



Depósito de Investigación
Universidad de Sevilla

Depósito de investigación de la Universidad de Sevilla

<https://idus.us.es/>

“This is an Accepted Manuscript of an article published by Elsevier in *Journal of Cleaner Production* on Jiménez-Rosado, M., Bouroudian, E., Perez-Puyana, V., Guerrero, A., & Romero, A. (2020). Evaluation of different strengthening methods in the mechanical and functional properties of soy protein-based bioplastics. *Journal of Cleaner Production*, 262, 121517, available at: <https://doi.org/10.1016/j.jclepro.2020.121517>

Evaluation of different strengthening methods in the mechanical and functional properties of soy protein-based bioplastics

M. Jiménez-Rosado^{1*}, E. Bouroudian¹, V. Perez-Puyana², A. Guerrero¹, A. Romero²

¹Departamento de Ingeniería Química, Escuela Politécnica Superior, Universidad de Sevilla, 41011, Sevilla, Spain.

²Departamento de Ingeniería Química, Facultad de Química, Universidad de Sevilla, 41012, Sevilla, Spain.

***MERCEDES JIMÉNEZ-ROSADO**

Departamento de Ingeniería Química

Universidad de Sevilla,

41011, Sevilla (Spain)

e-mail: mjimenez42@us.es

Phone: +34 954557179 Fax: +34 954556441

1 **Abstract**

2 The bioplastics manufactured are still not competitive compared to conventional
3 plastics, due to their higher price and poor mechanical properties. For this purpose,
4 different physical strengthening methods have been studied to evaluate the
5 reinforcement of soy protein-based bioplastics: mold temperature increase (from
6 70 °C to 130 °C), as the application of a dehydrothermal (4 and 24 h at 50 °C) or
7 ultrasound (for 5 and 45 min at 20 kHz) treatment. In this sense, the crosslinking
8 degree, the mechanical properties, water uptake measurements and scanning
9 electron micrographs of the different bioplastics were compared. The results
10 conclude that suitable processing conditions and post-treatments could favor some
11 characteristics of bioplastics (such as maximum stress (~5 times) or strain at break
12 (~3 times)), although worsening others (such as water uptake capacity (~50%)).
13 Specifically, thermal treatments improved the mechanical properties of the
14 structures obtained, whereas the ultrasound treatment leads to the formation of a
15 structure with smaller pores.

16

17 **keywords:** Soy bioplastic; pea bioplastic; mold temperature; dehydrothermal
18 treatment; ultrasounds.

19 **1. Introduction**

20 Nowadays, plastics have an ever-increasing production and consumption due to
21 the large number of domestic and industrial applications, such as packaging or
22 hygienic products (Ahmed et al., 2018). However, this trend involves great
23 contamination due to the low degradability of plastics according to the studies
24 driven by Ahmed et al. (2018) or Derraik (2002). Thus, the weight of plastics in the
25 ocean will be greater than that of fish in 2050 (Ellen MacArthur Foundation, 2016).
26 Furthermore, most products we eat contain traces of plastics (Carrington, 2019).
27 The substitution of these petroleum-based plastics with bioplastics (bio-based
28 plastics) is seen as a potential alternative (Russo et al., 2019), since it will minimize
29 the dependency of plastic on petrol fuels and the pressure on landfills from solid
30 wastes (Álvarez-Chávez et al., 2012).

31 Bioplastics can be either bio-sourced (from biomass) or biodegradable, including
32 fossil resources, but also there are bioplastics that are both bio-sourced and
33 biodegradable (European Bioplastics, 2019). The latter, which have both
34 characteristics, are the most interesting and the most recently studied by using
35 different raw materials as soy protein (Jiménez-Rosado et al., 2019), cornhusk
36 fibers (Saenghirunwattana et al., 2014) or porcine plasma protein (Álvarez-Castillo
37 et al., 2019), among other alternatives (Flieger et al., 2003), by injection molding or
38 extrusion processing (Verbeek and van den Berg, 2010). In this context, bioplastics
39 can be made of polymers derived from biomass, such as proteins, which, in
40 combination with a plasticizer, can be easily processed (Tummala et al., 2006). In
41 addition, these proteins could come from byproducts or waste of agri-food industry,
42 generating added value to these products and closing its life cycle
43 (Mohammadhosseini and Tahir, 2018a), therefore encouraging the circular

44 economy. However, their mechanical properties are much lower (i.e. they are a
45 young's modulus of 7 MPa in contract with 25 MPa of PE or 35 MPa of PS)
46 (Zhuang et al., 2014), and their price is often higher than that of conventional
47 plastics (around 10 times more expensive), thus their use is still limited (Confente
48 et al., 2019). These mechanical properties can be improved by using chemical,
49 enzymatic or physical treatments. Thus, formaldehyde, glutaraldehyde or glyoxal
50 (Marquié, 2001) as well as even citric acid (Awadhiya et al., 2016) have been used
51 such as chemical crosslinker and transglutaminase (Giosafatto et al., 2018) have
52 been used like enzymatic ones. In addition, fillers (i.e. metalized plastic fibers) can
53 be added, which without interacting with proteins, improve the final properties of
54 the bioplastic (Mohammadhosseini et al., 2018). However, the use of some of
55 these materials can cause toxicity or the transmission of harmful properties to the
56 product they are being used for (Gerrard, 2002). In this context, the use of physical
57 treatments is the most recommended to could prevent these disadvantages and
58 improve the mechanical properties of bioplastics without causing toxicity problems
59 that may affect its subsequent use. Among the different physical treatments (i.e.
60 ultrasound, microwaves or thermal treatments), thermal treatments are the most
61 used, both during processing (Mo et al., 1999) and post-processing (Álvarez-
62 Castillo et al., 2018). In addition, there are also works where ultrasound
63 (Jayasooriya et al., 2004) or microwaves (Ghasri et al., 2019) are used to increase
64 the degree of crosslinking of bioplastics. However, these improvements normally
65 affect, apart from the mechanical properties, other properties such as water uptake
66 capacity, which could decrease between 1000-2500%, (Álvarez-Castillo et al.,
67 2018) or even the morphology of the final structure obtained and the degradation

68 rate. Therefore, an optimization is required to reach the final desired properties
69 (Perez et al., 2016).

70 Among the possible applications, protein-based bioplastics can develop a
71 sustainable product that may act as superabsorbent materials (SABs) (Cuadri et
72 al., 2017). SABs are materials with the ability to absorb and retain more than 10
73 times their own weight of water, keeping their integrity without dissolving (Cuadri et
74 al., 2016). The forces which allow water absorption by polymers are mainly the
75 osmotic pressure and the formation of hydrogen bonds (Barbe and Storz, 2005).
76 There are several applications for these materials, such as construction
77 (Mohammadhosseini and Tahir, 2018b), waste management, agriculture,
78 electronics and horticulture (Nnadi and Brave, 2011). Among them, personal
79 hygiene products constitute most of the market of these materials (Magnay et al.,
80 2010).

81 Specifically, soy protein has a high content of glutamic and aspartic acids, more
82 than other proteins such as rice or pea, which favor the formation of these
83 hydrogen bonds and, therefore, making soy protein-based bioplastics a potential
84 option as SABs (Fernández-Espada et al., 2016a). In addition, soy protein normally
85 used in this field is a co-product with soy oil and one of the cheapest proteins in
86 nature, which is another advantage to consider it the best alternative to plastics
87 (Fernández-Espada et al., 2016b). However, the properties (especially the
88 mechanical properties) shown by soy protein-based bioplastics (Gironi and
89 Piemonte, 2011) or other compostable alternatives (Song et al., 2009)
90 manufactured to date are not good enough to compete with conventional plastics;
91 therefore, further research is necessary to find a methodology that can generate an
92 adequate relationship between the properties of these bioplastics (Karana, 2012).

93 In this context, the main objective of this work was the use of different physical
94 strengthening in order to enhance the mechanical properties of soy protein-based
95 bioplastics without worsening their functional properties (i.e. water uptake
96 capacity). To this end, the manufacturing conditions were evaluated and different
97 post-treatments (dehydrothermal or ultrasounds treatments) were conducted to
98 reinforce the structure of the bioplastics. In order to compare the results,
99 mechanical and microstructural measurements were carried out, as well as water
100 uptake capacity tests.

101

102 **2. Materials and methods**

103 ***2.1 Materials***

104 Bioplastics are usually composed of three different elements: matrix, plasticizer
105 and additives (optional). In this work, the matrix was soy protein isolate (SPI, 91
106 wt.% protein), which was supplied by Protein Technologies International (SUPRO
107 500E, Belgium). This raw material is a byproduct of a soybean oil production, so its
108 use in this work gives it an added value. Its chemical composition was evaluated
109 obtaining a minimum of 90 wt.% of protein, maximum of 6 wt.% of humidity, 1 wt.%
110 lipids, maximum of 0.1 wt.% carbohydrates and 5 wt.% of ash. In addition, its pH is
111 between 6.9 and 7.4, being negatively charged (isoelectric point 4.5). Thus, this
112 source of soy protein have a higher protein content than others such as used by
113 Tummala et al. (2006), 91 vs. 52 wt.%.

114 In addition, glycerol (Gly) was used as plasticizer, which was purchased from
115 Panreac Química Ltd. (Spain). The use of other plasticizers has been proved
116 (Tummala et al., 2006), but glycerol is the one that generate bioplastics with the
117 best mechanical properties.

118 **2.2 Preparation of soy protein-based bioplastics**

119 The soy protein-based bioplastics were prepared in a two-step process, which was
120 used and optimized in previous studies related to the production of soy-based
121 bioplastics combined with albumen (Fernández-Espada et al., 2016b),
122 lignocellulose (Gamero et al., 2019) or even functionalized soy protein (Cuadri et
123 al., 2017). Firstly, SPI and Gly in a 1:1 mass ratio was homogenized in a mixing
124 step. For this, both raw materials were introduced in a two-blade counter-rotating
125 ThermoHaake mixer PolyLab QC (Germany) for 10 min at 50 rpm and adiabatic
126 conditions. In this step, the temperature and torque were controlled to prevent the
127 plasticization of the blends in the chamber. In this case, the temperature was below
128 37 °C and the maximum torque was 5 Nm, so the blends were always under their
129 plasticization parameters (Fernández-Espada et al., 2016b).

130 The second step consisted in an injection molding of the dough-like blend obtained
131 in the mixing. For this, a ThermoHaake MiniJet Piston Injection Molding System II
132 (Germany) was used to obtain rectangular bioplastics (60x10x1 mm³) and dumb-
133 bell-type bioplastics (UNE-EN ISO 527-2, 2012). The parameters used, according
134 to previous studies, were cylinder and mold temperature of 40 and 70 °C,
135 respectively, injected for 20 s at 500 bar and using a post- injection pressure of 200
136 bar for 300 s. These parameters were selected to highlight the water uptake
137 capacity of soy protein-based bioplastics, but they have poor mechanical
138 properties (Fernández-Espada et al., 2016a). In this work we aimed to enhance
139 these mechanical properties without significantly affecting the water uptake
140 capacity.

141 **2.2.1 Strengthening modifications**

142 To enhance the mechanical properties, three different experiments were carried
143 out. In the first case, the mold temperature was increased. Previous studies state
144 that protein-based bioplastics have a better crosslinking with a higher mold
145 temperature (Thakur, 2017). This greater crosslinking could improve the
146 mechanical properties of these bioplastics. In this context, an increment of 60 °C in
147 the mold temperature was applied during the injection molding step, so the final
148 mold temperature used was 130 °C instead of 70 °C. It worth mentioning that
149 higher temperatures could cause protein disintegration without achieving the
150 desired effect.

151 The second experiment consisted in the addition of a post-treatment. Thus, the
152 bioplastics were subjected to a thermal step at 50 °C in a conventional oven
153 (Memmert, Germany). The application of this step, called dehydrothermal
154 treatment (DHT), for a long time (12-14 h) can favor the formation of covalent
155 bonds in it (Álvarez-Castillo et al., 2018). In order to study the effect of this step
156 with the time of treatment in the bioplastic properties, different times (4 and 24
157 hours) were evaluated.

158 Finally, the last experiment was an ultrasound post-treatment (US). US treatment
159 produces localized cavitation, which facilitates the disintegration of the particles
160 (Karki, 2009), allowing the structure to rearrange and, consequently, improving the
161 mechanical properties of the bioplastics. To carry out this experiment, the
162 bioplastics, after the injection molding step, were inserted into vacuum bags. Then,
163 these bags with the bioplastics were immersed in an ultrasound bath (JP Selecta)
164 at 50 kHz with 100 W (power) and 0,4 A (intensity), using water as medium. In this
165 case, the treatment time was also evaluated at 5 and 45 min.

166 The selected times in both treatments (thermal and US) were chosen to achieve a
167 maximum change in the bioplastic properties (long times) and a less radical
168 change (short times) to assess if all the bioplastic properties change uniformly with
169 the application of the treatment.

170 **2.3 Characterization of soy protein-based bioplastics**

171 *2.3.1 Degree of crosslinking*

172 The degree of crosslinking was determined in order to evaluate the modification
173 produced in the microstructure caused by each of the variations in the process. For
174 this, the same protocol used by Zárte-Ramírez et al. (2014) was following. Thus,
175 a portion of each bioplastic (15x10x1 mm³) was immersed for 2 h in a denaturing
176 agent solution (0.086 mol/L Tris base, 0.045 mmol/L glycine, 2 mmol/L EDTA, 10
177 g/L sodium dodecyl sulfate (SDS) pH 6 buffer) to denaturalize the uncrosslinked
178 protein. Subsequently, the solutions were subjected to a centrifugation step at
179 10000xg for 10 min to separate the denatured protein solution. Finally, the soluble
180 protein fraction was determined using Lowry's method (Markwell et al., 1978).
181 From these data, the degree of crosslinking of the bioplastics was estimated using
182 as reference the bioplastic for which the process was not modified (0%
183 crosslinking) and denaturing agent solution without bioplastic (100% crosslinking).
184 In this way, the crosslinking produced by the different treatments added can be
185 evaluated with respect to that performed by the traditional method (without physical
186 treatment carried out).

187 *2.3.2 Mechanical properties*

188 *2.3.2.1 Tensile tests*

189 Breakage resistance under tensile stress is a widely measured property of
190 materials used in structural applications. Tensile tests were performed in a MTS

191 insight Electromechanical-10kN Standard Length (Eden Prairie, USA) where the
192 dumb-bell-type bioplastics were subjected to an axial force until breakage,
193 following the UNE-EN ISO 527-2 standard (2012). The tests were carried out at
194 room temperature (22 ± 1 °C), using an extensional rate of 10 mm/min. The
195 equipment used can detect when the material breaks and provides parameters
196 such as maximum tensile stress (σ_{\max}), strain at the break (ε_{\max}) and Young's
197 modulus.

198 *2.3.2.2 Bending tests*

199 Bending tests were performed in order to evaluate the flexural resistance of the
200 bioplastics. In order to compare these results with the literature results (Patel et al.,
201 2016), a dynamic-mechanical analyzer RSA3 (TA Instrument, USA) with a dual
202 cantilever geometry were used to carry out these tests to rectangular bioplastics.

203 First, the linear viscoelastic range (the linear region where the elastic and viscous
204 moduli remain independent of the applied strain) were determined through strain
205 sweep tests (between 0.002 and 2% and 1 Hz). Subsequently, frequency sweep
206 tests were carried out between 0.02 and 20 Hz at a constant strain below the
207 critical strain (maximum strain where the bioplastics remain in the linear
208 viscoelastic range). All these measurements were performed at room temperature
209 (22 ± 1 °C). Thus, the elastic modulus (E') and loss tangent ($\tan \delta = E''/E'$) were
210 evaluated over the entire frequency range.

211 *2.3.4 Water uptake capacity & soluble matter loss*

212 In order to determine the superabsorbent character of the bioplastics (functional
213 property), water uptake capacity and soluble matter loss tests were performed.
214 These tests were carried out following a modification of the ASTM standard
215 ("ASTM D570-98: Standard Test Method for Water Absorption of Plastics," 2005).

216 Therefore, rectangular bioplastics (60x10x1 mm³) were immersed in 300 mL of
217 distilled water for 24 h at room temperature (22 ± 1 °C). Later, the samples were
218 subjected to a freeze-drying step for 24 h at -80 °C and low pressure (< 15 Pa)
219 using a Lyoquest freeze-dryer (Telstar, Spain) in order to remove all the bioplastic
220 water.

221 The water uptake capacity was then obtained using equation 1 in order not to
222 modify the water uptake capacity with the elimination of glycerol (plasticizer) that
223 occurs during immersion.

$$224 \quad \text{Water uptake capacity (\%)} = \frac{w_2 - w_3}{w_3} \cdot 100 \quad (1)$$

225 Where w_2 (g) is the weight of the bioplastic after the immersion step and w_3 (g) is
226 the weight of the bioplastic after the freeze-drying stage.

227 Finally, soluble matter loss was determined using equation 2.

$$228 \quad \text{Soluble matter loss (\%)} = \frac{w_1 - w_3}{w_1} \cdot 100 \quad (2)$$

229 Where w_1 (g) is the weight of the bioplastic before the immersion step.

230 *2.3.5 Scanning electron microscopy (SEM)*

231 Scanning electron microscopy (SEM) was used in order to compare the
232 microstructure of the bioplastics processed by different treatments before and after
233 the water uptake capacity tests. For this, Orawan et al. (2006) protocol was used,
234 who used it for similar systems with good results. The samples were subjected to a
235 previous sputtering treatment with palladium/gold to improve the electrical
236 conductivity of the bioplastics and improve the quality of the micrographs. Then,
237 the samples were observed using a Zeiss EVO microscope (Germany) at an
238 acceleration voltage of 10 kV and x100 magnification.

239 **2.4 Statistical analysis**

240 In order to confirm a variation of the measurements according to the parameters
241 tested, at least three replicates of each measurement were carried out and the
242 sample standard deviation was calculated with EXCEL (Microsoft public domain).

243

244 **3. Results & Discussion**

245 **3.1 Degree of crosslinking**

246 The degree of crosslinking induced by each of the strengthening actions is shown
247 in Table 1. It is important to mention that the bioplastic processed with a molding
248 temperature of 70 °C and without post-treatment was used as a 0% crosslinking
249 reference, with which the calculated degree of crosslinking of the other samples
250 was compared.

251 **Table 1:** Degree of crosslinking (DC, %) of the different bioplastics: Reference
252 (Ref.), mold temperature increase (130 °C), dehydrothermal treatment (DHT) at 4
253 and 24 h and ultrasound treatment (US) at 5 and 45 min. Different letters show
254 significant differences in the degree of crosslinking of the systems ($p \leq 0.05$).

Sample	DC (%)	
Ref.	-	
130 °C	32.2^a	
DHT	4 h	0.8^b
	24 h	22.5^c
US	5 min	1.9^b
	45 min	19.2^c

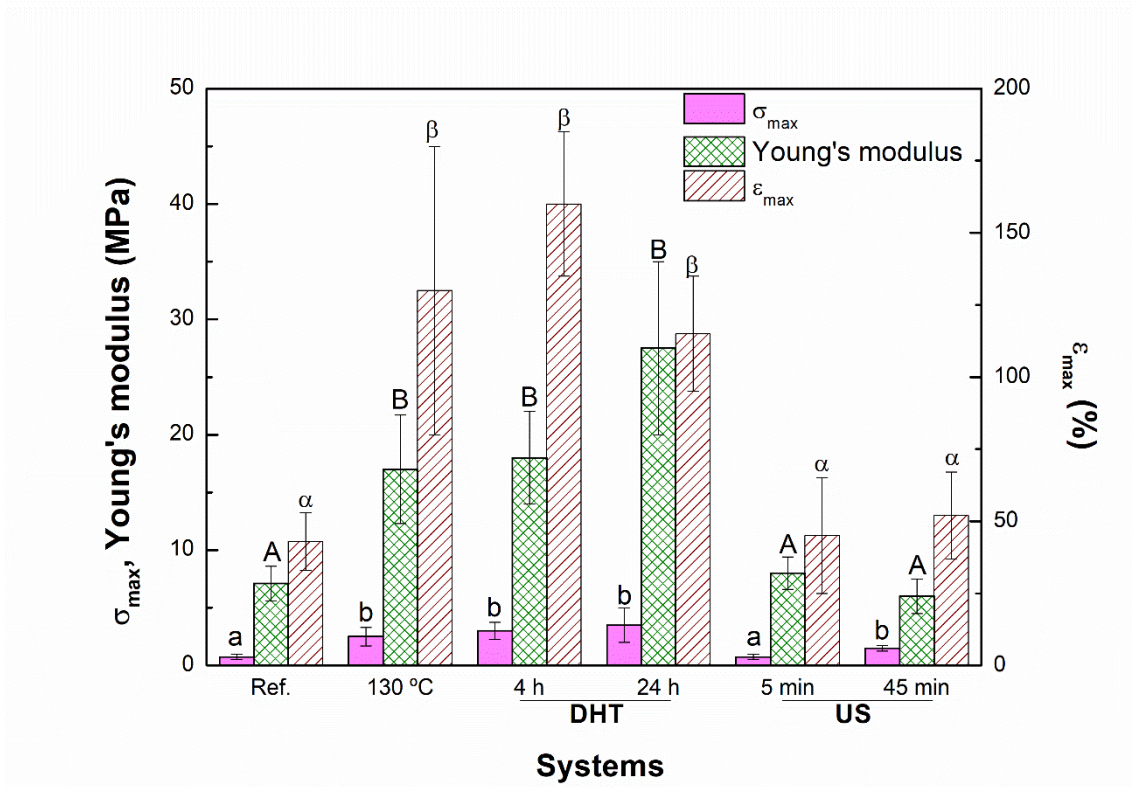
255 As it can be observed, the action that caused the most significant improvement in
256 the degree of crosslinking was the increase in the mold temperature to 130 °C
257 (32.2% more crosslinked than in the reference system). Therefore, it is intuited that
258 more severe processing parameters induce a greater number of covalent bonds in
259 the bioplastics, as anticipated in previous studies (Fernández-Espada et al.,
260 2016a). Moreover, the use of a long-time post-treatment (24 h DHT or 45 min US)
261 also caused a higher degree of crosslinking (22.5 and 19.2%, respectively),
262 although this improvement was not as significant as the increase in mold
263 temperature. On the other hand, at short times, neither of the two post-treatments
264 induced a great degree of crosslinking (0.8% in DHT and 1.9% in US). In this
265 regard, it should be noted that the US treatment needs much less time to cause the
266 same crosslinking as DHT (several minutes instead of several hours). This fact
267 could be decisive in their large-scale manufacture since a shorter processing time
268 can reduce the costs of the product, making it more competitive in the market
269 (Fowler et al., 2006), as long as this shorter processing time does not generate
270 additional costs to the process. Therefore, all the alternatives seem to produce
271 some crosslinking degree, being a greener method than the addition of other
272 chemical substances (i.e. glutaraldehyde) that can produce environmental
273 contamination. However, it is important evaluate the carbon footprint caused for the
274 different physical strengthening methods, since an excess in their use can cause
275 global warming problems.

276 **3.2 Mechanical properties**

277 *3.2.1 Tensile tests*

278 Figure 1 shows the maximum stress (σ_{max}), strain at break (ϵ_{max}) and Young's
279 modulus of the different processed bioplastics. The increase in the mold

280 temperature (130 °C) caused an improvement in σ_{\max} , ϵ_{\max} and Young's modulus.,
 281 as in other previous studies (Fernández-Espada et al., 2016a). This also occurred
 282 when a stage of DHT was added, although without significant differences between
 283 the different treatment times. However, the US treatment did not significantly
 284 improve any of the bioplastic tensile parameters, neither at short nor long times.
 285 These results suggest that a heat treatment (i.e. higher mold temperature or DHT)
 286 improves the mechanical tensile properties of bioplastics, probably due to a greater
 287 strengthening of the bioplastic (increasing both the maximum stress and the strain
 288 at break) through covalent bonds (Álvarez-Castillo et al., 2018; Fernández-Espada
 289 et al., 2016b). However, the US treatment, although it induces a greater degree of
 290 crosslinking than the reference system, can affect the proteins by denaturing them;
 291 leading to weaker bonds (Park et al., 1993).



292

293 **Figure 1:** Maximum stress (σ_{\max}), strain at break (ϵ_{\max}) and Young's modulus
 294 obtained in tensile tests of the different bioplastics (systems): Reference (Ref.),

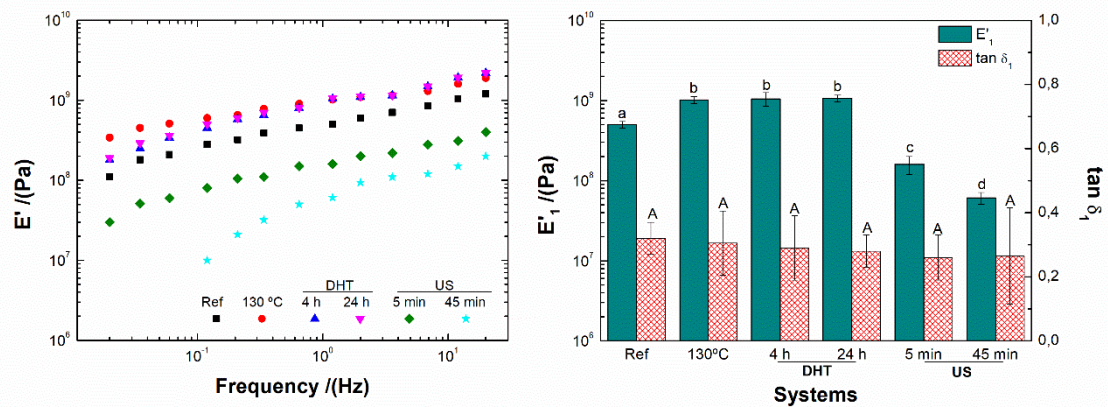
295 mold temperature increase (130 °C), dehydrothermal treatment (DHT) at 4 and 24
296 h and ultrasound treatment (US) at 5 and 45 min. Different letters show significant
297 differences ($p \leq 0.05$).

298

299 *3.2.2 Bending tests*

300 Figure 2 shows the results obtained from the bending tests. In Figure 2A, the
301 evolution of the elastic modulus (E') with the frequency can be observed. All the
302 bioplastics studied showed a dependency of the flexural elastic modulus (E') on the
303 frequency studied range. This means that the properties of the bioplastics vary
304 depending on the force applied and the application time, making it more difficult to
305 predict their behavior. This dependence is higher in bioplastic processed thermally,
306 since its rise is steeper than US processed bioplastics. Thus, it seems that higher
307 tensile parameters lead to less flexural stability. These results may be because the
308 bioplastic, although it supports higher stresses, deforms plastically when a certain
309 force is applied, changing its structure and flexural stability. Similar results were
310 obtained in a previous work (Jiménez-Rosado et al., 2018). On the other hand,
311 Figure 2B shows the elastic modulus and loss tangent at 1 Hz (E'_1 and $\tan \delta_1$,
312 respectively). As in the tensile tests, a higher mold temperature or the incorporation
313 of a thermal stage (DHT) caused an improvement in the flexural strength of the
314 bioplastics. However, the US treatment worsened the elastic modulus of the
315 bioplastics, which was higher when a longer treatment time was applied. These
316 results are consistent with those obtained in the tensile tests, showing that a
317 thermal treatment caused a strengthening of bioplastic bonds, whereas an
318 ultrasound treatment weakened them. As for $\tan \delta_1$, it remained invariant below 1
319 in all the systems analyzed. This reflects the high solid character of the systems,

320 which was not altered by the change in the processing method. This solid
321 character was also observed in previous studies (Fernández-Espada et al., 2016a;
322 Perez-Puyana et al., 2018).



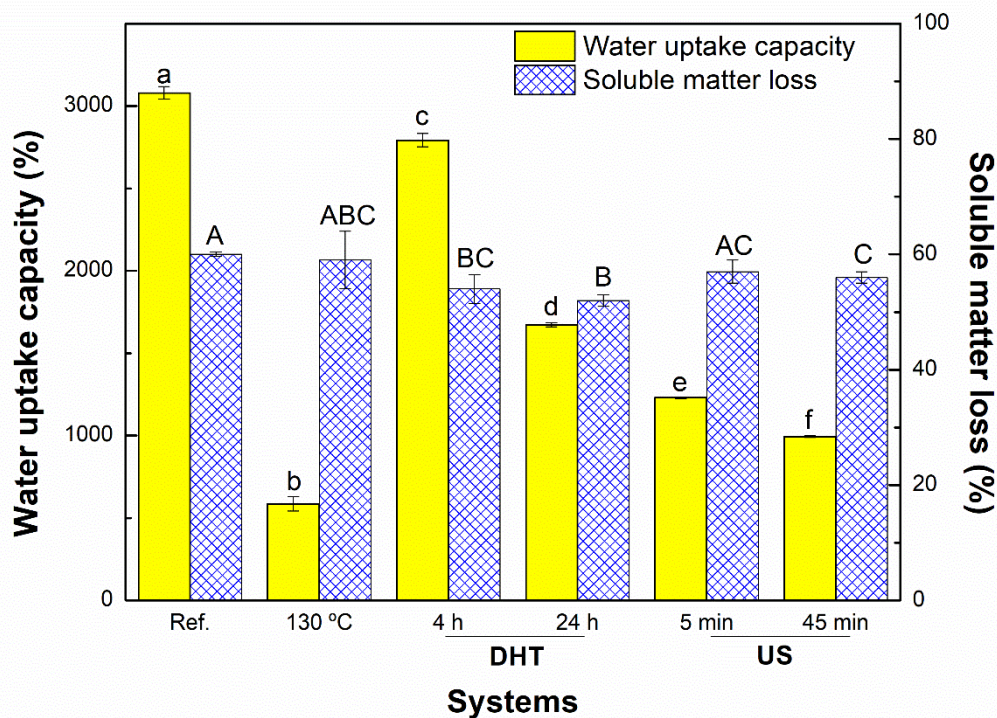
323

324 **Figure 2:** Bending tests of the different processed bioplastics. (A) Elastic modulus
 325 (E') in the entire frequency range and (B) elastic modulus and loss tangent at 1 Hz
 326 (E'_1 and $\tan \delta_1$, respectively). Systems: Reference (Ref.), mold temperature
 327 increase (130 °C), dehydrothermal treatment (DHT) at 4 and 24 h and ultrasound
 328 treatment (US) at 5 and 45 min. Different letters show significant differences ($p \leq$
 329 0.05).

330 If the mechanical properties of these bioplastics are compared with those of
 331 conventional plastics, it can be observed that after thermal strengthening of the
 332 bioplastics have better mechanical properties. In fact, it achieves properties similar
 333 to that of polyethylene or polyvinylchloride (Young's modulus 25 and 35 MPa,
 334 respectively), but not so high as polystyrene (3-3.4 GPa). However, the US
 335 treatment does not improve these properties.

336 **3.3 Water uptake capacity & soluble matter loss**

337 The measurements of water uptake capacity and soluble matter loss are shown in
 338 Figure 3. Considering the soluble matter loss, there were no significant differences
 339 between the systems, where, in all cases, all Gly is lost, due to its hydrophilic
 340 character, and the soluble part of the protein (about 10 wt.%). These results were
 341 similar to those obtained in previous works, where all Gly and part of the protein
 342 were lost (Fernández-Espada et al., 2016b).



343

344 **Figure 3:** Water uptake capacity and soluble matter loss measurements for the
 345 different processed bioplastics (systems): Reference (Ref.), mold temperature
 346 increase (130 °C), dehydrothermal treatment (DHT) at 4 and 24 h and ultrasound
 347 treatment (US) at 5 and 45 min. Different letters show significant differences ($p \leq$
 348 0.05).

349 On the other hand, for the water uptake capacity, there were major differences
 350 between the bioplastics studied. The greatest difference was observed with the
 351 increase in mold temperature, losing the superabsorbent capacity (<1000%) of the
 352 bioplastic. This is due to the greater structuring of the bioplastic while it is
 353 conferred. It creates a more reinforced structure with more difficulty to swell, and
 354 therefore, with less capacity to retain water inside (Fernandez-Espada et al.,
 355 2016a).

356 As for the application of DHT, it also caused a decrease of the bioplastic's water
 357 uptake capacity, which was more significant when longer DHT time was needed.

358 However, the functionality of the bioplastic was not lost (they were
359 superabsorbent). These results show that, although there is a strengthening of the
360 system, improving its mechanical properties, it was not sufficiently consolidated.
361 Consequently, the bioplastic could swell to retain a greater amount of water than in
362 the case of mold temperature change.

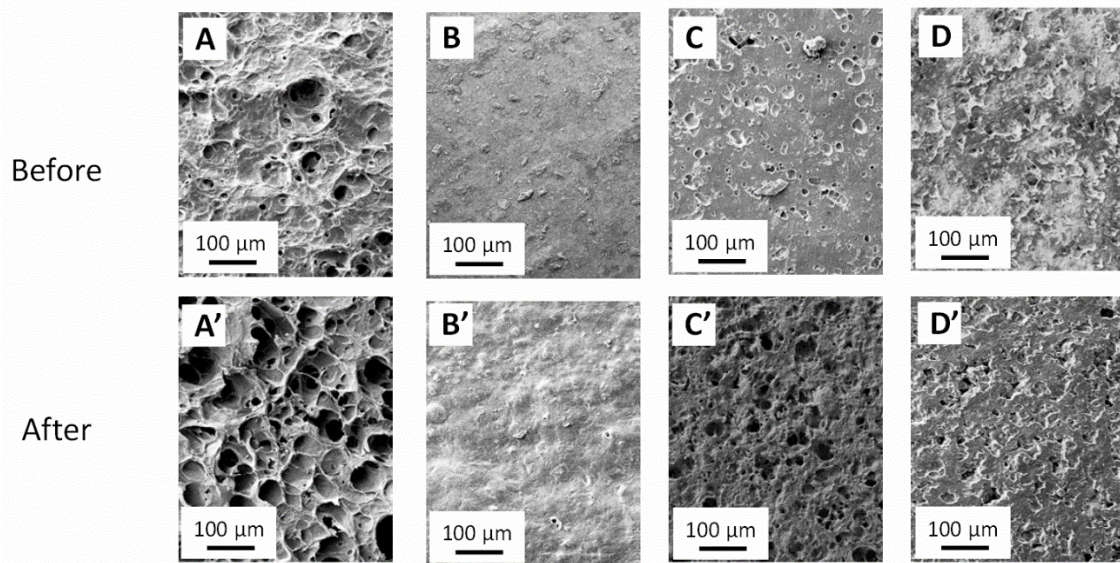
363 The US treatment also worsened the water uptake capacity of the bioplastics,
364 which remained at the limit of being considered superabsorbent. These results are
365 not consistent with those obtained in previous studies (Álvarez-Castillo et al.,
366 2018), since these predicted that the mechanical properties of bioplastics were
367 closely linked to their water uptake capacity, which worsens when the better
368 mechanical properties are presented by the bioplastics. In this case, this prediction
369 is not fulfilled, which may be due to the protein denaturation that was previously
370 intuited. Thus, the protein loses the ability to create hydrogen bonds with water,
371 which worsens its retention capacity.

372 **3.4 Scanning electron microscopy (SEM)**

373 SEM imaging was performed in the different systems studied before and after the
374 water uptake measurements. The micrographs of the bioplastics before (A, B, C
375 and D) and after (A', B', C' and D') the water immersion can be seen in Figure 4.

376 Before water absorption, the different processes performed on the bioplastics had
377 an impact on the microstructure in each case. The reference system (A) was the
378 one with the greatest number of pores, which were also larger than in the rest of
379 the systems. This is due to the lower structuring of the bioplastic when softer
380 processing conditions were used. This lower structuring induced a greater water
381 uptake capacity, with the subsequent swelling and opening of the structure

382 reflected by the increase in the number and size of pores in the microstructure (A').
383 Previous work also shows these results (Fernandez-Espada et al., 2016a).



384

385 **Figure 4:** Microstructure images of the different processed bioplastics obtained by
386 scanning electronic microscopy (reference without modification (A, A'), processed
387 with 130 °C in mold temperature (B, B'), with 24 h dehydrothermal treatment (C, C')
388 and with 45 min ultrasounds treatment (D, D')) before (A, B, C and D) and after (A',
389 B', C' and D') water immersion.

390 On the other hand, any change in the processing method led to a less porous
391 structure (B, C and D), probably due to the reinforcement produced by the
392 crosslinking achieved in these bioplastics. The most solid and compact structure
393 was achieved with the highest mold temperature (B). The tightness obtained
394 implies a lower water absorption (as seen in Section 3.3) and, therefore, no
395 variation in the structure after the immersion (B'). A similar effect took place after
396 performing the DHT post-treatment (C), but with a slight modification of the
397 microstructure with the formation of some pores on it (C'). These results are similar
398 to these obtained by Álvarez-Castillo et al. (2018). As for the bioplastic submitted
399 to US (D), it can be seen that the ultrasound caused a modification of the

400 microstructure respect to the reference system, presenting a large number of small
401 pores that did not vary after the water immersion (D'). This was surely due to the
402 denaturation discussed above.

403

404 **4. Conclusions**

405 Soy protein-based bioplastics processed by injection molding have demonstrated
406 their potential to replace conventional plastics. However, suitable processing
407 conditions are extremely important to reach the required properties for these
408 bioplastics.

409 Thus, thermal treatments (both higher mold temperature and dehydrothermal
410 treatment) improve the mechanical properties of the bioplastics (specially the
411 Young's modulus and strain at break). Nevertheless, higher mold temperature
412 leads to bioplastics more compact and without superabsorbent capacity, while
413 dehydrothermal treatment decreases slowly this capacity, allowing bioplastics to
414 still have superabsorbent capacity. Thus, the first ones could be used in
415 applications as packaging, and the second ones could be used in hygienic
416 applications.

417 On the other hand, ultrasound treatment leads to a change in the structure of
418 bioplastic with a decrease in the water uptake capacity and worse mechanical
419 properties. In this way, however a greater crosslinking normally results in an
420 improvement of the mechanical properties and a loss of the water uptake capacity,
421 this is only true if the microstructure of the materials is not altered too much.

422 Finally, this work opens the possibility of creating sustainable bioplastics
423 competitive with commercial ones, making the consumption of plastics cleaner
424 without creating pollution problems. However, further study is necessary where

425 combinations between the different strengthening used (i.e. mold temperature in
426 addition to post-treatment), as well as the use of other intermediate temperatures
427 and times, would be evaluated.

428 **Acknowledgements**

429 This work is part of a project funded by “*Ministerio de Economía y Competitividad*”
430 (Ref. RTI2018-097100-B-C21), the authors gratefully acknowledge their financial
431 support. The authors also acknowledge “*Ministerio de Educación y Formación*
432 *Profesional*” for the PhD grant of M. Jiménez-Rosado (FPU2017/01718). The
433 authors also thank CITIUS for granting access and their assistance with the
434 Microscopy services.

435

436 **References**

437 AENOR, 2012. UNE-EN ISO 527-2:2012. Plásticos. Determinación de las
438 propiedades en tracción. Parte 2: Condiciones de ensayo de plásticos para
439 moldeo y extrusión.

440 Ahmed, T., Shahid, M., Azeem, F., Rasul, I., Shah, A.A., Noman, M., Hameed, A.,
441 Manzoor, N., Manzoor, I., Muhammad, S., 2018. Biodegradation of plastics:
442 current scenario and future prospects for environmental safety. *Environ. Sci.*
443 *Pollut. Res.* 25, 7287–7298. <https://doi.org/10.1007/s11356-018-1234-9>

444 Álvarez-Castillo, E., Bengoechea, C., Rodríguez, N., Guerrero, A., 2019.
445 Development of green superabsorbent materials from a by-product of the meat
446 industry. *J. Clean. Prod.* 223, 651–661.
447 <https://doi.org/10.1016/j.jclepro.2019.03.055>

448 Álvarez-Castillo, E., Del Toro, A., Aguilar, J.M., Guerrero, A., Bengoechea, C.,

449 2018. Optimization of a thermal process for the production of superabsorbent
450 materials based on a soy protein isolate. *Ind. Crops Prod.* 125, 573–581.
451 [https://doi.org/https://doi.org/10.1016/j.indcrop.2018.09.051](https://doi.org/10.1016/j.indcrop.2018.09.051)

452 Álvarez-Chávez, C.R., Edwards, S., Moure-Eraso, R., Geiser, K., 2012.
453 Sustainability of bio-based plastics: general comparative analysis and
454 recommendations for improvement. *J. Clean. Prod.* 23, 47–56.
455 <https://doi.org/10.1016/j.jclepro.2011.10.003>

456 Carrington, D., 2019. People eat at least 50,000 plastic particles a year, study finds
457 [WWW Document]. *Guard.* URL
458 [https://www.theguardian.com/environment/2019/jun/05/people-eat-at-least-](https://www.theguardian.com/environment/2019/jun/05/people-eat-at-least-50000-plastic-particles-a-year-study-finds)
459 [50000-plastic-particles-a-year-study-finds](https://www.theguardian.com/environment/2019/jun/05/people-eat-at-least-50000-plastic-particles-a-year-study-finds)

460 Confente, I., Scarpi, D., Russo, I., 2019. Marketing a new generation of bio-plastics
461 products for a circular economy: The role of green self-identity, self-congruity,
462 and perceived value. *J. Bus. Res.*
463 <https://doi.org/10.1016/j.jbusres.2019.10.030>

464 Cuadri, A.A., Bengoechea, C., Romero, A., Guerrero, A., 2016. A natural-based
465 polymeric hydrogel based on functionalized soy protein. *Eur. Polym. J.* 85,
466 164–174. <https://doi.org/10.1016/j.eurpolymj.2016.10.026>

467 Cuadri, A.A., Romero, A., Bengoechea, C., Guerrero, A., 2017. Natural
468 superabsorbent plastic materials based on a functionalized soy protein. *Polym.*
469 *Test.* 58, 126–134. <https://doi.org/10.1016/j.polymertesting.2016.12.024>

470 Derraik, J.G.B., 2002. The pollution of the marine environment by plastic debris: a
471 review. *Mar. Pollut. Bull.* 44, 842–52.

472 Ellen MacArthur Foundation, 2016. The new plastics economy: Rethinking the
473 future of plastics. World Economic Forum, New York.

474 European Bioplastics, 2019. Commission's Circular Economy Proposal leaves
475 room for more ambitious actions on bio-industries such as bioplastics [WWW
476 Document]. URL [https://www.european-bioplastics.org/commissions-circular-](https://www.european-bioplastics.org/commissions-circular-economy-proposal-leaves-room-for-more-ambitious-actions-on-bio-industries-such-as-bioplastics/)
477 [economy-proposal-leaves-room-for-more-ambitious-actions-on-bio-industries-](https://www.european-bioplastics.org/commissions-circular-economy-proposal-leaves-room-for-more-ambitious-actions-on-bio-industries-such-as-bioplastics/)
478 [such-as-bioplastics/](https://www.european-bioplastics.org/commissions-circular-economy-proposal-leaves-room-for-more-ambitious-actions-on-bio-industries-such-as-bioplastics/)

479 Fernández-Espada, L., Bengoechea, C., Cordobés, F., Guerrero, A., 2016a.
480 Thermomechanical properties and water uptake capacity of soy protein-based
481 bioplastics processed by injection molding. *J. Appl. Polym. Sci.* 133, 43524.
482 <https://doi.org/10.1002/app.43524>

483 Fernández-Espada, L., Bengoechea, C., Cordobés, F., Guerrero, A., 2016b.
484 Protein/glycerol blends and injection-molded bioplastic matrices: Soybean
485 versus egg albumen. *J. Appl. Polym. Sci.* 133, 42980.
486 <https://doi.org/10.1002/app.42980>

487 Flieger, M., Kantorová, M., Prell, A., \Rezanka, T., Votruba, J., 2003.
488 Biodegradable plastics from renewable sources. *Folia Microbiol. (Praha)*. 48,
489 27. <https://doi.org/10.1007/BF02931273>

490 Fowler, P.A., Hughes, J.M., Elias, R.M., 2006. Biocomposites: technology,
491 environmental credentials and market forces. *J. Mech. Behav. Biomed. Mater.*
492 86, 1781–1789. <https://doi.org/10.1002/jsfa.2558>

493 Gamero, S., Jiménez-Rosado, M., Romero, A., Bengoechea, C., Guerrero, A.,
494 2019. Reinforcement of Soy Protein-Based Bioplastics Through Addition of
495 Lignocellulose and Injection Molding Processing Conditions. *J. Polym.*

496 Environ. 27, 1285–1293. <https://doi.org/10.1007/s10924-019-01430-1>

497 Gerrard, J.A., 2002. Protein–protein crosslinking in food: methods, consequences,
498 applications. Trends Food Sci. Technol. 13, 391–399.
499 [https://doi.org/https://doi.org/10.1016/S0924-2244\(02\)00257-1](https://doi.org/https://doi.org/10.1016/S0924-2244(02)00257-1)

500 Ghasri, M., Bouhendi, H., Kabiri, K., Zohuriaan-Mehr, M.J., Karami, Z., Omidian,
501 H., 2019. Superabsorbent polymers achieved by surface cross linking of
502 poly(sodium acrylate) using microwave method. Iran. Polym. J. 28, 539–548.
503 <https://doi.org/10.1007/s13726-019-00722-6>

504 Giosafatto, C., Al-Asmar, A., D’Angelo, A., Roviello, V., Esposito, M., Mariniello, L.,
505 2018. Preparation and Characterization of Bioplastics from Grass Pea Flour
506 Cast in the Presence of Microbial Transglutaminase. Coatings 8, 435.
507 <https://doi.org/10.3390/coatings8120435>

508 Gironi, F., Piemonte, V., 2011. Bioplastics and Petroleum-based Plastics:
509 Strengths and Weaknesses. Energy Sources Part A: Re, 1949–1959.
510 <https://doi.org/10.1080/15567030903436830>

511 Jayasooriya, S.D., Bhandari, B.R., Torley, P., D’Arcy, B.R., 2004. Effect of High
512 Power Ultrasound Waves on Properties of Meat: A Review. Int. J. Food Prop.
513 7, 301–319. <https://doi.org/10.1081/JFP-120030039>

514 Jiménez-Rosado, M., Pérez-Puyana, V., Cordobés, F., Romero, A., Guerrero, A.,
515 2018. Development of soy protein-based matrices containing zinc as
516 micronutrient for horticulture. Ind. Crops Prod. 121, 345–351.
517 <https://doi.org/10.1016/j.indcrop.2018.05.039>

518 Jiménez-Rosado, M., Zarate-Ramírez, L.S., Romero, A., Bengoechea, C., Partal,

519 P., Guerrero, A., 2019. Bioplastics based on wheat gluten processed by extrusion.
520 J. Clean. Prod. 239, 117994. <https://doi.org/10.1016/j.jclepro.2019.117994>

521 Julavittayanukul, O., Benjakul, S., Visessanguan, W., 2006. Effect of phosphate
522 compounds on gel-forming ability of surimi from bigeye snapper (*Priacanthus*
523 *tayenus*). Food Hydrocoll. 20, 1153–1163.
524 <https://doi.org/10.1016/j.foodhyd.2005.12.007>

525 Karana, E., 2012. Characterization of 'natural' and 'high-quality' materials to
526 improve perception of bio-plastics. J. Clean. Prod. 37, 316–325.
527 <https://doi.org/10.1016/j.jclepro.2012.07.034>

528 Karki, B., 2009. Use of high-power ultrasound during soy protein production and
529 study of its effect on functional properties of soy protein isolate. Iowa State
530 University, Digital Repository, Ames. [https://doi.org/10.31274/etd-180810-](https://doi.org/10.31274/etd-180810-3395)
531 [3395](https://doi.org/10.31274/etd-180810-3395)

532 Magnay, J.L., Nevatte, T.M., Dhingra, V., O'Brien, S., 2010. Menstrual blood loss
533 measurement: validation of the alkaline hematin technique for feminine
534 hygiene products containing superabsorbent polymers. Fertil. Steril. 94, 2742–
535 2746. <https://doi.org/10.1016/j.fertnstert.2010.03.061>

536 Markwell, M.A.K., Haas, S.M., Bieber, L.L., Tolbert, N.E., 1978. A modification of
537 the Lowry procedure to simplify protein determination in membrane and
538 lipoprotein samples. Anal. Biochem. 87, 206–210.
539 [https://doi.org/https://doi.org/10.1016/0003-2697\(78\)90586-9](https://doi.org/10.1016/0003-2697(78)90586-9)

540 Marquié, C., 2001. Chemical Reactions in Cottonseed Protein Cross-Linking by
541 Formaldehyde, Glutaraldehyde, and Glyoxal for the Formation of Protein Films
542 with Enhanced Mechanical Properties. J. Agric. Food Chem. 49, 4676–4681.

543 <https://doi.org/10.1021/jf0101152>

544 Mo, X., Sun, X.S., Wang, Y., 1999. Effects of molding temperature and pressure on
545 properties of soy protein polymers. *J. Appl. Polym. Sci.* 73, 2595–2602.
546 [https://doi.org/10.1002/\(SICI\)1097-4628\(19990923\)73:13<2595::AID-
547 APP6>3.0.CO;2-I](https://doi.org/10.1002/(SICI)1097-4628(19990923)73:13<2595::AID-APP6>3.0.CO;2-I)

548 Mohammadhosseini, H., Tahir, M.M., 2018a. Durability performance of concrete
549 incorporating waste metalized plastic fibres and palm oil fuel ash. *Constr.*
550 *Build. Mater.* 180, 92–102. <https://doi.org/10.1016/j.conbuildmat.2018.05.282>

551 Mohammadhosseini, H., Tahir, M.M., 2018b. Production of sustainable fibre-
552 reinforced concrete incorporating waste chopped metallic film fibres and palm
553 oil fuel ash. *Sādhanā* 43, 156. <https://doi.org/10.1007/s12046-018-0924-9>

554 Mohammadhosseini, H., Tahir, M.M., Sam, A.R.M., 2018. The feasibility of
555 improving impact resistance and strength properties of sustainable concrete
556 composites by adding waste metalized plastic fibres. *Constr. Build. Mater.*
557 169, 223–236. <https://doi.org/10.1016/j.conbuildmat.2018.02.210>

558 Nnadi, F., Brave, C., 2011. Environmentally friendly superabsorbent polymers for
559 water conservation in agricultural lands. *J. Soil Sci. Environ. Manag.* 2, 206–
560 211.

561 Park, K., Shalaby, W.S.W., Park, H., 1993. *Biodegradable hydrogels for drug*
562 *delivery*. CRC Press, Boca Raton.

563 Patel, A. V, Panchal, T.M., Rudakiya, D., Gupte, A., Patel, J. V, 2016. Fabrication
564 of bio-plastics from protein isolates and its biodegradation studies. *Int. J.*
565 *Chem. Sci. Technol.* 1, 1–13. <https://doi.org/18.04.001/20160104>

566 Perez-Puyana, V., Felix, M., Romero, A., Guerrero, A., 2018. Development of eco-
567 friendly biodegradable superabsorbent materials obtained by injection
568 moulding. *J. Clean. Prod.* 198, 312–319.
569 <https://doi.org/https://doi.org/10.1016/j.jclepro.2018.07.044>

570 Perez, V., Felix, M., Romero, A., Guerrero, A., 2016. Characterization of pea
571 protein-based bioplastics processed by injection moulding. *Food Bioprod.*
572 *Process.* 97, 100–108. <https://doi.org/10.1016/j.fbp.2015.12.004>

573 Russo, I., Confente, I., Scarpi, D., Hazen, B.T., 2019. From trash to treasure: The
574 impact of consumer perception of bio-waste products in closed-loop supply
575 chains. *J. Clean. Prod.* 218, 966–974.
576 <https://doi.org/10.1016/j.jclepro.2019.02.044>

577 Saenghirunwattana, P., Noomhorm, A., Rungsardthong, V., 2014. Mechanical
578 properties of soy protein based “green” composites reinforced with surface
579 modified cornhusk fiber. *Ind. Crops Prod.* 60, 144–150.
580 <https://doi.org/10.1016/j.indcrop.2014.06.010>

581 Song, J.H., Murphy, R.J., Narayan, R., Davies, G.B.H., 2009. Biodegradable and
582 compostable alternatives to conventional plastics. *Philos. Trans. R. Soc. Lond.*
583 *B. Biol. Sci.* 364, 2127–2139. <https://doi.org/10.1098/rstb.2008.0289>

584 Thakur, V.K., 2017. *Soy-Based Bioplastics*. Smithers Information Limited,
585 Shawbury.

586 Tummala, P., Liu, W., Drzal, L.T., Mohanty, A.K., Misra, M., 2006. Influence of
587 Plasticizers on Thermal and Mechanical Properties and Morphology of Soy-
588 Based Bioplastics. *Ind. Eng. Chem. Res.* 45, 7491–7496.
589 <https://doi.org/10.1021/ie060439l>

- 590 Verbeek, R.C.J., van den Berg, L.E., 2010. Extrusion Processing and Properties of
591 Protein-Based Thermoplastics. *Macromol. Mater. Eng.* 295, 10–21.
592 <https://doi.org/doi:10.1002/mame.200900167>
- 593 Zárate-Ramírez, L.S., Romero, A., Martínez, I., Bengoechea, C., Partal, P.,
594 Guerrero, A., 2014. Effect of aldehydes on thermomechanical properties of
595 gluten-based bioplastics. *Food Bioprod. Process.* 92, 20–29.
596 <https://doi.org/10.1016/j.fbp.2013.07.007>
- 597 Zhuang, H., Barth, M.M., Cisneros-Zevallos, L., 2014. Modified Atmosphere
598 Packaging for Fresh Fruits and Vegetables, in: *Innovations in Food Packaging*.
599 Elsevier, pp. 445–473. <https://doi.org/10.1016/B978-0-12-394601-0.00018-7>