The part of the line $(x=4 / 5$, $y=0,0<y^{\prime}<1$ ) corresponds to a flat surface (goes as $\beta_{a}^{4}$ ). At the point $\left(x=4 / 5, y=0, y^{\prime}=1\right)$ the energy surface is even flatter and goes as $\beta_{a}^{6}$. Finally, in the part of the line $\left(x \approx 4 / 5, y=0, y^{\prime}>1\right)$ three degenerated minima coexist (one spherical and two deformed ones). The point $x=4 / 5$, $y=0$, and $y^{\prime}=0$ corresponds to a tricritical point in the language of the Ginzburg-Landau theory for phase transitions.

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