

# OPTIMAL TEMPERATURE RANGE FOR DETERMINING MAGNETOCALORIC MAGNITUDES FROM HEAT CAPACITY

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## ABSTRACT

The determination of the magnetocaloric magnitudes (specific magnetic entropy change,  $\Delta s_M$ , and adiabatic temperature change,  $\Delta T_{ad}$ ) from heat capacity ( $c_H$ ) measurements requires measurements performed at very low temperatures (~0 K) or data extrapolation when the low temperature range is unavailable. In this work we analyze the influence on the calculated  $\Delta s_M$  and  $\Delta T_{ad}$  of the usually employed linear extrapolation of  $c_H$  from the initial measured temperature down to 0 K. Numerical simulations have been performed using the Brillouin equation of state, the Debye model and the Fermi electron statistics to reproduce the magnetic, lattice and electronic subsystems, respectively. It is demonstrated that is not necessary to reach experimentally temperatures very close to 0 K due to the existence of certain starting temperatures of the experiments, the same for  $\Delta s_M$  and  $\Delta T_{ad}$ , that minimize the error of the results. A procedure is proposed to obtain the experimental magnitudes of  $\Delta s_M$  and  $\Delta T_{ad}$  with a minimum error from  $c_H$  data limited in temperature. It has been successfully applied to a GdZn alloy after comparing with results derived from magnetization measurements.

## **1. INTRODUCTION**

The application of a magnetic field in adiabatic conditions to a magnetic material causes a variation of the sample temperature ( $\Delta T_{ad}$ ) due to the coupling between the lattice and magnetic subsystems. This effect is known as the magnetocaloric effect (MCE) [1,2]. Alternatively, the MCE can be quantified as the specific magnetic entropy change ( $\Delta s_M$ ) during the variation of an applied magnetic field in an isothermal process. This effect was widely used to achieve ultralow temperatures (below 1 K) making use of paramagnetic salts [3]. Nowadays, the interest on MCE is increasing due to the possibility to perform magnetic refrigerators at room temperature. This technology has been shown as an energy efficient and environmental friendly (due to the absence of gasses responsible for greenhouse effect and ozone depletion) alternative to the conventional systems [4,5].

In order to optimize the material performances to be applied in a refrigerator device, a basic step is an accurate characterization of the magnetocaloric magnitudes. In isothermal conditions, the  $\Delta s_M$  for a magnetic field change  $\Delta H$  is obtained using the Maxwell relations [6] as:

$$\Delta s_M(T, \Delta H) = \mu_0 \int_{H_I}^{H_F} \left(\frac{\partial \sigma}{\partial T}\right)_H dH$$
<sup>(1)</sup>

where  $H_I$  and  $H_F$  are the initial and final magnetic fields, respectively, T is the temperature,  $\sigma$  is the specific magnetization and  $\mu_0$  is the magnetic permeability of the vacuum (in this work, equations and magnitudes are expressed in the SI).

On other hand, making use of the definition of the specific heat capacity at constant magnetic field ( $c_H$ ) and taking into the Maxwell relations and the adiabatic condition,  $\Delta T_{ad}$  can be obtained as:

$$\Delta T_{ad}(T, \Delta H) = -\mu_0 \int_{H_I}^{H_F} \frac{T}{c_H} \left(\frac{\partial \sigma}{\partial T}\right)_H dH.$$
 (2)

From equations (1) and (2) it can be deduced that the MCE is maximum when there is an abrupt change in magnetization with respect to the temperature, i.e. in the region close to a magnetic transition.

Previous expression require the acquisition of magnetization data as a function of temperature and field, for  $\Delta s_M$ , and besides this,  $c_H$  measurements as a function of temperature and field for determining  $\Delta T_{ad}$ . On the other hand, the two fundamental magnetocaloric magnitudes, can be obtained using only calorimetric data [7,8]. For a constant magnetic field, the specific total entropy of the system ( $s_H$ ) can be obtained from heat capacity data through:

$$s_{H}(T) = \int_{0}^{T} \frac{c_{H}}{T} dT + s_{0 K, H}$$
(3)

where  $s_{0 K,H}$  is the entropy at 0 K for a magnetic field *H*.  $\Delta s_M$  and  $\Delta T_{ad}$  are obtained from equation (3) as:

$$\Delta s_M(T, \Delta H) = [s_{H_F}(T) - s_{H_I}(T)]_T \tag{4}$$

$$\Delta T_{ad}(T,\Delta H) = [T_{H_F}(s) - T_{H_I}(s)]_s \tag{5}$$

where in order to calculate  $\Delta T_{ad}$ , the entropy curves  $s_H(T)$  have to be inverted as  $T_H(s)$ .

In both cases, equations (1 and 2) and equations (4 and 5), the heat capacity measurements are needed to obtain  $\Delta T_{ad}$ , although in the first case, it is also necessary to have the magnetization data and, in the second case, we have to be able to calculate *s*<sub>0</sub>  $_{K,H}$  and to reach temperatures close to 0 K (see equation (3)).

Concerning the calculus of the MCE from calorimetric measurements, the  $s_0 _{K,H}$  term would not affect  $\Delta s_M$  if it is assumed that, in a condensed system, it is field independent.

However, for  $\Delta T_{ad}$ , its contribution is not zero but it is assumed small [7], and usually this term is neglected in the calculus of both magnitudes. In the case that temperatures close to 0 K could not be reached, the approximated calculus will be considerably affected (some kind of assumption must be done for the missing data range, e.g. a linear behavior of  $c_H$ ). The experimental limitations can be ascribed to limitations of the experimental setup (e.g. the sample is cooled down using liquid N<sub>2</sub>) or to the difficulties to measure  $c_H$  in a large temperature range (e.g. due to stability limitations of the grease usually employed to attach the sample to the calorimetric chip).

In the present work, the influence of assuming a linear behavior of the heat capacity from the initial temperature measured down to 0 K (assuming  $c_H(0 \text{ K})=0$ ) on the calculated magnetocaloric magnitudes will be discussed. Numerical simulations have been performed using the Brillouin equation of state, the Debye model and the Fermi electron statistics to reproduce the magnetic, lattice and electronic subsystems, respectively. The obtained results from the simulations allow us to propose a procedure to minimize the associated error in experimental  $\Delta s_M$  and  $\Delta T_{ad}$  data. In order to check the validity of the proposed procedure, it has been applied to a single phase GdZn alloy. The results are compared to calculations derived from magnetization data.

## 2. EXPERIMENTAL TECHNIQUES AND MODELS

For both experimental data as well as for numerical simulations, the total entropy of the system has been numerically calculated from heat capacity data approximating equation (3) as [7]:

$$s_{H}^{ap}(T) = \frac{1}{2}c_{H}(T_{ini}) + \int_{T_{ini}}^{T} \frac{c_{H}}{T} dT$$
<sup>(6)</sup>

Where  $s_H^{ap}$  is the approximated entropy at a constant magnetic field (the superscript 'ap' will also denote the different magnitudes calculated from this data),  $c_H$  was measured at constant magnetic field, with  $T_{ini}$  as the initial temperature and the zero temperature entropy is not considered. In this expression, it is assumed a linear extrapolation from  $T_{ini}$  down to 0 K for  $c_H$  (assuming  $c_H(0 \text{ K})=0$ ) as proposed by Pecharsky et al. [7] for measurements close to 0 K.

Theoretically, the heat capacity of the magnetic material can be expressed as the sum of the magnetic, lattice and electronic subsystems contributions. To simulate the magnetic subsystem, the Brillouin equation of state has been considered [9], where the heat capacity of the magnetic subsystem ( $C_M$ ) is calculated according to [10]:

$$C_{M} = N_{m}K_{B}T\left(\partial\left[ln\left(\frac{\sinh\left(\frac{2J+1}{2J}x\right)}{\sinh\left(\frac{1}{2J}x\right)}\right) - xB_{J}(x)\right]/\partial T\right)_{H}$$
(7)

where  $B_J(x)$  is the Brillouin function,  $x=\mu_0g\mu_BJH^*/k_BT$ ,  $H^*$  is the total field (considered as the applied magnetic field plus the molecular field), g is the spectroscopic splitting factor,  $\mu_B$  is the Bohr magneton, J is the total angular momentum quantum number and  $N_m$  is the number of magnetic atoms. Although the Brillouin equation of state is a mean field approximation that does not predict the correct critical exponents for certain materials and it also presents some limitations at low temperatures due to not consider spin waves. Nevertheless, it is profusely used as a simple model for the simulation of magnetocaloric materials and, as it will be argued below, these mentioned limitations do not affect the main conclusions of this work: the existence of an optimal initial temperature for the lower limit of integration of  $c_H(T_{inl}opt)$  and the procedure to identify it from experimental measurements. It has to be noted that the use of different thermomagnetic equations of state will produce different values of  $T_{ini}^{opt}$ . The lattice contribution ( $C_l$ ) has been considered assuming the Debye model for which [9]:

$$C_l = 9Nk_B \left(\frac{T}{\theta_D}\right)^3 \int_0^{\frac{\theta_D}{T}} \frac{x^4 e^x}{(e^x - 1)^2} \mathrm{d}x \tag{8}$$

where *N* is the number of particles,  $k_B$  is the Boltzmann constant and  $\theta_D$  is the Debye temperature.

For the electronic subsystem, the Fermi-Dirac statistics [9] gives for the heat capacity (*Ce*):

$$C_e = \frac{2}{3}\pi^2 k_B^2 V D(E_F) T \approx \gamma T \tag{9}$$

where *V* is the molar volume and  $D(E_F)$  is the electron density of states at the Fermi level  $E_F$ . Gadolinium has been considered as the model material for the simulations as it is the well-known reference magnetocaloric material for room temperature applications with a ferro-paramagnetic transition, for which the main parameters are J=7/2,  $T_C=293$ K,  $\theta_D=163$  K and  $\gamma=6.4$  mJ mol<sup>-1</sup> K<sup>-2</sup> [11].

The single phase GdZn alloy was prepared by induction melting. Its structural and magnetic characterization can be found in [12]. GdZn presents the advantages of a simpler magnetic transition than pure Gd (with a spin reorientation transition close to the ferro-paramangetic transition [13,14]). Moreover, Gd behavior can be easily modified by impurities [15] and it is easily oxidated, while GdZn does not present such problems. The heat capacity and magnetization curves have been performed in a commercial Physical Property Measurement System from Quantum Design in the temperature range of 200–400 K for magnetic fields up to 2 T.

## 3. **RESULTS AND DISCUSSIONS**

#### **3.1 SIMULATIONS**

The simulated specific heat capacity  $(c_H)$  data of Gd at various magnetic fields are presented in figure 1. Using these data, the specific total entropy of the system  $(s_H)$  was calculated (inset of figure 1) according to equation (6) from 0 K. Figure 2 shows the calculated specific magnetic entropy change curves ( $\Delta s_M^{ap}$ ) for  $\mu_0 \Delta H=2$  T ( $H_I=0$  in this work) using equation (6) starting from differentinitial temperatures ( $T_{ini}$ ). It is observed that each curve differs from the curve starting integration at 0 K (denoted as *complete* curve from now) in a constant value which depends on the magnetic field change. As the initial temperature of integration increases, it can be observed that a nonmonotonous tendency exists. The inset of figure 2 shows the differences of the peak between the approximated magnetic entropy change curve<sup>*p*</sup> ( $\Delta s_M^{ap,pk}$ ) with respect to the complete curve one  $(\Delta s_M^{pk})$ . Besides a flat region close to 0 K, there are two values of the initial temperature  $(T_{ini}^{opt})$ , for which the  $\Delta s_M^{ap}$  values are coincident with those of the complete curve (marked with arrows in the inset of figure 2). For practical purposes the most useful optimal initial temperature would be the highest, as the necessity to achieve temperatures close to zero is drastically avoided. From now, we focus only on the highest  $T_{ini}^{opt}$ . If we consider the relation between the complete entropy,  $s_H$  (equation (6) starting from 0 K), and the approximated entropy,  $s_H^{ap}$  (equation (6)):

$$s(T) = \int_0^T \frac{c_H}{T} dT = s_H^{ap}(T) - \frac{1}{2}c_H(T_{\text{ini}}) + \int_0^{T_{\text{ini}}} \frac{c_H}{T} dT = s_H^{ap}(T) + \xi_H(T_{ini})$$
(10)

where the parameter  $\xi_{\rm H}$  depends on *H* and *T*<sub>*ini*</sub>. For any initial temperature, the relation between the approximate magnetic entropy change and the complete one is:

$$\Delta s_{M} = \Delta s_{M}^{ap} + [\xi_{H}(T_{ini}) - \xi_{0}(T_{ini})]$$
<sup>(11)</sup>

where the condition for the optimal temperature is:

$$\xi_H(T_{ini}^{opt}) = \xi_0(T_{ini}^{opt}) \tag{12}$$

This implies that the shift in the total entropy is the same for both magnetic fields. This condition is equivalent to:

$$\frac{1}{2}\Delta c(T_{ini}^{opt}) - \int_0^{T_{ini}^{opt}} \frac{\Delta c}{T} dT = 0$$
<sup>(13)</sup>

with  $\Delta c = c_H - c_0$ . This constitutes the formal definition of  $T_{ini}^{opt}$ . It is worth mentioning that the fulfilment of condition (13) is independent of the model used (Brillouin function in our study).

Figure 3 shows the approximated adiabatic temperature change curves ( $\Delta T_{ad}^{ap}$ ) from different values of the initial temperature of integration using equation (5). Unlike for the  $\Delta s_M{}^{ap}$  data, the differences with respect to the complete curve are not constant and depend on the temperature. However, as for the  $\Delta s_M{}^{ap}$  case, it can be observed some initial temperaturevalues for which the differences with respect to the completed curve (integration performed from 0 K)are zero (the differences of the peak of  $\Delta T_{ad}{}^{ap}$  with respect to the complete curve are shown in the inset of figure 3). These optimal initial temperatures for  $\Delta T_{ad}{}^{ap}$  are the same found for  $\Delta s_M{}^{ap}$ . To demonstrate this coincidence, we consider the definitions of both  $\Delta T_{ad}$  and  $\Delta T_{ad}{}^{ap}$ :

$$\Delta T_{ad}(T,s) = [T_H(s_H) - T_0(s_0)]_s$$
(14)

$$\Delta T_{ad}^{ap}(T, s^{ap}) = [T_H^{ap}(s_H^{ap}) - T_0^{ap}(s_0^{ap})]_{s^{ap}}$$
(15)

Where we establish the equality at a certain temperature  $T=T_0(s)=T_0^{ap}(s^{ap})$  and from the inverse of equation (10):

$$T_H^{ap}\left(s_H^{ap}\right) = T_H\left(s_H - \xi_H(T_{ini})\right) \tag{16}$$

Therefore, as for  $T_{ini}^{opt}$  equation (12) holds and the displacements of both approximated curves are the same in the entropy axis with respect to the complete curves, the change

between temperatures remains constant and  $\Delta T_{ad}^{ap}(T) = \Delta T_{ad}(T)$ . However, when  $T_{ini}$  is different to  $T_{ini}^{opt}$ , the displacements in entropy axis of the approximated curves differ and the temperature change is not preserved. Figure 4 illustrates the calculus of the different  $\Delta T_{ad}^{ap}$  values at  $T=T_{peak}$ : a) shows the procedure when  $T_{ini}=0$  K (corresponding to the complete curve) b) corresponds to  $T_{ini}=T_{ini}^{opt}$  (211.5 K) and c) uses  $T_{ini}=141$  K (a value below  $T_{ini}^{opt}$ ). As observed when  $\xi_{\rm H}(T_{ini}^{opt}) \neq \xi_0(T_{ini}^{opt})$ ,  $\Delta T_{ad}^{ap}(T) \neq \Delta T_{ad}(T)$ . Figure 5 shows the  $\Delta T_{ad}^{ap}(T) - \Delta T_{ad}(T)$  for several initial temperatures at a magnetic field change of 2 T. It can be observed that for a curve with  $T_{ini}$  different to  $T_{ini}^{opt}$ , the differences with respect to the complete curve increases as temperature increase, while for  $T_{ini}=T_{ini}^{opt}$  the differences are zero for all the temperature range. The continuous dependence of  $\Delta T_{ad}^{ap}(T_{ini}) - \Delta T_{ad}(T_{ini})$  is also represented in figure 5 (dotted line) to show the followed trend.

With respect to the field dependence of the analysis, figure 6 shows the field and temperature dependence of  $(\Delta s_M{}^{ap,pk}-\Delta s_M{}^{pk})/\Delta s_M{}^{pk}$ . It can be observed that the shape of the temperature dependence of this magnitude is not affected by field, although the position of  $T_{ini}^{opt}$  is slightly shifted to higher temperatures with increasing field, varying linearly at a rate of 2.1 K/T (inset of figure 5). The shape of the  $(\Delta T_{ad}{}^{ap,pk}-\Delta T_{ad}{}^{pk})/\Delta T_{ad}{}^{pk}$  surface is the same. Selecting a single magnetic field (e.g. 1 T that is in the middle of the range explored here) the error using its  $T_{ini}^{opt}$  for other magnetic fields is below 1% at the peak, which is within the error margin of the experimental measurements. Using  $T_{ini}^{opt}$  values different to  $T_{ini}^{opt}$ , even if they were closer to 0 K than  $T_{ini}^{opt}$ , larger errors can be obtained (around 8 % at the peak) and anomalous behaviors in the temperature dependencies of  $\Delta s_M$  and  $\Delta T_{ad}$  are found (e.g. at the paramagnetic range).

In our simulations, the values of  $T_{ini}^{opt}$  mainly depend on the magnetic parameters (*J* and  $T_C$ ), while the lattice and electronic parameters ( $\theta_D$  and  $\gamma$ , respectively) do not show any significant effect. It is worth noting that, fixing  $T_C$  for small values of *J* (1/2 and 1), the curve describing the differences between the approximated calculus and the complete ones does not intercept the  $\Delta_{SM}^{ap,pk}$ - $\Delta_{SM}^{pk}$ =0 axis, while for higher values of *J* it does (figure 7). However, if  $T_C$  is modified (fixing *J*>1) the values of  $T_{ini}^{opt}$  vary linearly with  $T_C$  (inset of figure 7).

## **3.2 APPLICATION TO EXPERIMENTAL DATA**

For practical purposes, the calculus of  $T_{ini}^{opt}$  from its mathematical definition in equation (13) is of little use as the complete curves should be known. Nevertheless, as:

- 1) the previous section demonstrated the existence of  $T_{ini}^{opt}$ ,
- 2) figure 5 shows that using this starting temperature the approximated curve is corrected for the temperature span starting from  $T_{ini}^{opt}$  and
- 3) both  $\Delta s_M$  and  $\Delta T_{ad}$  are zero well above the transition temperature,

we can use this property to identify the value of  $T_{ini}^{opt}$  for experimental data.

We can focus on the temperature range well above the transition temperature, for which  $\Delta s_M$  and  $\Delta T_{ad}$  must be practically zero. In this temperature range, the approximated values  $\Delta s_M{}^{ap}$  and  $\Delta T_{ad}{}^{ap}$  should be different to zero (either positive or negative) except for  $T_{ini}^{opt}$  (see figures 2 and 3). This feature can be used to identify  $T_{ini}^{opt}$  experimentally:  $T_{ini}^{opt}$  corresponds to that temperature which produces  $\Delta s_M{}^{ap}(T>>T_c)$  and  $\Delta T_{ad}{}^{ap}(T>>T_c)=0$ . The proposed procedure to correct the experimental  $\Delta s_M$  and  $\Delta T_{ad}$  curves when temperatures close to 0 K were not achievable can be summarized in two simple steps:

- 1) Calculate the evolution of  $\Delta s_M{}^{ap}$  and  $\Delta T_{ad}{}^{ap}$  curves for different initial temperatures.
- 2) Find the optimal initial temperature as the value of  $T_{ini}$  that makes  $\Delta s_M{}^{ap}=0$  and  $\Delta T_{ad}{}^{ap}=0$  well above the transition (the same optimal initial temperature for both).

The  $\Delta s_M{}^{ap}$  and  $\Delta T_{ad}{}^{ap}$  curves from this optimal initial temperature should be considered as the best approximation (in the range  $T > T_{ini}^{opt}$ ) to the complete curves.

The proposed procedure to minimize the error associated to  $\Delta s_M$  and  $\Delta T_{ad}$  has been applied to experimental heat capacity data measured for a single phase GdZn material (figure 8). The initial temperature of the measurements is limited by the stability of the grease used in the experimental setup (other greases are suitable to measure at lower temperatures but their range is not extended to room temperature, where the transition occurs). Figure 9 and 10 show the obtained experimental results for  $\Delta s_M{}^{ap}$  and  $\Delta T_{ad}{}^{ap}$ , respectively, calculated using different initial temperatures. It can be observed that ~100 K above the peak temperature (where  $\Delta s_M{}^{ap}$  curves remain almost constant), the values of  $\Delta s_M{}^{ap}$  and  $\Delta T_{ad}{}^{ap}$  reach zero only for a  $T_{ini}{}^{opt}\approx 221.5$  K (as predicted, the temperature is coincident for  $\Delta s_M$  and  $\Delta T_{ad}$  data). Moreover, the behavior of the curves is in agreement with the predictions derived from our simulations: while  $\Delta s_M$  varies due to  $T_{ini}$  as a temperature independent shift, the  $\Delta T_{ad}$  varies in a more complex form (changing with temperature).

In order to confirm the validity of the procedure proposed here, we have compared the obtained optimal  $\Delta s_M{}^{ap}$  and  $\Delta T_{ad}{}^{ap}$  curves to calculations from independent magnetization measurements (hollow symbols in figures 9 and 10) using equations (1) and (2), respectively. An excellent agreement between both procedures can be observed.

It is worth mentioning that, using the procedure proposed in this work, measurements at low temperatures are not needed and we avoid the necessity to combine two types of measurements (that requires a careful sample preparation to avoid artefacts in the different measurements and a large number of measurements as a function of H and Tfor both magnetization and heat capacity data).

## 4. CONCLUSIONS

We propose a procedure to minimize the associated error in the approximated calculus of the magnetocaloric parameters from heat capacity measurements. It is based on the existence of optimal initial temperatures that correct the effect of truncation of the temperature integration range (as temperatures close to 0 K can be beyond the experimental range). The optimal initial temperatures are found to be the same for  $\Delta s_M$ and  $\Delta T_{ad}$  data. These optimal temperatures can be found as the initial temperatures that make the calculated  $\Delta s_M$  and  $\Delta T_{ad}$  zero well above the transition. These features have been checked through numerical simulations and experimental measurements in a single phase GdZn alloys. A good agreement has been found between the results using the present procedure and those data obtained using the combination of heat capacity and magnetization measurements.

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## FIGURES



Figure 1. Simulated specific heat capacity data from 0 K for different magnetic fields. Inset: Specific total entropy obtained using simulated  $c_H$  data.



Figure 2. Approximated specific magnetic entropy change for a magnetic field change of 2 T for different initial temperatures. Inset: Differences between the peak values of  $\Delta s_M{}^{ap}$  for each  $T_{ini}$  with respect to the peak value with  $T_{ini}=0$  K.  $T_{ini}^{opt}$  values are marked with arrows.



Figure 3. Approximated adiabatic temperature change for a magnetic field change of 2 T for different initial temperatures. Inset: Differences between the peak values of  $\Delta T_{ad}^{ap}$  for each  $T_{ini}$  with respect to the peak value with  $T_{ini}=0$  K.  $T_{ini}^{opt}$  values are marked with arrows.



Figure 4. Illustration of the procedure to obtain the adiabatic temperature change from

temperature versus entropy curves for: a)  $T_{ini}=0$  K b)  $T_{ini}=T_{ini}^{opt}$  (211.5 K) and c)  $T_{ini}=141$  K.



Figure 5.  $\Delta T_{ad}^{ap}$ - $\Delta T_{ad}$  curves for different initial temperatures in all the temperature range above the corresponding  $T_{ini}$ . Dotted line represents this differences at  $T_{ini}$  in a continuous curve. Inset:  $T_{ini}^{opt}$  for different magnetic field change.



Figure 6. Field and temperature dependence of  $(\Delta s_M^{ap,pk} - \Delta s_M^{pk})/\Delta s_M^{pk}$ . The red line corresponds to the  $T_{ini}^{opt}$  values as a function of the magnetic field.



Figure 7. Differences between the peak value of  $\Delta s_M{}^{ap}$  at a  $T_{ini}$  with respect to the peak value from  $T_{ini}=0$  K for different J values ( $T_C=293$  K). Inset:  $T_{ini}^{opt}$  as a function of  $T_C$  for J=3.5.



Figure 8. Experimental specific heat capacity data for a GdZn alloy for different magnetic fields.



Figure 9. Calculated  $\Delta s_M{}^{ap}$  values from experimental heat capacity data for a GdZn alloy using different initial temperatures at  $\mu_0 \Delta H=2$  T. Circles represents the experimental values derived from magnetization measurements and obtained using equation (3). Inset: Evolution of  $\Delta s_M{}^{ap}$  well above  $T_C$  for different  $T_{ini}$ . The intercept of this curve with zero is used to find  $T_{ini}^{opt}$  (marked with an arrow).



Figure 10. Calculated  $\Delta T_{ad}^{ap}$  values from experimental heat capacity data for a GdZn alloy for different initial temperatures at  $\mu_0 \Delta H=2$  T. Circles represents the experimental values from combining magnetization and calorimetric data and obtained using equation (5). Inset: Evolution of  $\Delta T_{ad}^{ap}$  well above  $T_C$  for different  $T_{ini}$ . The intercept of this curve with zero is used to find  $T_{ini}^{opt}$  (marked with an arrow).

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