

# Theoretical and Numerical Results on Modeling of Oceanic Turbulent Mixing Layers

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# Outline

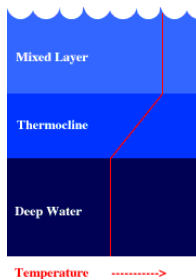
- 1 Introduction of the mean features of oceanic turbulent mixing layers.
- 2 Introduction of turbulent mixing-layer models, based on the **gradient Richardson number**.
- 3 Some results on the mathematical analysis of the proposed models.
- 4 Comparison with a more general model, based on the **Primitive Equations**.
- 5 Numerical tests.

# Oceanic Turbulent Mixing Layers

- The right computation of the **Sea Surface Temperature (SST)** is needed to predict different aspects related to oceanic biosystems and global climate changes.
- This problem shows its importance especially in **tropical regions**, where the high temperatures generate well-developed surface mixing layers.
- Many physical oceanographers started to study this problem during the *80's*, formulating the so-called "standard models".
- Turbulent mixing-layer models are usually vertical first-order closure models, and they do not include pressure gradients.

## Structure of Mixing Layer

- The wind-stress generates strong mixing phenomena in a layer located below the ocean surface: the **mixing layer**.
- The mixing layer is divided in two sections: the **mixed layer** and the **pycnocline**.
- Mixed layer: almost constant density.
- Pycnocline: remarkable gradient of density.



# Mathematical Formulation

- 1 Physically, vertical fluxes strongly dominate the mixing layer.  
⇒ We assume velocity and density horizontally homogeneous.
- 2 We set:

$$\mathbf{U} = (u(z, t), v(z, t), 0), \quad \rho = \rho(z, t).$$

- 3 We neglect the Coriolis force, that is a good approximation for equatorial regions.
- 4 In tropical seas:

$$\rho = \rho(\text{Temperature}) \longrightarrow (\text{state equation})$$

# Mathematical Formulation

The variables  $u, v, \rho$  satisfy the Reynolds-averaged equations:

$$\begin{cases} \partial_t u - a_1 \partial_{zz} u = -\partial_z \langle u' w' \rangle - D_1 \\ \partial_t v - a_1 \partial_{zz} v = -\partial_z \langle v' w' \rangle - D_2 \\ \partial_t \rho - a_2 \partial_{zz} \rho = -\partial_z \langle \rho' w' \rangle \end{cases} \quad (1)$$

- $(a_1, a_2) =$  laminar viscosity and diffusion
- $(D_1, D_2) = \nabla_{HP} =$  imposed horizontal pressure gradient

To close the problem, we use the concept of *eddy* viscosity and diffusion.

⇒ Application of a turbulence model based on the **gradient Richardson number**.

# Richardson number-based Model

We set:

$$-\langle u' w' \rangle = \nu_{T1} \partial_z u, \quad (2)$$

$$-\langle v' w' \rangle = \nu_{T1} \partial_z v, \quad (3)$$

$$-\langle \rho' w' \rangle = \nu_{T2} \partial_z \rho. \quad (4)$$

The eddy coefficients  $\nu_{T1}$  and  $\nu_{T2}$  are expressed as functions of the **gradient Richardson number**  $R$ , defined as:

$$R = -\frac{g}{\rho_r} \frac{\partial_z \rho}{(\partial_z u)^2 + (\partial_z v)^2}. \quad (5)$$

- Case  $R < 0$  ( $\partial_z \rho > 0$ ):

Unstable density configurations.

## Richardson number-based Model

## IBVP for the analysis of the Mixing Layer

$$\left\{ \begin{array}{l} \partial_t u - \partial_z(\nu_1 \partial_z u) = -D_1, \\ \partial_t v - \partial_z(\nu_1 \partial_z v) = -D_2, \\ \partial_t \rho - \partial_z(\nu_2 \partial_z \rho) = 0, \text{ for } t \geq 0 \text{ and } -h \leq z \leq 0, \\ u = u_b(t), v = v_b(t), \rho = \rho_b(t), \text{ for } z = -h, \\ \nu_1 \partial_z u = (\rho_a/\rho_r) V_x(t), \nu_1 \partial_z v = (\rho_a/\rho_r) V_y(t), \nu_2 \partial_z \rho = Q(t), \text{ for } z = 0, \\ u = u_0(z), v = v_0(z), \rho = \rho_0(z), \text{ for } t = 0. \end{array} \right. \quad (6)$$

$$\nu_1 = a_1 + \nu_{T1}, \quad \nu_2 = a_2 + \nu_{T2};$$

$$(V_x(t), V_y(t)) = C_D |\mathbf{U}^a(t)| \mathbf{U}^a(t), \quad (7)$$

$$\mathbf{U}^a(t) = (u_a(t), v_a(t)) = \text{air velocity}, \quad C_D (= 1.2 \cdot 10^{-3}) = \text{friction coef.} \quad (8)$$



A. C. Bennis, T. Chacón Rebollo, M. Gómez Mármol, R. Lewandowski,

*Numerical modelling of algebraic closure models of oceanic turbulent mixing layers*, (2010).



# Several Models for the Turbulent Coefficients

We set:

$$\nu_1 = f_1(R), \quad \nu_2 = f_2(R)$$

- **Pacanowski-Philander**

$$f_1(R) = a_1 + \frac{b_1}{(1 + 5R)^2}, \quad f_2(R) = a_2 + \frac{f_1(R)}{1 + 5R} \quad (9)$$

- **Gent**

$$f_1(R) = a_1 + \frac{b_1}{(1 + 10R)^2}, \quad f_2(R) = a_2 + \frac{b_2}{(1 + 5R)^3} \quad (10)$$

- **Non-standard model**

$$f_1(R) = a_1 + \frac{b_1}{(1 + 5R)^2}, \quad f_2(R) = a_2 + \frac{f_1(R)}{(1 + 5R)^2} \quad (11)$$

# Equilibrium Solutions

## Steady Problem:

$$\begin{cases} \partial_z(f_1(R^e)\partial_z u^e) = D_1 \\ \partial_z(f_1(R^e)\partial_z v^e) = D_2 \\ \partial_z(f_2(R^e)\partial_z \rho^e) = 0 \end{cases} \quad (12)$$

Integrating (12) with respect to  $z$ , we obtain:

$$\begin{cases} \partial_z u^e = (D_1 z + V_x^e \rho_a / \rho_r) / f_1(R^e) \\ \partial_z v^e = (D_2 z + V_y^e \rho_a / \rho_r) / f_1(R^e) \\ \partial_z \rho^e = Q^e / f_2(R^e) \end{cases} \quad (13)$$

By definition of  $R$ , we deduce the implicit equation for  $R^e$ :

$$R = G(z) \frac{[f_1(R)]^2}{f_2(R)}, \quad (14)$$

$$G(z) = -\frac{g}{\rho_r} \frac{Q^e}{(D_1 z + V_x^e \rho_a / \rho_r)^2 + (D_2 z + V_y^e \rho_a / \rho_r)^2}. \quad (15)$$

# Equilibrium Solutions

Integrating (13) with respect to  $z$ , we deduce the **equilibrium solutions**:

$$\left\{ \begin{array}{l} u^e(z) = u_b^e + D_1 \int_{-h}^z \frac{s}{f_1(R^e(s))} ds + \frac{V_x^e \rho_a}{\rho_0} \int_{-h}^z \frac{1}{f_1(R^e(s))} ds \\ v^e(z) = v_b^e + D_2 \int_{-h}^z \frac{s}{f_1(R^e(s))} ds + \frac{V_y^e \rho_a}{\rho_0} \int_{-h}^z \frac{1}{f_1(R^e(s))} ds \\ \rho^e(z) = \rho_b^e + Q^e \int_{-h}^z \frac{1}{f_2(R^e(s))} ds \end{array} \right. \quad (16)$$

- $\underline{D_1 = D_2 = 0}$

Linear profiles for velocity and density.

# Existence of Unsteady Solutions

## Theorem

If  $\mathbf{C} = (V_x, V_y, Q)(t) \in [L^2(0, T)]^3$ ,  $\mathbf{U}_b = (u_b, v_b, \rho_b)(t) \in [C^0(0, T)]^3$ ,  $\mathbf{U}_0 = (u_0, v_0, \rho_0)(z) \in [H^1(I)]^3$ , and these quantities are close enough to the corresponding quantities at the equilibrium, problem (6) with smoothly extended viscosities  $\nu_1, \nu_2$  admits a unique solution  $\mathbf{U}$  in an open neighborhood of the equilibrium  $\mathbf{U}^e$ , satisfying the estimate:

$$\|\mathbf{U} - \mathbf{U}^e\|_{L^2(0, T; [H^2(I)]^3)} + \|\partial_t(\mathbf{U} - \mathbf{U}^e)\|_{L^2(0, T; [L^2(I)]^3)} \leq$$

$$C(\|\mathbf{C} - \mathbf{C}^e\|_{L^2(0, T)} + \|\mathbf{U}_b - \mathbf{U}_b^e\|_{L^\infty(0, T)} + \|\mathbf{U}_0 - \mathbf{U}^e\|_{H^1(I)}) \quad (17)$$

where  $C$  is a positive constant independent of  $\mathbf{U}$ .

**Sketch of the Proof:** Inverse Function Theorem (Banach Spaces).

# Non-linear Stability of Continuous Equilibria

## Theorem

*Under the hypotheses of the existence theorem, and for small enough data, the equilibrium solutions of problem (6) with smoothly extended viscosities  $\nu_1, \nu_2$  are non-linearly exponentially asymptotically stable, in the sense that:*

$$\|\mathbf{U}'(t)\|_{L^2(I)} \leq e^{-\lambda t} \|\mathbf{U}'_0\|_{L^2(I)},$$

for some  $\lambda > 0$ , where  $\mathbf{U}' = \mathbf{U} - \mathbf{U}^e$ .

**Sketch of the Proof:** Standard Inequalities and Grönwall Lemma.

## Conservative Finite Difference Scheme

Assume that the interval  $[-h, 0]$  is divided into  $N$  subintervals of length  $\Delta z = h/N$ , with nodes  $z_i = -h + i\Delta z$ ,  $i = 0, \dots, N$ , and construct the FE space:

$$V_\Delta = \left\{ w_\Delta \in C^0([-h, 0]) \text{ s.t. } w_\Delta|_{|z_{i-1}, z_i|} \text{ is affine, } i = 1, \dots, N; w_\Delta(-h) = 0 \right\}. \quad (18)$$

- **Eq. for  $u$  (Semi-Implicit Method):** Obtain  $u_\Delta \in u_b + V_\Delta$  s.t.

$$\int_{-h}^0 \frac{u_\Delta^{n+1} - u_\Delta^n}{\Delta t} w_\Delta + \int_{-h}^0 f_1(R_\Delta^n) \partial_z u_\Delta^{n+1} \partial_z w_\Delta = \frac{\rho_a}{\rho_r} V_x w_\Delta(0) - D_1 \int_{-h}^0 w_\Delta. \quad (19)$$

- **FD Scheme for  $u$ :** For  $i = 1, \dots, N-1$ ,

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} - \frac{f_1(R_{i-1/2}^n) u_{i-1}^{n+1} - [f_1(R_{i-1/2}^n) + f_1(R_{i+1/2}^n)] u_i^{n+1} + f_1(R_{i+1/2}^n) u_{i+1}^{n+1}}{(\Delta z)^2} = -D_1, \quad (20)$$

$$f_1(R_{N-1/2}^n) \frac{u_N^{n+1} - u_{N-1}^{n+1}}{\Delta z} = \frac{\rho_a}{\rho_r} V_x. \quad (21)$$

# Analysis of the Numerical Scheme

## Hypothesis:

$$f_1, f_2 \in W^{1,\infty}(\mathbb{R}^3) \cap C^1(\mathbb{R}^3), \exists 0 < \nu \leq M \text{ s.t. } \nu \leq f_1(R), f_2(R) \leq M, \forall R \in \mathbb{R}. \quad (22)$$

## **Stability result:**

### Lemma

*Under Hypothesis (22), the discrete unsteady solution  $\mathbf{U}_\Delta$  (in its semi-implicit and implicit version) satisfy:*

$$\|\mathbf{U}_\Delta\|_{L^\infty(L^2)} + \|\mathbf{U}_\Delta\|_{L^2(H^1)} + \|\partial_t \mathbf{U}_\Delta\|_{L^2(H^{-1})} \leq C,$$

*where  $C$  is a positive constant that only depends on the data (and not on  $\Delta z$  and  $\Delta t$ ).*

## **Discrete maximum principle:**

### Lemma

*Under Hypothesis (22), if  $u_0$ ,  $u_b$  and  $V_x$  are positive, and  $D_1 \leq 0$ , then  $u_\Delta$  is positive in  $[-h, 0] \times [0, +\infty)$ .*

# Analysis of Discrete Equilibria

## Existence and uniqueness:

### Theorem

*Under Hypothesis (22), for small enough data, the steady version of the discrete problem admits a unique solution that satisfies:*

$$C_1 \leq |\partial_z u_\Delta|, |\partial_z v_\Delta|, |\partial_z \rho_\Delta| \leq C_2.$$

## Convergence and non-linear stability:

### Theorem

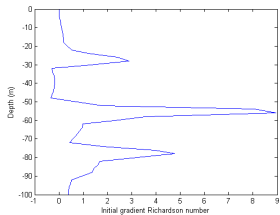
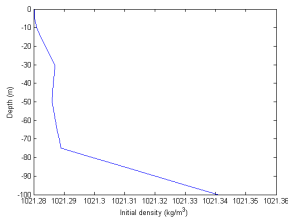
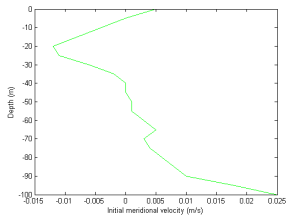
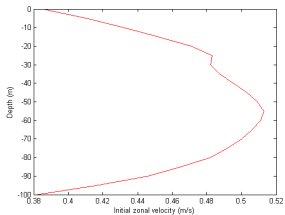
*Under Hypothesis (22), for small enough data:*

$$\{(u_\Delta, v_\Delta, \rho_\Delta)\}_{\Delta z > 0} \longrightarrow (u^e, v^e, \rho^e) \text{ in } [H^1(I)]^3,$$

$$\limsup_{n \rightarrow +\infty} \|\mathbf{U}_\Delta^n - \Pi_\Delta \mathbf{U}^e\|_{L^2(I)} \leq C \Delta z.$$

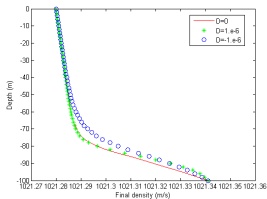
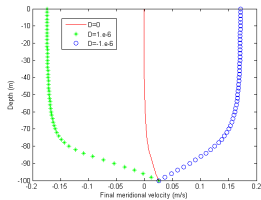
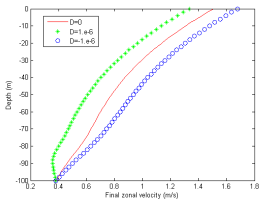


# Initial Conditions with Unstable Density Profile



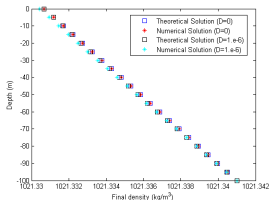
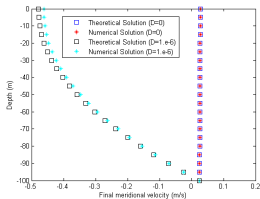
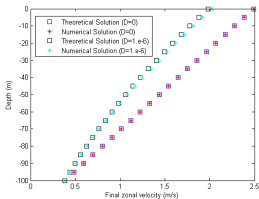
# Formation of the Mixing Layer

$$T = 48h.$$



# Equilibrium Solutions

$$T = 10000h.$$



# Primitive Equations of the Ocean

- The **Primitive Equations** govern the behavior of oceanic flows for large time and horizontal spatial scales.
- Physical basic model to analyze global climate changes and oceanic biosystems.
- Reduced formulation  $\rightarrow$  PDEs for horizontal velocity, surface pressure and density.  
(**Boussinesq Equations + Hydrostatic Approximation**)

## Setting of the Model

- 1 We consider the rigid-surface domain of the flow:

$$\omega = (0, L), L > 0.$$

- 2 We define the 2D domain of the flow:

$$\Omega = \{(x, z) \in \mathbb{R}^2 \text{ s.t. } x \in \omega, -h < z < 0\}.$$

- 3 We set:

$$\mathbf{U} = (u(x, z, t), w(x, z, t)), \rho = \rho(x, z, t), p = p(x, z, t).$$

- 4 We neglect the Coriolis force.

The anisotropy of the domain ( $L \gg h$ ) permits to apply the hydrostatic approximation:

$$\partial_z p = -\frac{\rho}{\rho_r} g.$$

## Setting of the Model

The set of 2D Primitive Equations governing the mixing layer becomes :

$$\left\{ \begin{array}{l} \nabla \cdot \mathbf{U} = 0, \\ \partial_t u + (\mathbf{U} \cdot \nabla)u - a_1 \Delta u + \partial_x p = -\nabla \cdot \langle \mathbf{U}' u' \rangle, \\ \partial_z p = -\frac{\rho}{\rho_r} g, \\ \partial_t \rho + (\mathbf{U} \cdot \nabla)\rho - a_2 \Delta \rho = -\nabla \cdot \langle \mathbf{U}' \rho' \rangle. \end{array} \right. \quad (23)$$

We set:

$$-\langle \mathbf{U}' u' \rangle = (\nu_h^t \partial_x u, \nu_v^t \partial_z u), \quad (24)$$

$$-\langle \mathbf{U}' \rho' \rangle = (k_h^t \partial_x \rho, k_v^t \partial_z \rho), \quad (25)$$

where:

$$(i) \quad \nu_h^t = (C_s \Delta x)^2 |\partial_x u|, \quad k_h^t = \frac{a_2}{a_1} \nu_h^t \quad (\text{Smagorinsky}),$$

$$(ii) \quad \nu_v^t = \frac{b_1}{(1+5R)^2}, \quad k_v^t = \frac{a_1}{(1+5R)^2} + \frac{\nu_v^t}{(1+5R)^2}, \quad R = -\frac{g}{\rho_r} \frac{\partial_z \rho}{(\partial_z u)^2} \quad (\text{Richardson}).$$

# Reduced Formulation

- $\partial\Omega =$  boundary of  $\Omega = \Gamma_b \cup \Gamma_s \cup \Gamma_{l1} \cup \Gamma_{l2}$ .
- Vertical integration of the **hydrostatic pressure**:

$$\int_z^0 \partial_s p = -\frac{g}{\rho_r} \int_z^0 \rho \Rightarrow \boxed{p(x, z, t) = p_s(x, t) + \frac{g}{\rho_r} \int_z^0 \rho}$$

$$\partial_x p = \partial_x p_s + \frac{g}{\rho_r} \partial_x \int_z^0 \rho = \nabla_H(\text{Surf. Pres.}) + \text{Baroclinic Contr.}$$

# Reduced Formulation

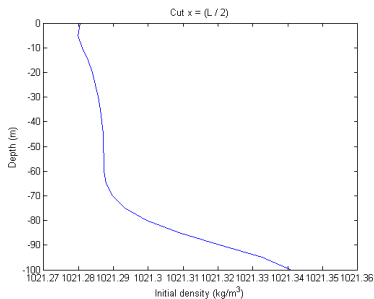
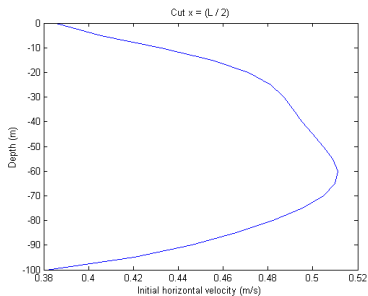
## IBVP for the analysis of the Mixing Layer

$$\left\{ \begin{array}{ll}
 (a) \partial_t u + (\mathbf{U} \cdot \nabla) u - \partial_x (\nu_h \partial_x u) - \partial_z (\nu_v \partial_z u) + \partial_x p_s + (g/\rho_r) \partial_x \int_z^0 \rho = 0 & \text{in } \Omega \times ]0, T[, \\
 (b) \partial_t \rho + (\mathbf{U} \cdot \nabla) \rho - \partial_x (k_h \partial_x \rho) - \partial_z (k_v \partial_z \rho) = 0 & \text{in } \Omega \times ]0, T[, \\
 (c) \partial_z w = -\partial_x u & \text{in } \Omega \times ]0, T[, \\
 (d) u|_{\Gamma_b} = u_b, \quad \rho|_{\Gamma_b} = \rho_b & \text{in } [0, T], \\
 (e) w|_{\Gamma_b} = w|_{\Gamma_s} = 0 & \text{in } [0, T], \\
 (f) u|_{\Gamma_{\ell 1}} = u|_{\Gamma_{\ell 2}}, \quad \rho|_{\Gamma_{\ell 1}} = \rho|_{\Gamma_{\ell 2}} & \text{in } [0, T], \\
 (g) \nu_v \partial_z u|_{\Gamma_s} = (\rho_a/\rho_r) V_x, \quad k_v \partial_z \rho|_{\Gamma_s} = Q & \text{in } [0, T], \\
 (h) u(0) = \hat{u}_0, \quad \rho(0) = \hat{\rho}_0 & \text{in } \Omega.
 \end{array} \right. \quad (26)$$

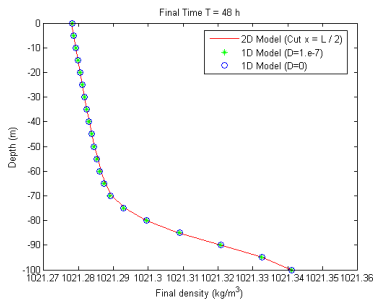
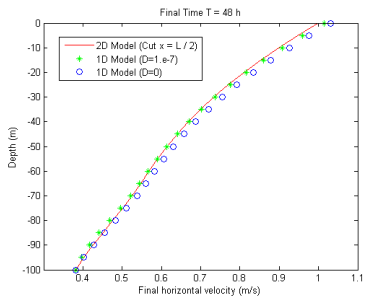
- 1 Spatial discretization: **Galerkin FEM.**
- 2 Temporal discretization: **Semi-Implicit Euler Scheme.**



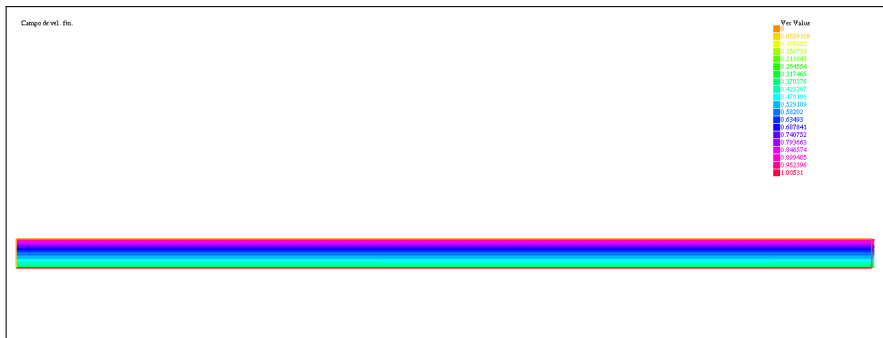
# Initial Velocity and Density Profiles



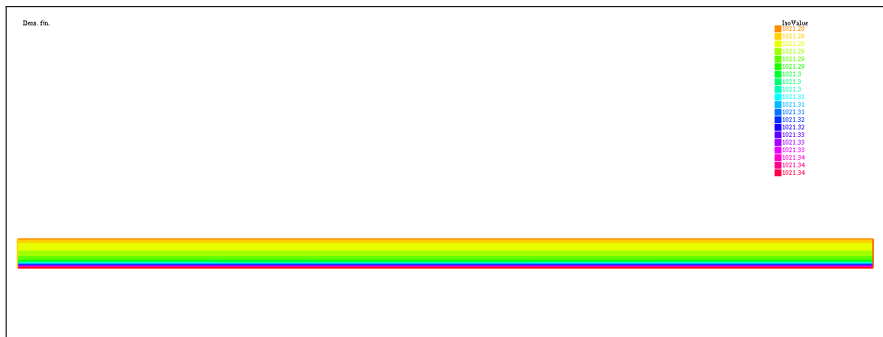
# Comparison between Models 2D and 1D



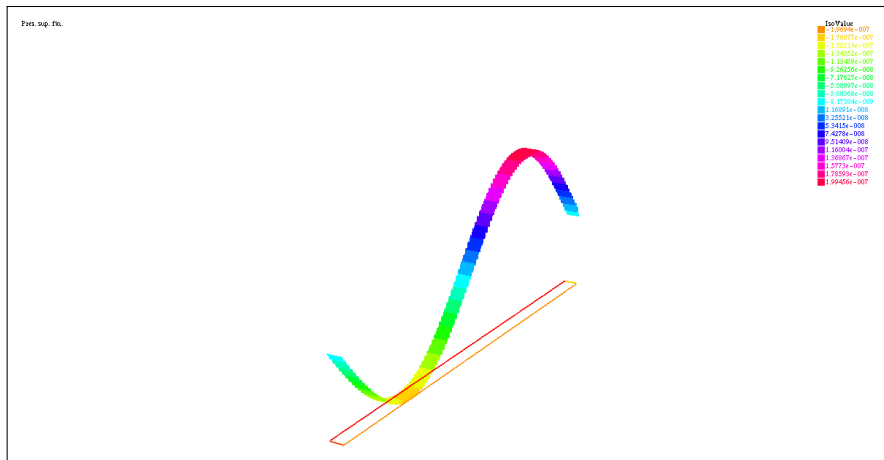
# Final Fluid Flow 2D



# Final Density 2D



# Final Surface Pressure



## Observations:

- The 2D model justifies the assumptions leading to the 1D model (lower computational cost).
- The introduction of an imposed pressure gradient in the 1D model permits to improve the accuracy in the computation of the velocity, if the initial conditions are not 1D.

## References:



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