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1 **SIMPLIFIED MODEL TO CORRECT THERMOPILE PYRANOMETER SOLAR RADIATION**  
2 **MEASUREMENTS FOR PHOTOVOLTAIC MODULE YIELD ESTIMATION**

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11 **Abstract**

12 This article presents and evaluates the performance of a simplified model to generate 10-min  
13 global horizontal synthetic solar radiation data that would correspond to the measurements of  
14 a calibrated photovoltaic monocrystalline cell. The model, which only requires global horizontal  
15 solar radiation data measured with a thermopile pyranometer as input, is based on the  
16 characterization of the relation between the data measured with a thermopile pyranometer and  
17 a calibrated cell as a function of the sky condition and the solar elevation. We have used an  
18 extensive solar radiation database for the location of Seville (Spain) for the training of the model  
19 that has been tested in Seville and Lancaster (USA), showing satisfactory results and suggesting  
20 a global applicability with no local adaptation or calibration requirement.

21 The model shows the best results for high levels of solar radiation and solar elevations and  
22 decreases its performance on days with high levels of diffuse irradiation and for very low solar  
23 elevation angles. We obtain a daily RMSD between measured and synthetic data of 1.9% in  
24 Seville and 5.2% in Lancaster. The frequency distribution of the synthetic datasets shows a KSI  
25 of 3.7 W/m<sup>2</sup> in Seville and 8.6 W/m<sup>2</sup> in Lancaster. We also evaluate the ramp rates of measured  
26 and synthetic sets through the KSI of the measured and synthetic ramp rates sets, obtaining 0.11  
27 W/m<sup>2</sup>·min in Seville and 0.20 W/m<sup>2</sup>·min in Lancaster.

28 **Keywords**

29 Photovoltaic yield, calibrated solar cell, pyranometer.

30 **1 Introduction**

31

32 Photovoltaic (PV) modules have a practically identical spectral response, time, temperature  
33 coefficient and angular response to a calibrated solar cell of the same technology and  
34 encapsulation. For this reason, if radiation measurements are obtained by means of a calibrated  
35 photovoltaic cell of the same technology and encapsulation as the photovoltaic modules of the  
36 installation, most of the uncertainties in the determination of the electrical production of the

37 photovoltaic installation are already included. Meydbray et al., [1-2] compare the use of solar  
 38 reference cell and thermopile for PV applications, and point out that solar reference cells are  
 39 especially useful for precise characterization of the PV performance, allowing a better detection  
 40 of changes in PV system performance with time and shorter time assessment of the PV operating  
 41 efficiency. Table 1 summarises the comparison of the use of solar reference cell and thermopile  
 42 pyranometers for PV applications proposed by Meydbray et al [2].

43 **Table 1.** Cell-pyranometer comparison made by Meydbray et al [2] for PV applications.

|                         | <b>Reference Cell</b>                        | <b>Thermopile pyranometer</b>  |
|-------------------------|--|--|
| Spectral Response       | Can be made to closely match solar panel     | Broadband response needs to be corrected   |
| Angle of incidence      | Can be made to closely match solar panel     | Response to all angles   |
| Temperature response    | Temperature response is similar to PV system | Are designed to minimize sensitivity to temperature. Not corrected for temperature |
| Time response           | < milliseconds; matched to PV response       | Up to 30 seconds, can be problematic for measuring PV performance                  |
| Other issues            |  | Emission to cold sky and transients in ambient temperature affects output          |
| International standards | IEC 60904                                    | ISO 9847, ISO 9845, ISO 9846   |

44

45 For PV applications, Dunn et al., [3] analysed the expanded uncertainties in the measurements  
 46 of the irradiance made in the plane of array throughout the course of a representative day with  
 47 a thermopile pyranometer and a PV reference device. They conclude that during most of the  
 48 day, uncertainties are in the order of  $\pm 5\%$  for a pyranometer, and  $\pm 2.4\%$  for a calibrated cell,  
 49 both stated with 95% confidence intervals. So calibrated cells provide superior irradiance  
 50 measurements for PV power plant monitoring applications. Haeberlin et al., [4] compare the use  
 51 of a pyranometer and a calibrated silicon solar cell and reach similar conclusions: it is preferable  
 52 to use a calibrated Si-cell (of the same type as the cells in the PV array) as a reference device of  
 53 the irradiance measurements for PV plant monitoring than a pyranometer.

54 The PV module performance is generally evaluated by manufacturers under standard test  
 55 conditions (STC), which refer to 25°C module temperature, 1000 W/m<sup>2</sup> of incident solar  
 56 irradiance on the PV module plane with 1.5 solar spectrum air mass (AM) as reference spectrum  
 57 (IEC 60904-3, 2016) [5]. Nevertheless, in real conditions the PV module temperature, solar  
 58 irradiance with incident angle and solar spectrum differ from STC.

59 Incident solar global irradiance that reaches the PV module is affected by the distribution of its  
60 solar spectrum. This solar spectrum depends on cloud cover, AM, precipitable water (PW) and  
61 aerosol optical depth (AOD) [6]. The short-circuit current is the main parameter affected by the  
62 distribution of the solar spectrum, but in some technologies efficiency, maximum power and fill  
63 factor are also influenced. Polo et al, [7] analyse the use of reference modules as irradiance  
64 sensor for monitoring and modelling rooftop PV systems for different PV technologies with  
65 different spectral responses. If such affection is neglected and only the broadband irradiance is  
66 used for PV-module performance modelling, then errors of up to 10% can be introduced in  
67 extreme conditions [8].

68 Therefore, a spectral correction shall be used in order to adjust the incident solar irradiance and,  
69 hence, improve the PV module performance modelling [9]. This spectral correction depends on  
70 the PV module technology. Polo et al., [10] give the spectral factor for seven photovoltaic  
71 technologies and 124 sites. They found that the annual spectral factor for crystalline silicon  
72 technologies is rather homogenous worldwide with maxima spectral losses and gains of  $\approx 3\%$   
73 and  $\approx 1\%$ , respectively. On the contrary, the spectral factor for thin film devices displays a higher  
74 spatial variability. Nuñez et al., [11] proposed a spectral matching ratio for multijunction cells  
75 within a concentrating photovoltaic module. The Sandia Array Performance Model applies a  
76 fourth-order polynomial correction based on AM [12]. M. Lee et al., [13] included in their model  
77 the influence of AM and PW in a similar function. Theristis et al., [14] developed a model  
78 including AM, PW and AOD to improve concentrating photovoltaic system performance  
79 modelling. Another option is to use direct measurements of spectral radiation, but the use of  
80 spectroradiometers is not yet widespread and an adequate validation is required [15].

81 Moreover, in many cases the PV module structure does not have two-axis tracking.  
82 Consequently, the incident solar global irradiance that reaches the PV module is affected by the  
83 solar angle of incidence (AOI). Angular losses in PV modules can introduce differences in the  
84 short circuit current under STC of up to 3.5% under global normal irradiance conditions with  
85 horizontal orientation compared with a device without losses due to angular effects [16]. King  
86 et al., [17] suggest the use of a 5<sup>th</sup> order polynomial function to represent the angular optical  
87 losses on the short circuit current. Martin et al., [18] formulated similar functions. Instead, given  
88 the importance of these effects on the performance of the photovoltaic module, manufacturers  
89 test their PV modules according to IEC standard 61853-2:2016 [19] where the effect of the angle  
90 of incidence and the spectral responsivity on the output power of the photovoltaic module is  
91 measured. The most used software for the design of photovoltaic installations has implemented  
92 a model to take into account the angular losses. PVSyst software [20] has implemented the  
93 model developed by Souka and Safat and adopted by the American Society of Heating,  
94 Refrigeration, and Air Conditioning (ASHRAE) [17]. Plag F et al., [21] related the spectral and  
95 angular effect showing that the spectral effect depends on the incident angle too.

96 An alternative to these methods to link the silicon photovoltaic calibrated cell measurement  
97 with the measurements made by a thermopile pyranometer are specific simplified models to  
98 relate the global solar radiation measured by both devices. J. J. Michalsky et al., [22] propose a  
99 table of correction factors depending on the clearness index and the brightness index. It requires  
100 the knowledge of diffuse and direct radiation from the site. King & Myers [23] correct the  
101 response of the PV device as a function of the solar spectrum, AOI and temperature. This

102 corrected response allows us to obtain an improvement in the estimation of the total irradiance.  
103 The method also requires diffuse and direct data among the calculation of functions related to  
104 the absolute air mass, the AOI and a temperature coefficient. The main drawback in the  
105 implementation of the described methods is the requirement of rarely available measurements  
106 such as AOD, PW, diffuse and direct irradiance for the location under study.

107 The purpose of this work is the development of a simplified model for estimating the solar global  
108 radiation that a calibrated monocrystalline silicon cell would measure using only thermopile  
109 pyranometer measurements as input. This model could be used as a correction factor that would  
110 allow us to characterize the PV module performance from thermopile pyranometer radiation  
111 data.

112 Simplicity is the main advantage of this model because it depends only on the global irradiation  
113 data measured by a thermopile pyranometer avoiding the need to use more complex variables  
114 which are generally more difficult to obtain. The model has been developed for one location  
115 (Seville) and tested in the same location (Seville) and a different one (Lancaster) without any  
116 local adaptation showing satisfactory results.

117 The paper is presented as follows: Section 2 presents the database used for the training and  
118 testing of the model. In Section 3 we explain step by step the development of the model. In  
119 Section 4 we perform the result analysis of the model in two locations. Conclusions are then  
120 made in Section 5.

## 121 **2 Meteorological database**

122 In this work, an extensive database is used for training the method proposed (Table 2). This  
123 database is composed of 10-min averages values of GHI recorded during 42 consecutive months  
124 from July 2012 to December 2015 for the location of Seville (Spain). The measurements were  
125 taken with a sampling and storage time resolution of 5 s. A secondary standard pyranometer  
126 Kipp & Zonen CMP21 and an Atersa calibrated monocrystalline silicon PV cell measured the GHI.  
127 The devices used for the design and testing of the methodology are located at the  
128 meteorological station of the Group of Thermodynamics and Renewable Energy of the  
129 University of Seville and have been periodically calibrated, according to the recommendations  
130 from the instrument manufacturers. Data used in this work have been subjected to quality-  
131 control procedures [24] following the BSRN recommendations [25]. Only 1% of the data has  
132 been filled for the entire database. Data recorded at sun altitude lower than 2° have not been  
133 used in this study.

134 **Table 2.** Location selected for the method training.

|         | Latitude<br>(°N) | Longitude<br>(°W) | Altitude (m) | Köppen-Geiger<br>Climate | Period    |
|---------|------------------|-------------------|--------------|--------------------------|-----------|
| Seville | 37.4             | 6.0               | 12           | Csa                      | 2012-2015 |

135

136 In addition, the model has been tested in two locations. We use data for one entire year for the  
137 location of Seville and for the location of Lancaster, USA (Table 3). GHI data from Lancaster were  
138 measured with a secondary standard pyranometer Kipp & Zonen CMP21 and an Atersa  
139 calibrated monocrystalline silicon PV cell, and has been subjected to quality control procedures

140 [24] following the BSRN recommendations [25]. According to the Köppen-Geiger climate  
 141 classification system [26], Seville’s climate is classified as Mediterranean with hot summers and  
 142 Lancaster’s climate is classified as Mediterranean with mild summers. When performing the  
 143 quality control procedure of Lancaster database, we identify a period of 12 consecutive days  
 144 with irregularities in the measurements in October. This period is not computed in the  
 145 performance evaluation of the algorithm.

146 We use 10-min averaged data because high-quality data for the testing of the method was  
 147 available in that time step, but the method can be used in any time resolution greater than 1-  
 148 min.

149 **Table 3.** Location selected for testing the method.

|           | Latitude<br>(°N) | Longitude<br>(°W) | Altitude (m) | Köppen-Geiger<br>Climate | Period |
|-----------|------------------|-------------------|--------------|--------------------------|--------|
| Seville   | 37.4             | 6.0               | 12           | Csa                      | 2016   |
| Lancaster | 34.6             | 118.3             | 812          | Csb                      | 2016   |

150

### 151 **3 Methodology**

152 In this section we describe the methodology implemented for the synthetic generation of  
 153 reference PV cell solar radiation data ( $G_{cell}^{synth}$ ) from pyranometer measurements ( $G_{pyr}$ ). The  
 154 model has been developed for 10-min time resolution and its only input is the  $G_{pyr}$ . The rest of  
 155 the used parameters are theoretically estimated from the geographic position of the location  
 156 under study (latitude and longitude) and the record time of the measurements. The method can  
 157 be described in a sequence of 5 steps.

#### 158 **3.1 Step 1: Data clustering**

159 In the first step, we cluster the data from pyranometer and PV cell measurements as a function  
 160 of the clearness index  $k_t$  and the solar elevation,  $\alpha$ . To characterize the type of day, other indices  
 161 such as the Perez clearness index ( $\epsilon$ ), Perraudau's brightness ( $I_N$ ), sky ratio index ( $SR$ ) [27] or  
 162 illuminance fluctuation frequency index [28] could be used, but they require the knowledge of  
 163 more variables such as diffuse and/or beam normal irradiance. Previous approaches have shown  
 164 that using only one radiometric variable, different sky conditions can be identified [29]. We  
 165 propose to cluster the data into 9 groups in terms of the clearness index, dividing the datasets  
 166 into intervals of 0.1 from 0 to 0.8. Values greater than 0.8 have been clustered into the same  
 167 group. For the solar elevation we chose 7 groups dividing the dataset into intervals of 5° from  
 168 20° to 40° and intervals of 10° from 40° to 60°. Data for solar elevations lower than 20° are  
 169 clustered in the same group as well as data for solar elevations greater than 60°. We group the  
 170 solar data into a total of 63 clusters.

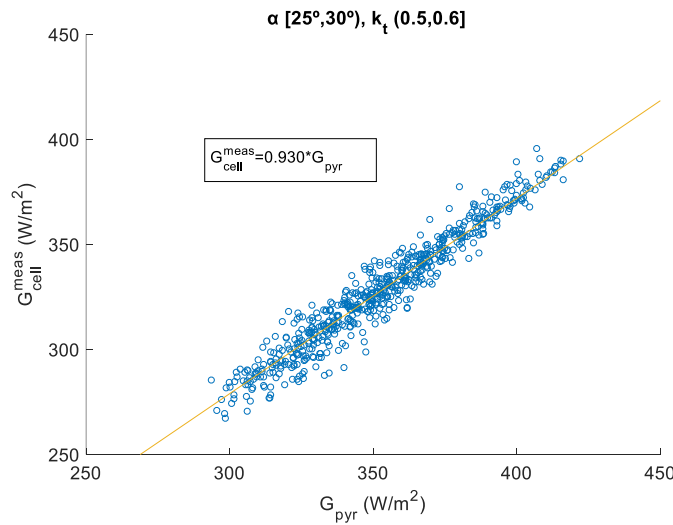
#### 171 **3.2 Step 2: First regression**

172 In the second step, we use a least squares procedure to perform a linear regression fit to the  
 173 cloud point obtained, when comparing the solar radiation values measured with the  
 174 pyranometer ( $G_{pyr}$ ) with the solar radiation values measured with the calibrated solar cell  
 175 ( $G_{cell}^{meas}$ ), obtaining a function dependant on the solar elevation ( $\alpha$ ) and sky condition defined by

176 the clearness index ( $k_t$ ). See equation 1. In figure 1 we present an example of the cloud points  
 177 and the linear fit for the cluster interval corresponding to solar elevations lower than 30° and  
 178 greater than 25°, and clearness index lower than 0.6 and greater than 0.5. In table 4 we present  
 179 the first regression coefficient  $RC(\alpha, k_t)$  obtained for each cluster from the training dataset.

$$180 \quad RC(\alpha, k_t) = \frac{G_{cell}^{meas}}{G_{pyr}} \quad (1)$$

181 We can relate the first regression coefficient ( $RC$ ) to the spectral and angular losses related to  
 182 the measurements of solar radiation with silicon monocrystalline cells in comparison to solar  
 183 radiation data measured with a pyranometer, since those losses show a strong dependency on  
 184 the solar elevation and sky condition.



185  
 186

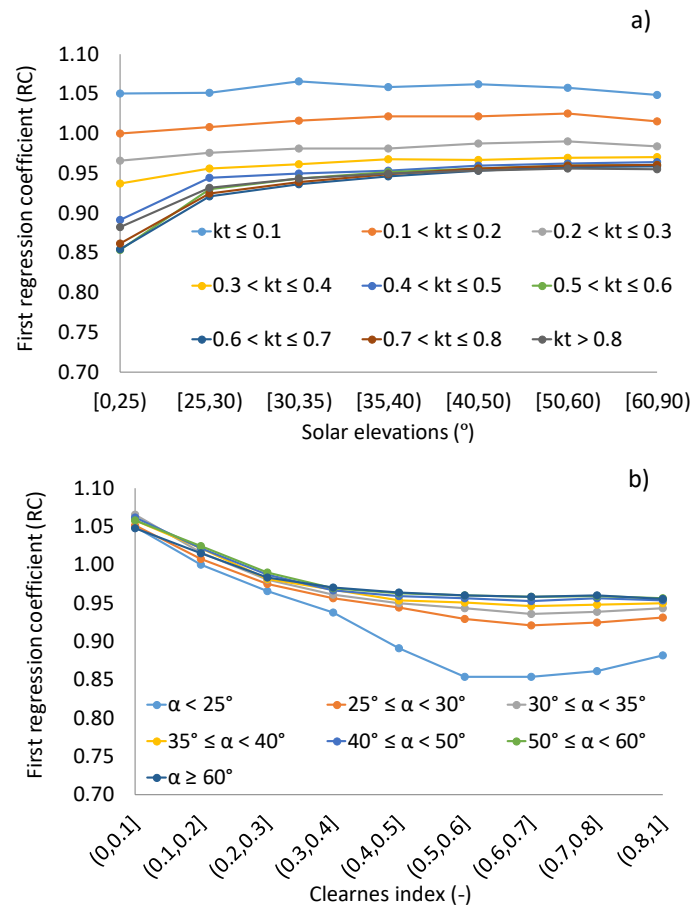
187 **Figure 1.** Cloud points and first linear regression fit for solar elevations between 25° and 30° and  
 188 clearness indexes between 0.5 and 0.6 for the location of Seville.

189 **Table 4.** First regression coefficient ( $RC$ ) for each cluster for the location of Seville. We shaded the  
 190 result for the data exposed in figure 1.

| 1 <sup>st</sup> Regression coefficient $RC(\alpha, k_t)$ | $\alpha < 25^\circ$ | $25^\circ \leq \alpha < 30^\circ$ | $30^\circ \leq \alpha < 35^\circ$ | $35^\circ \leq \alpha < 40^\circ$ | $40^\circ \leq \alpha < 50^\circ$ | $50^\circ \leq \alpha < 60^\circ$ | $\alpha \geq 60^\circ$ |
|--|---------------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|------------------------|
| $k_t \leq 0.1$   | 1.050               | 1.052                             | 1.065                             | 1.059                             | 1.062                             | 1.058                             | 1.049                  |
| $0.1 < k_t \leq 0.2$                                     | 1.000               | 1.008                             | 1.017                             | 1.022                             | 1.022                             | 1.025                             | 1.016                  |
| $0.2 < k_t \leq 0.3$                                     | 0.966               | 0.976                             | 0.981                             | 0.981                             | 0.987                             | 0.990                             | 0.984                  |
| $0.3 < k_t \leq 0.4$                                     | 0.938               | 0.957                             | 0.961                             | 0.967                             | 0.967                             | 0.970                             | 0.970                  |
| $0.4 < k_t \leq 0.5$                                     | 0.891               | 0.944                             | 0.950                             | 0.954                             | 0.960                             | 0.963                             | 0.964                  |
| $0.5 < k_t \leq 0.6$                                     | 0.854               | 0.930                             | 0.944                             | 0.951                             | 0.956                             | 0.960                             | 0.960                  |
| $0.6 < k_t \leq 0.7$                                     | 0.854               | 0.921                             | 0.936                             | 0.946                             | 0.953                             | 0.958                             | 0.959                  |
| $0.7 < k_t \leq 0.8$                                     | 0.862               | 0.925                             | 0.939                             | 0.949                             | 0.956                             | 0.960                             | 0.960                  |
| $k_t > 0.8$  | 0.882               | 0.932                             | 0.944                             | 0.950                             | 0.954                             | 0.956                             | 0.955                  |

191

192 In figure 2 we present the first regression coefficient ( $RC$ ) for all the sky conditions as a function of  
 193 the solar elevation selected intervals (a) and the first regression coefficient ( $RC$ ) vs the solar  
 194 elevations as a function of the sky condition (b)



195

196

197 **Figure 2.** First regression coefficient ( $RC$ ) versus all the selected intervals of solar elevations as a  
 198 function of the clearness indexes (a) for the location of Seville. First regression coefficient ( $RC$ )  
 199 versus the clearness indexes for all the selected intervals of solar elevations as a function of all  
 200 the selected intervals of solar elevations (b) for the location of Seville.

201 From table 4 and figure 2, we can observe that the first regression coefficient ( $RC$ ) shows a  
 202 different tendency for solar elevations lower than  $25^\circ$  and clearness indexes greater than 0.4.  
 203 For  $k_t$  values lower than 0.4 and solar elevations lower than  $25^\circ$ , we can observe in both figures  
 204 a, and b, that  $RC$  shows a change in its performance with respect to the rest of the  $k_t$  and  $\alpha$   
 205 values.

206 This can be explained by the greater impact of the refraction effects for low solar elevations of  
 207 the solar radiation on the PV reference cell in comparison to the pyranometer. Reference cell  
 208 errors are particularly large at sunset and sunrise (up to  $50 \text{ W/m}^2$ ) according to the Hukseflux  
 209 Thermal Sensors report [30]. The greater the clearness index, the greater the direct component  
 210 amount on the total global radiation which in turn is strongly affected by the refraction effects  
 211 due to low solar elevations and horizon distortions. Moreover, the PV reference cells present a  
 212 greater angular dependence.



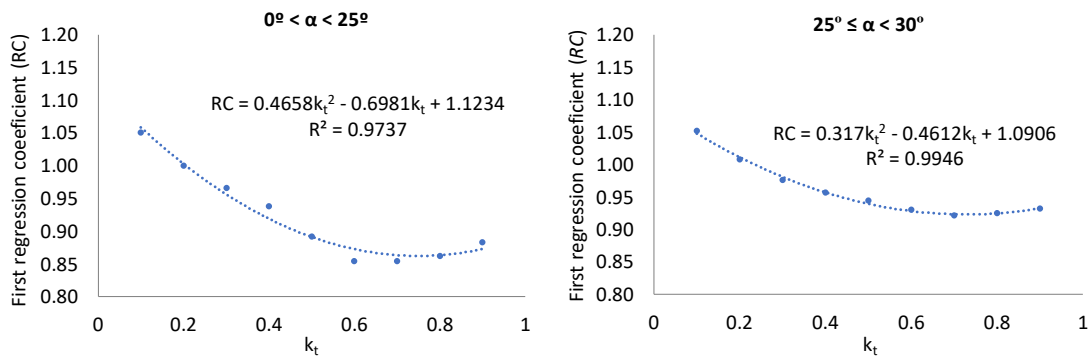
213

### 3.3 Step 3: Second regression

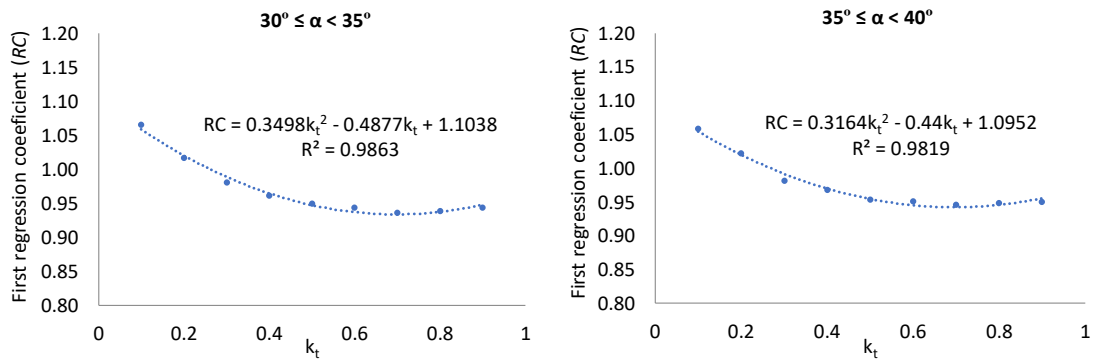
214 In the third step, we run again a least squares procedure but in this case we perform a second  
 215 order polynomial fit of the first regression coefficient ( $RC$ ) as a function of the clearness index  
 216 ( $k_t$ ). The calculation is performed separately for each solar elevation selected interval following  
 217 equation 2. From this step, we obtain the three functions ( $b(\alpha), c(\alpha), d(\alpha)$ ) dependant on the  
 218 solar elevation. In figure 3 we represent the polynomial fit of the first regression coefficient ( $RC$ )  
 219 as a function of the clearness index ( $k_t$ ) for each solar elevation interval.

220 
$$RC(\alpha, k_t) = b(\alpha) \cdot k_t^2 + c(\alpha) \cdot k_t + d(\alpha) \tag{2}$$

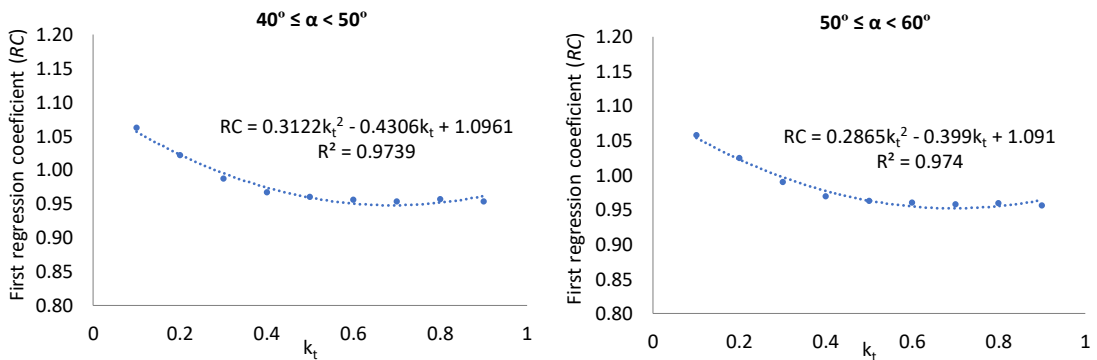
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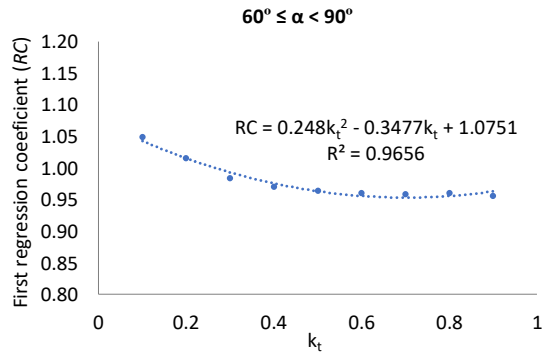


222



223





224

225 **Figure 3.** Polynomial fit of the first regression coefficient ( $RC$ ) as a function of the clearness index  
 226 ( $k_t$ ) for each solar elevation interval for the location of Seville

227 The coefficient of determination ranges between 0.974 and 0.995 in the solar elevation selected  
 228 intervals showing a high accuracy on the fit. In table 5 we present the functions obtained  
 229 applying equation 2 for each solar elevation interval

230 **Table 5.** Second regression coefficients, ( $b(\alpha)$ ,  $c(\alpha)$ ,  $d(\alpha)$ ) for each solar elevation interval for  
 231 the location of Seville.

| $\alpha$ ( $^\circ$ ) | $b(\alpha)$ | $c(\alpha)$ | $d(\alpha)$ |
|-----------------------|-------------|-------------|-------------|
| < 25                  | 0.466       | -0.698      | 1.123       |
| 25 - 30               | 0.317       | -0.461      | 1.091       |
| 30 - 35               | 0.350       | -0.488      | 1.104       |
| 35 - 40               | 0.316       | -0.440      | 1.095       |
| 40 - 50               | 0.312       | -0.431      | 1.096       |
| 50 - 60               | 0.287       | -0.399      | 1.091       |
| > 60                  | 0.248       | -0.348      | 1.075       |

232

### 233 3.4 Step 4: Third regression

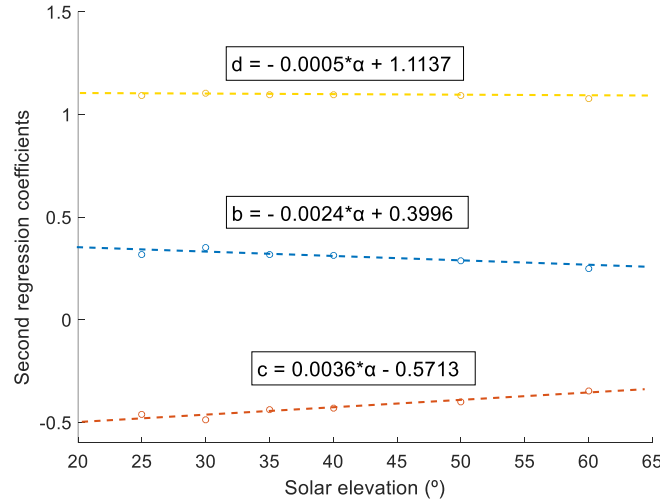
234 In this step, we run again a least squares procedure to perform a linear regression fit, but in this  
 235 case we fit the second regression coefficients, ( $b(\alpha)$ ,  $c(\alpha)$ ,  $d(\alpha)$ ) obtained in step 3 (Table 5) as  
 236 a function of the solar elevation defined intervals following equations 3-5.

$$237 \quad b(\alpha) = b_1 \cdot \alpha + b_2 \quad (3)$$

$$238 \quad c(\alpha) = c_1 \cdot \alpha + c_2 \quad (4)$$

$$239 \quad d(\alpha) = d_1 \cdot \alpha + d_2 \quad (5)$$

240 We run the third regression fit only for solar elevations greater than  $25^\circ$ . In figure 3 we present  
 241 the third regression linear fit of the second regression coefficients, ( $b(\alpha)$ ,  $c(\alpha)$ ,  $d(\alpha)$ ) obtained  
 242 in step 3 as a function of the solar elevation (greater than  $25^\circ$ ).



243

244 **Figure 4.** Linear fit of the second regression coefficients ( $b(\alpha)$ ,  $c(\alpha)$ ,  $d(\alpha)$ ) as a function of the  
 245 solar elevation for the location of Seville.

246

247

### 3.5 Step 5: Hyperbolic tangent fit

248 When substituting ( $b(\alpha)$ ,  $c(\alpha)$ ,  $d(\alpha)$ ) from equation 3-5 into equation 2 separating calculations  
 249 for solar elevations lower and greater than  $25^\circ$ , we obtain equations 6 and 7 respectively.

250 
$$RC = 0.466 \cdot k_t^2 - 0.698 \cdot k_t + 1.123 \quad \text{if } \alpha < 25^\circ \quad (6)$$

251 
$$RC = (-0.0024 \cdot \alpha + 0.3996) \cdot k_t^2 + (0.0036 \cdot \alpha - 0.5713) \cdot k_t + (-0.0005 \cdot \alpha +$$
  
 252 
$$1.1137) \quad \text{if } \alpha \geq 25^\circ \quad (7)$$

253 The model could be used from its corresponding equation (6-7) according to the solar elevation,  
 254 but it would lead to a discontinuity at the solar elevation  $\alpha=25^\circ$ . We use the hyperbolic tangent  
 255 function to join equations 6-7 in a simple equation (see equation 8) obtaining thus a continuous  
 256 function.

257 
$$RC(\alpha, k_t) = (0.5 \cdot \{((0.466 \cdot k_t^2 - 0.698 \cdot k_t + 1.123) \cdot (1 - \tanh(\beta \cdot (\alpha - 25)))) +$$
  
 258 
$$((-0.0024 \cdot \alpha + 0.3996) \cdot k_t^2 + (0.0036 \cdot \alpha - 0.5713) \cdot k_t + (-0.0005 \cdot \alpha + 1.1137)) \cdot$$
  
 259 
$$(1 + \tanh(\beta \cdot (\alpha - 25)))\}) \quad (8)$$

260  $\beta$  is a parameter that modifies the connection between equations 6 and 7. For a high  $\beta$  value,  
 261 the connection is more abrupt. For a low  $\beta$  value, the connection is smoother, but the data for  
 262 solar elevations different to  $25^\circ$  change significantly. We select a  $\beta=0.18$  by minimizing the  
 263 deviations between the reference PV cell measured and synthetic solar radiation sets from the  
 264 Seville training database. Any value between 0.1 and 0.2 can be applied and no significant  
 265 variation would be obtained. We recommend using  $\beta=0.18$  for any location where the model  
 266 may be applied.

267 By substituting equation 8 in equation 1 we can obtain the synthetic reference PV cell solar  
 268 radiation data  $G_{cell}^{synth}$  from thermopile pyranometer measurements  $G_{pyr}$  following equation 9

$$\begin{aligned}
269 \quad G_{cell}^{synth} &= (0.5 \cdot \{(0.466 \cdot k_t^2 - 0.698 \cdot k_t + 1.123) \cdot (1 - \tanh(0.18 \cdot (\alpha - 25))) + \\
270 \quad &((-0.0024 \cdot \alpha + 0.3996) \cdot k_t^2 + (0.0036 \cdot \alpha - 0.5713) \cdot k_t + (-0.0005 \cdot \alpha + 1.1137)) \cdot \\
271 \quad &(1 + \tanh(0.18 \cdot (\alpha - 25)))\}) \cdot G_{pyr} \quad (9)
\end{aligned}$$

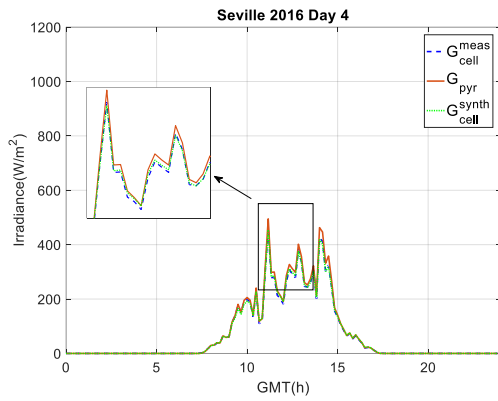
#### 272 4 Results and discussion

273 To assess the performance of the model, we evaluate the mean, distribution and autocorrelation  
274 of the synthetically generated time series  $G_{cell}^{synth}$  obtained from pyranometer measurements  
275  $G_{pyr}$  in comparison to the data measured with the reference cell  $G_{cell}^{meas}$  in each of the test  
276 datasets (Table 3).

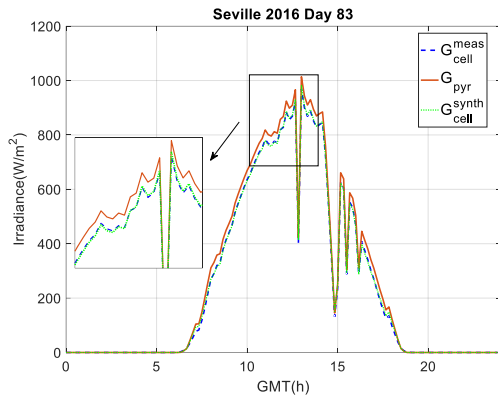
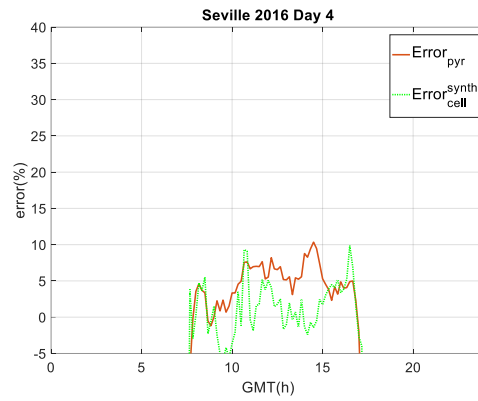
277 In figure 5 we represent the pyranometer measured solar radiation in continuous orange, the  
278 reference PV cell measured solar radiation in discontinuous blue and the synthetic solar  
279 radiation in dotted green, of four selected days throughout the year in different sky conditions  
280 for the location of Seville on the figures on the left. We also present the deviation between the  
281 pyranometer ( $Error_{pyr}$ ) and the PV calibrated cell measurements in continuous red and the  
282 deviation between the measured and synthetic calibrated cell data in dotted green on the right  
283 ( $Error_{cell}^{synth}$ ). The deviations are calculated following equations 10 and 11.

$$284 \quad Error_{pyr} = 100 \cdot \left( \frac{G_{pyr} - G_{cell}^{meas}}{G_{cell}^{meas}} \right) \quad (10)$$

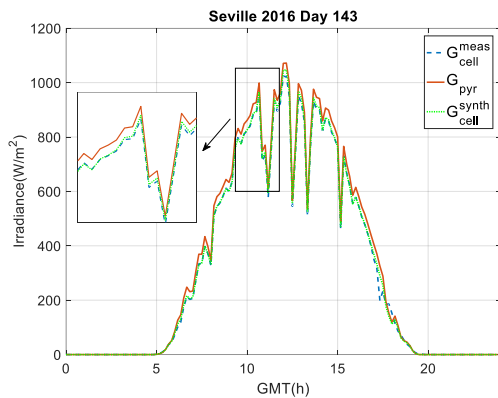
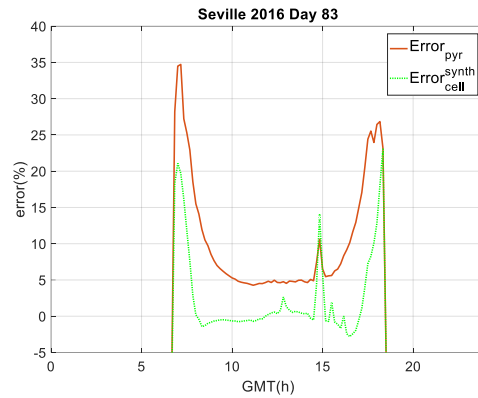
$$285 \quad Error_{cell}^{synth} = 100 \cdot \left( \frac{G_{cell}^{synth} - G_{cell}^{meas}}{G_{cell}^{meas}} \right) \quad (11)$$



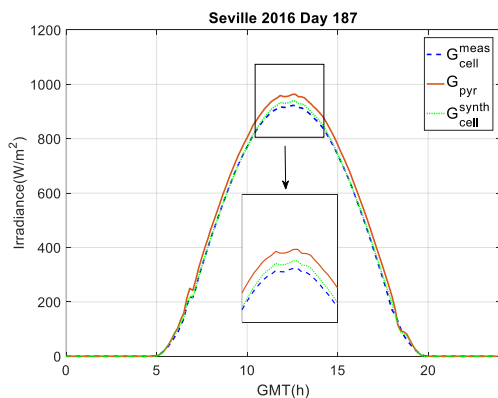
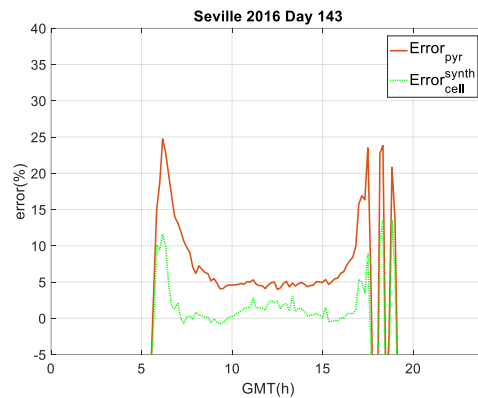
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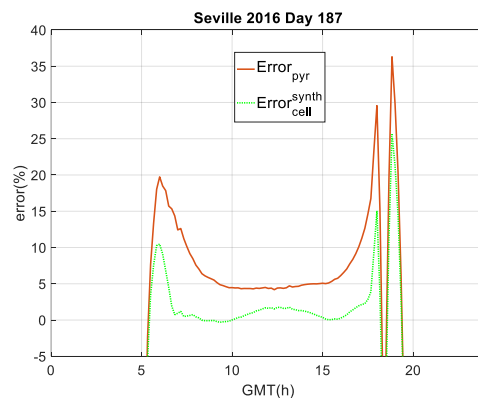
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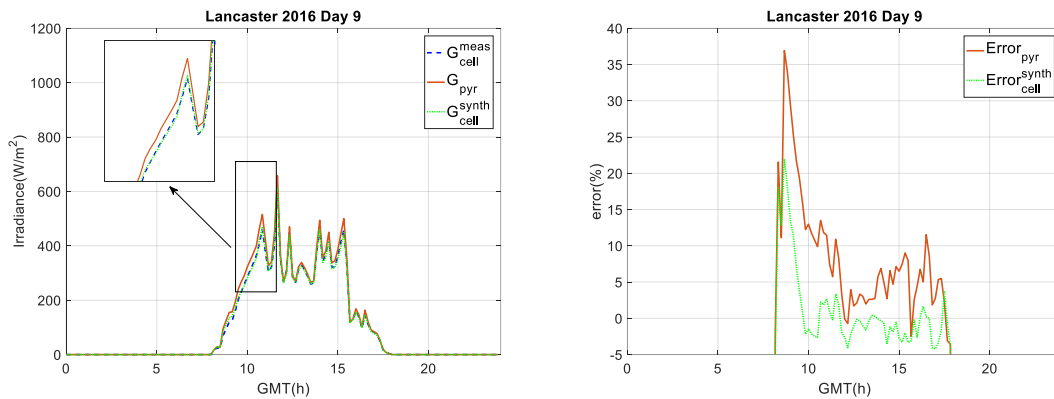
291 **Figure 5.** Four daily 10-min solar radiation profiles for the location of Seville.  $G_{pyr}$  is the solar  
 292 radiation measured with the pyranometer,  $G_{cell}^{meas}$  is the solar radiation measured with the PV  
 293 reference cell and  $G_{cell}^{synth}$  is the synthetically obtained PV reference cell data. On the left, the  
 294 daily profiles, on the right the instant errors.

295 From day 187 of figure 5 we can observe that the greater error values are found for low solar  
 296 elevations at clear sky conditions  $\alpha < 5^\circ$  mainly caused by high incidence angles. It is noticeable  
 297 that on cloudy days, such as the one presented in day 4 in figure 5, this tendency is not observed.  
 298 From day 4 we can observe that on cloudy days, with a greater amount of DHI, the differences  
 299 between both errors is lower than on sunny days, meaning that the model shows worse  
 300 performance on cloudy days, possibly due to the spectral distribution of the solar radiation that  
 301 may drop most of the energy in the accepted wavelengths range of the cell on cloudy days.  
 302 According to Nann et al., [31] clouds act somewhat as a neutral density filter upper wavelength  
 303 limit of the VIS region of the spectrum. At the upper wavelength limit of VIS and in the NIR  
 304 region, clouds are strong absorbers of radiation in selected wavelength bands, due to increased  
 305 water-vapour absorption and by liquid-water absorption.

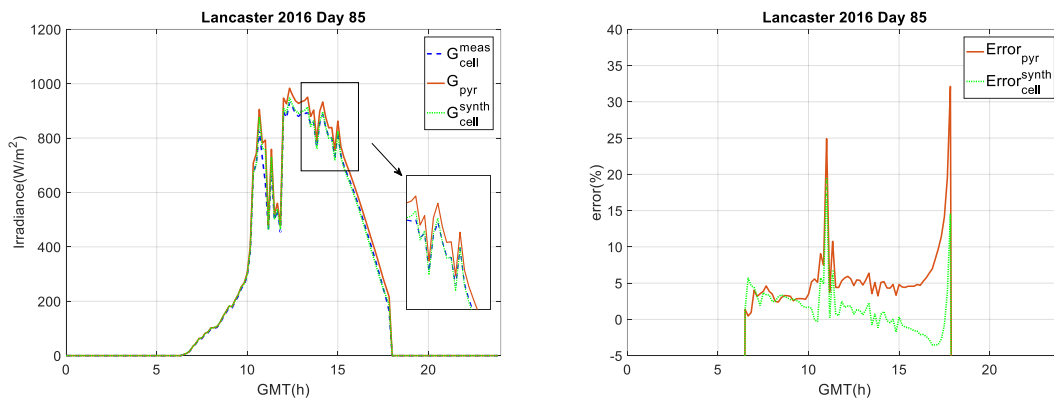
306 In any case, synthetic data errors ( $Error_{cell}^{synth}$ ) are lower than pyranometer data errors  
 307 ( $Error_{pyr}$ ) for all sky conditions and for a wide range of solar elevations and solar radiation  
 308 levels.

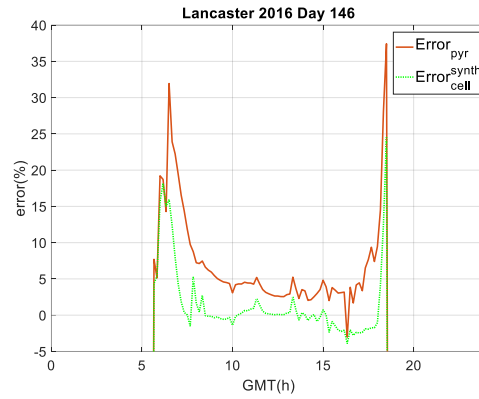
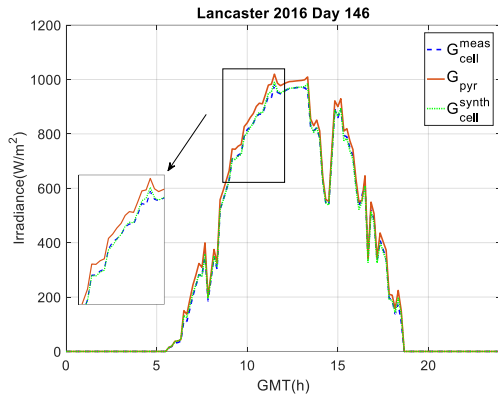
309 In figure 6 we perform the same evaluation for Lancaster. The error of the synthetic data  
 310 ( $Error_{cell}^{synth}$ ) is lower than the error when comparing pyranometer to calibrated cell data  
 311 ( $Error_{pyr}$ ) for all the sky conditions. In any case, the approach is more accurate for clear sky  
 312 conditions and greater solar elevations. We can only find errors in the synthetic data greater  
 313 than 5% for solar elevations lower than  $5^\circ$ . It should be noted that solar radiation data at low  
 314 elevations have negligible impact on the photovoltaic module yield.

315

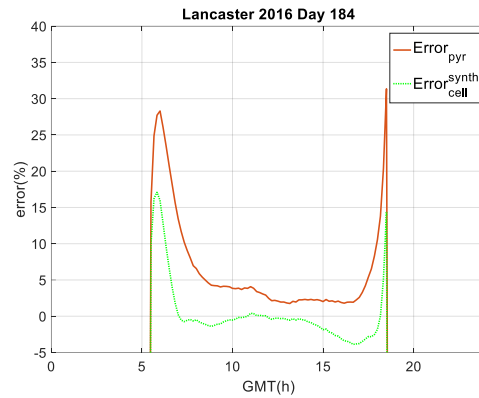
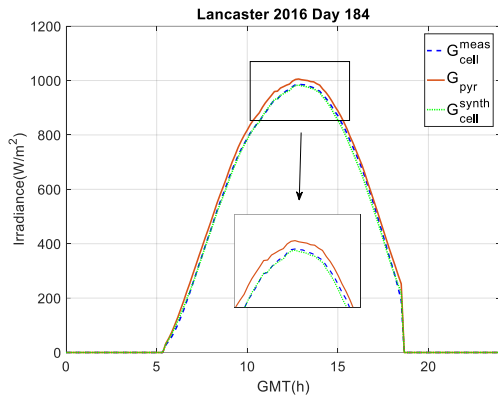


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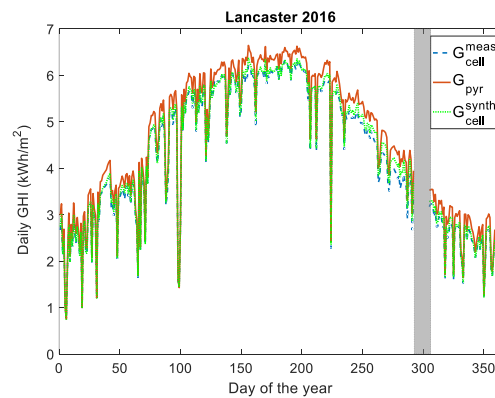
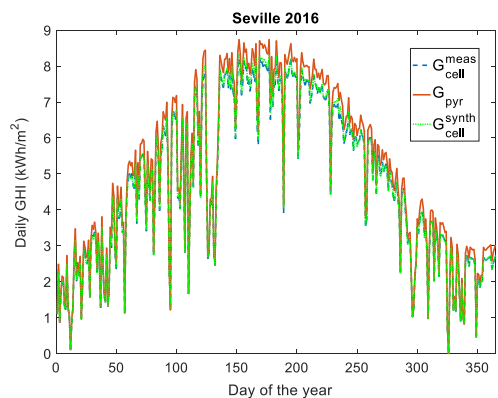
317



318

319 **Figure 6.** Four daily 10-min solar radiation profiles for the location of Lancaster.  $G_{pyr}$  is the solar  
 320 radiation measured with the pyranometer,  $G_{cell}^{meas}$  is the solar radiation measured with the PV  
 321 reference cell and  $G_{cell}^{synth}$  is the synthetically obtained PV reference cell data. On the left, the  
 322 daily profiles, on the right the instant errors.

323 In figure 7 we present the daily cumulative values of  $G_{pyr}$ ,  $G_{cell}^{meas}$  and  $G_{cell}^{synth}$  for the location of  
 324 Seville and Lancaster. In Lancaster there is a period with no available data covering 12 days in  
 325 October. In the correct data, we can observe that the synthetically obtained daily cumulative  
 326 data is more similar to the PV reference measured solar radiation data than the pyranometer  
 327 measurements daily cumulative data.



328

329 **Figure 7.** Daily cumulative solar radiation values for the location of Seville (left) and Lancaster  
 330 (right).  $G_{pyr}$  is the solar radiation measured with the pyranometer,  $G_{cell}^{meas}$  is the solar radiation

331 measured with the PV reference cell and  $G_{cell}^{synth}$  is the synthetically obtained PV reference cell  
 332 data.

333 In tables 6-7 we present the monthly and annual cumulative values of the measured and  
 334 synthetic time series for one year for the location of Seville and Lancaster respectively with the  
 335 percentage differences in comparison to the reference PV cell measured data. We identified  
 336 continuous irregularities on twelve consecutive days in October in Lancaster. We have not  
 337 included this month in the performance evaluation of the model. We can observe that the  
 338 synthetically generated data show lower differences in the monthly cumulative values in  
 339 comparison to the monthly cumulative values of the reference PV cell-measured dataset varying  
 340 from -0.2% to 1.4% in Seville and from 0.3% to 3.3% in Lancaster, while the monthly cumulative  
 341 values of the pyranometer measurements show differences that range from 5.3% to 9.5% in  
 342 Seville and 4.4% to 11.1% in Lancaster. We can observe that the greater differences in the  
 343 pyranometer monthly data in comparison to the cell-measured monthly data are found from  
 344 September to March coinciding with the time of the year with the lower solar elevations.

345 **Table 6.** Monthly and annual cumulative values of the synthetic sets and their differences in  
 346 comparison to the measured reference cell data for the location of Seville.  
 347

| Dataset            | Unit                   | Jan  | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep  | Oct  | Nov  | Dec  | Year |
|--------------------|------------------------|------|-----|-----|-----|-----|-----|-----|-----|------|------|------|------|------|
| $G_{cell}^{meas}$  | kWh/m <sup>2</sup>     | 62   | 87  | 154 | 159 | 195 | 229 | 229 | 210 | 165  | 114  | 77   | 70   | 1751 |
| $G_{pyr}$          | kWh/m <sup>2</sup>     | 66   | 93  | 164 | 167 | 206 | 243 | 242 | 224 | 175  | 121  | 83   | 77   | 1861 |
|                    | $Error_{pyr}$          | 7.0  | 7.1 | 6.5 | 5.3 | 5.7 | 6.1 | 5.8 | 6.5 | 5.7  | 6.2  | 7.5  | 9.5  | 6.3  |
| $G_{cell}^{synth}$ | kWh/m <sup>2</sup>     | 62   | 87  | 154 | 160 | 197 | 232 | 231 | 212 | 165  | 114  | 76   | 70   | 1760 |
|                    | $Error_{cell}^{synth}$ | -0.2 | 0.4 | 0.2 | 0.4 | 1.1 | 1.4 | 0.9 | 1.0 | -0.4 | -0.5 | -0.7 | -0.1 | 0.5  |

348

349 **Table 7.** Monthly and annual cumulative values of the synthetic sets and their differences in  
 350 comparison to the measured reference cell data for the location of Lancaster.

| Dataset            | Unit                   | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov  | Dec | Year(*) |
|--------------------|------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|---------|
| $G_{cell}^{meas}$  | kWh/m <sup>2</sup>     | 74  | 95  | 122 | 150 | 174 | 180 | 185 | 166 | 136 | -   | 80   | 71  | 1432    |
| $G_{pyr}$          | kWh/m <sup>2</sup>     | 80  | 102 | 130 | 159 | 181 | 190 | 194 | 176 | 149 | -   | 89   | 78  | 1527    |
|                    | $Error_{pyr}$          | 7.8 | 8.0 | 6.1 | 5.6 | 4.4 | 5.6 | 4.7 | 6.4 | 9.4 | -   | 11.1 | 9.3 | 6.6     |
| $G_{cell}^{synth}$ | kWh/m <sup>2</sup>     | 75  | 96  | 123 | 152 | 174 | 182 | 186 | 169 | 141 | -   | 82   | 72  | 1452    |
|                    | $Error_{cell}^{synth}$ | 0.8 | 1.9 | 1.0 | 0.9 | 0.3 | 1.4 | 0.4 | 1.6 | 3.7 | -   | 3.3  | 1.3 | 1.4     |

351 (\*)October not included in the total sum

352 The increased differences in Lancaster may be attributed to the good training of the model for  
 353 Seville (through the multi-step regression analysis) and the use of an empirical parameter  
 354 developed for Seville.



355

#### 4.1 Mean evaluation

356 We evaluate the deviations between the modelled and measured PV reference cell data using  
 357 the Root Mean Squared Deviation (*RMSD*) calculated following equation 12. We also calculate  
 358 the *RMSD* of the pyranometer data in comparison to the calibrated cell-measured data in order  
 359 to show a base to compare (equation 13).

$$360 \quad \text{RMSD}_{cell} = \sqrt{\frac{1}{N} \sum_{i=1}^N (G_{cell}^{meas} - G_{cell}^{synth})^2} \quad (12)$$

$$361 \quad \text{RMSD}_{pyr} = \sqrt{\frac{1}{N} \sum_{i=1}^N (G_{cell}^{meas} - G_{pyr})^2} \quad (13)$$

362 where  $N$  is the number of data pairs,  $G_{cell}^{meas}$  is the global horizontal irradiance measured with  
 363 the reference PV cell,  $G_{cell}^{synth}$  is the global horizontal irradiance synthetically obtained from  
 364 pyranometer measurements and  $G_{pyr}$  is the solar radiation measured with the pyranometer.  
 365 The evaluation is performed in the 10-min and daily resolution. Only data for solar elevations  
 366 greater than  $2^\circ$  are considered in this analysis. In table 8 we present the  $\text{RMSD}_{cell}$  and in table  
 367 9 the  $\text{RMSD}_{pyr}$  in the 10-min and daily resolution for the test datasets. We also present the  
 368 *RMSD* in % by dividing the *RMSD* by the average value (equations 14 and 15).

$$369 \quad \text{RMSD}_{cell}(\%) = 100 \cdot \left( \frac{\sqrt{\frac{1}{N} \sum_{i=1}^N (G_{cell}^{meas} - G_{cell}^{synth})^2}}{\overline{G_{cell}^{meas}}} \right) \quad (14)$$

$$370 \quad \text{RMSD}_{pyr}(\%) = 100 \cdot \left( \frac{\sqrt{\frac{1}{N} \sum_{i=1}^N (G_{cell}^{meas} - G_{pyr})^2}}{\overline{G_{cell}^{meas}}} \right) \quad (15)$$

371

372 For Seville, the average value ( $\overline{G_{cell}^{meas}}$ ) in the 10-min resolution is  $391 \text{ W/m}^2$  and in the daily  
 373 resolution is  $4.7 \text{ kWh/m}^2$ . For Lancaster, the average value ( $\overline{G_{cell}^{meas}}$ ) in the 10-min resolution is  
 374  $371 \text{ W/m}^2$  and in the daily resolution is  $3.8 \text{ kWh/m}^2$ .

375 **Table 8.**  $\text{RMSD}_{cell}$  in the 10-min and daily resolution for Seville and Lancaster test datasets.

| Station (year)   | $\text{RMSD}_{10\text{-min}}$ |     | $\text{RMSD}_{\text{daily}}$ |     |
|------------------|-------------------------------|-----|------------------------------|-----|
|                  | $\text{W/m}^2$                | %   | $\text{kWh/m}^2$             | %   |
| Seville (2016)   | 9.5                           | 2.4 | 0.06                         | 1.4 |
| Lancaster (2016) | 19.7                          | 3.8 | 0.09                         | 2.5 |

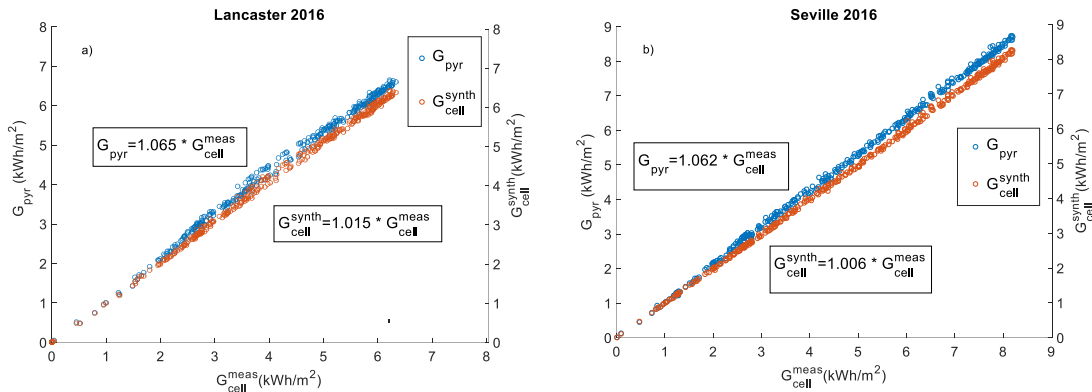
376

377 **Table 9.**  $\text{RMSD}_{pyr}$  in the 10-min and daily resolution for Seville and Lancaster test datasets.

| Station (year)   | $\text{RMSD}_{10\text{-min}}$ |     | $\text{RMSD}_{\text{daily}}$ |     |
|------------------|-------------------------------|-----|------------------------------|-----|
|                  | $\text{W/m}^2$                | %   | $\text{kWh/m}^2$             | %   |
| Seville (2016)   | 29.6                          | 7.5 | 0.33                         | 6.9 |
| Lancaster (2016) | 41.7                          | 8.1 | 0.29                         | 7.7 |

378

379 The RMSD between measured data from the reference cell and pyranometer, mainly related to  
 380 spectral and angular losses, reach 8% on a daily basis. Moreover, when applying the correction  
 381 algorithm, the RMSD between measured data from the reference cell and synthetic data is  
 382 reduced to 2%. In figure 8 we present the daily  $G_{cell}^{meas}$  vs the daily  $G_{pyr}$  together, with the  
 383 daily  $G_{cell}^{synth}$  in Lancaster in the figure on the left and Seville in the figure on the right in a scatter  
 384 plot. We can observe how the BIAS is reduced significantly from values around 6% to values  
 385 lower than 2%. Reduction is even higher in Seville.



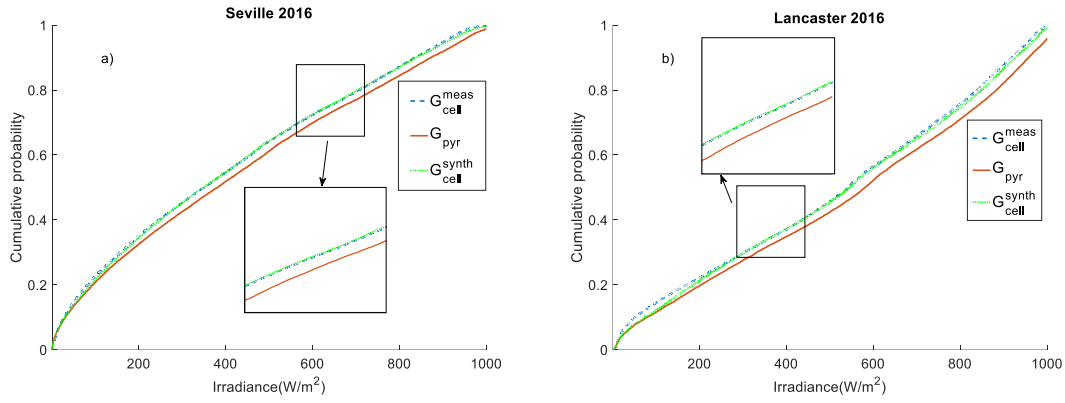
386  
 387 **Figure 8.** Scatter plot of the daily cumulative solar radiation values measured with the cell versus  
 388 the daily solar radiation values measured with the pyranometer and the synthetically generated  
 389 data for the location of Lancaster (a) and Seville (b).

## 390 4.2 Distribution evaluation

391 The distribution is evaluated since it is assumed that differences in these terms may lead to  
 392 differences in PV plant production. To evaluate the distribution, we calculate the KSI  
 393 (Kolmogorov-Smirnov test integral, equation 16) index defined as the integrated differences  
 394 between the CDFs of two datasets. It is a widely used index to compare cumulative distributions  
 395 of measured and synthetic solar radiation sets [32]. The unit of this index is the same for the  
 396 corresponding magnitude. We only analyse data for solar elevations greater than  $2^\circ$ .

$$397 \quad KSI = \int_{x_{min}}^{x_{max}} D_n dx, \quad (16)$$

398 where,  $x_{max}$  and  $x_{min}$  are the extreme values of the independent variable, and  $D_n$  are the  
 399 differences between the CDFs of datasets evaluated in 100 points. The higher the KSI values, the  
 400 greater the differences in the CDFs of the evaluated datasets. We calculate the KSI as a  
 401 comparison of the CDFs of the solar radiation sets measured with the pyranometer to the solar  
 402 radiation sets measured with the PV reference cell in one hand, and the synthetically obtained  
 403 PV reference cell solar radiation sets to the solar radiation sets measured with the PV reference  
 404 cell in the other hand. This calculation is performed in order to quantify the impact of the  
 405 developed model when used as a correction factor for spectral and angular losses of silicon cells.  
 406 In Figure 9 we represent the CDFs of the measured and synthetic sets for Seville and Lancaster  
 407 2016.



408

409 **Figure 9.** CDFs of the measured and synthetic sets for Seville 2016 (a) and Lancaster 2016 (b).  
 410  $G_{pyr}$  is the solar radiation measured with the pyranometer,  $G_{cell}^{meas}$  is the solar radiation  
 411 measured with the PV reference cell and  $G_{cell}^{synth}$  is the synthetically obtained PV reference cell  
 412 data.

413 In Table 10 we present the KSI value ( $W/m^2$ ) of the evaluated datasets. The measurements with  
 414 pyranometer and reference PV cell present different CDFs. However, the synthetically generated  
 415 reference PV cell data present a significant improvement towards similarity to the measured PV  
 416 cell CDF.

417 **Table 10.** KSI ( $W/m^2$ ) for Seville and Lancaster test datasets.

| Parameter       | Station (year)   | $G_{pyr}$ | $G_{cell}^{synth}$ |
|-----------------|------------------|-----------|--------------------|
| KSI ( $W/m^2$ ) | Seville (2016)   | 24.6      | 3.7                |
|                 | Lancaster (2016) | 35.6      | 8.6                |

418

419 The similarity on the measured and synthetic reference PV cell data can be quantified with the  
 420 KSI. It is reduced by 85% for the location of Seville and by 75% in Lancaster. The model has been  
 421 trained with more than three years of measurements from the location of Seville, therefore its  
 422 performance is slightly better for Seville than for Lancaster. In any case, it is worth highlighting  
 423 that the model can be globally applied without any local adaptation. Obviously the errors are  
 424 lower for the location where the model has been trained.

### 425 4.3 Autocorrelation evaluation

426 There is a relation between consecutive values that should be maintained when generating  
 427 synthetic solar radiation data. To that end, we evaluate the autocorrelation qualitatively by  
 428 calculating and representing the ramp rates (RRs), defined as the difference between successive  
 429 data points over 10 minutes (equation 17).

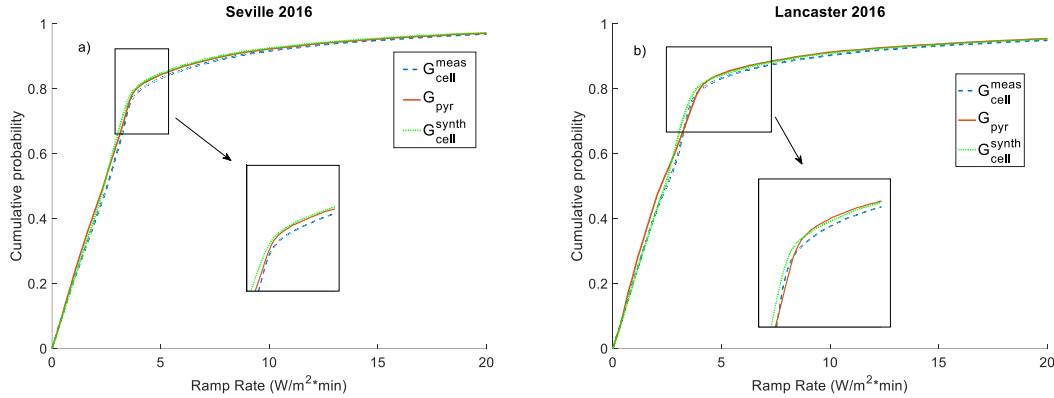
430

$$431 \quad RR = \frac{(GHI_k - GHI_{k-1})}{\Delta t} \quad (17)$$

432 where  $\Delta t$  refers to an interval of 10 minutes. The units will be given in  $W/m^2 \cdot min$ . We calculate  
 433 the absolute RR values for the annual datasets taking into account only daytime observations.  
 434 We qualitatively evaluate the RRs of each dataset through the CDFs (Figure 10) and

435 quantitatively through the Kolmogorov Smirnov Index of the CDFs of the Ramp rates ( $KSI_{RR}$ )  
 436 (Table 11).

437 **Figure 10.** CDFs of the RRs of the measured and synthetic sets for Seville 2016 (a) and Lancaster  
 438 2016 (b).  $G_{pyr}$  is the solar radiation measured with the pyranometer,  $G_{cell}^{meas}$  is the solar  
 439 radiation measured with the PV reference cell and  $G_{cell}^{synth}$  is the synthetically obtained PV  
 440 reference cell data.



441

442 **Table 11.**  $KSI_{RR}$  ( $W/m^2 \cdot min$ ) for Seville and Lancaster test datasets.

| Parameter                        | Station (year)   | $G_{pyr}$ | $G_{cell}^{synth}$ |
|----------------------------------|------------------|-----------|--------------------|
| $KSI_{RR}$ ( $W/m^2 \cdot min$ ) | Seville (2016)   | 0.22      | 0.11               |
|                                  | Lancaster (2016) | 0.41      | 0.20               |

443

444 From the RRs evaluation we can observe a reduction in the  $KSI_{RR}$  of around 50% in both locations  
 445 from  $G_{pyr}$  to  $G_{cell}^{synth}$ . The model, which has been trained with data measured in Seville, presents  
 446 therefore a better performance in terms of autocorrelation for the location of Seville than for  
 447 the location of Lancaster, but we can highlight its global applicability without any local  
 448 adaptation. Nevertheless, more locations should be evaluated to assess the performance of the  
 449 model in a wider range of climates.

## 450 5 Conclusions

451 In this paper, we present a simple model to obtain reference cell 10-min solar radiation data  
 452 from thermopile pyranometer measured data series with reasonable accuracy. Our model does  
 453 not require any other input data besides the pyranometer measurements and can be globally  
 454 applied with no local adaptation or calibration. We have trained the model in one location  
 455 (Seville, Spain) and applied it in two locations, Seville and Lancaster (USA), obtaining satisfactory  
 456 results. The model is developed from an initial cluster of the training data and several  
 457 regressions, taking into account the main parameters affecting the angular and spectral losses;  
 458 the solar elevation and the clearness index. At the time of using it, only thermopile pyranometer  
 459 data and a few geometrical calculations are required. This way, the model shows great simplicity  
 460 facilitating its applicability.

461 The model shows better performance on sunny days with high solar elevations, when most of  
462 the energy is obtained. We have evaluated the mean, distribution and autocorrelation of the  
463 synthetic sets in comparison to measured data with a reference cell using measured data with  
464 a pyranometer as input. Daily RMSD is reduced from 7-8% to 1-2% when evaluating a complete  
465 annual set. The frequency distribution of the synthetic sets is also improved. It has been  
466 quantified in an 80% reduction of the KSI. The autocorrelation is quantified through the KSI of  
467 the RRs obtaining also a reduction of 50%. The model shows better performance for the location  
468 of Seville, where it has been trained, since solar radiation depends on local phenomena. Future  
469 works will focus on the improvement of the model by using data from more different climates  
470 for its training, and tests will focus on the evaluation of its global applicability.

#### 471 **Acknowledgments**

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