

Modelling the kinetic reactive transport of pollutants at the sediment-water interface. Applications with atmospheric fallout radionuclides

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ABSTRACT

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Eddy diffusivity

Understanding the behaviour of particulate matter and chemicals at the sediment-water interface (SWI) is of interest in environmental studies and risk assessments. These processes are still poorly understood, and this work aims to gain relevant insights by using a kinetic reactive transport model. It merges early diagenetic processes and box models for the uptake kinetics. Numerical solutions have been found for synthetic scenarios and for studying real cases from the literature (²¹⁰Pb and Chernobyl fallout radionuclides in Lake Sniardwy, Poland, and ⁷Be in sediments from Tema Harbour, Ghana). The study identifies a series of factors that dynamically interact to govern the final fate of tracers in the SWI region, leading to a wide diversity of behaviours. When a term of eddy diffusivity is included in the upper regions of the pore fluid, which seems feasible for some energetic scenarios, it is possible to explain the observed large penetration depths for Cs and Be, while high particle-reactive elements are retained in thinner sediment layers. Desorption from the sediment occurs through the pore fluid as diffusive fluxes. Transient depth profiles of tracer concentrations can last from months up to a year, and they can show subsurface maxima at positions unrelated with the accretion rate. In the application cases, the model explained a wide set of observational data that was beyond the capabilities of other approaches involving physical mixing of solids and equilibrium k_d . This modelling study could provide useful guidance for future research works.

1. Introduction

Anthropogenic activities are increasingly altering the landscape and affecting the fluxes of pollutants and sediments that, in turn, result in the degradation of aquatic environments. At the sediment-water interface (SWI) meet the fluxes of matter, pollutants, and trace elements from diverse provenances, including atmospheric deposition. Understanding the behaviour of particulate matter and chemicals in the sediment region below the SWI is of great scientific interest. Among other topics, it is essential for assessing the fate of pollutants, including their potential remobilization and bioavailability, and for providing suitable boundary conditions for radiometric dating models for recent sediments (Mabit et al., 2014). These latter can then support a large variety of interdisciplinary studies. Examples include, among others, decoding past anthropogenic impacts and pollution history (Kennish, 2001; Bellucci et al., 2007; Cundy and Croudace, 2017), quantifying the carbon sequestration capacity of vegetated coastal sediments (Marchand, 2017), or assessing sea level changes at centennial scale (Cundy and

Croudace, 1996; Barnett et al., 2017).

Particulate matter in natural aqueous suspensions and surficial sediments show in their surfaces uncompensated electrical charges (mostly negative) so they can uptake ions of opposite charge from the dissolved phase (Eisma, 1993). Along with electrostatic adsorption, other physicochemical processes contribute to further fixation of trace elements at different time scales (Duursma and Carroll, 1996). As a result, for some trace elements the distribution or partition coefficient, k_d (defined as the dimensionless ratio at equilibrium between the mass concentrations in solids and in solution), is of the order of 10^3 to 10^7 (IAEA, 2004). Consequently, although sediments are saturated porous media, for most trace elements, almost 100% of them are expected to be bound to the solid phase. This justifies the common approach of considering the sediment as a continuous medium, allowing for the following continuity equation (Abril, 2003):

$$\frac{\partial(\rho A)}{\partial t} = \frac{\partial}{\partial z} \left(D \rho \frac{\partial A}{\partial z} \right) - \frac{\partial}{\partial z} (wA) \quad (1)$$

Abbreviations: SWI, sediment-water interface; NID, non-ideal deposition.

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In Eq. (1) A is the mass concentration of the studied element (with physical dimensions of MM^{-3}), ρ is the bulk density [ML^{-3}], w [$\text{ML}^{-2}\text{T}^{-1}$] is the advective mass flow due to sediment accretion (see more details below), D [L^2T^{-1}] is a diffusion coefficient, z [L] is the depth coordinate, measured positive downwards the SWI, and t [T] is time. In the case of unsupported radionuclides, A is the activity concentration (in units of Bq/kg or similar), and the term $-\lambda\rho A$ must be added to the right side of Eq. (1), where λ [T^{-1}] is the radioactive decay constant. Solving Eq. (1) requires providing initial and boundary conditions. At the SWI ($z = 0$) the continuity of fluxes is commonly imposed:

$$F(t) = -D\rho \left. \frac{\partial A}{\partial z} \right|_{z=0} + wA(0, t) \quad (2)$$

where $F(t)$ [$\text{ML}^{-2}\text{T}^{-1}$] is the flux of the studied element at the SWI.

The continuity equation for solids is written in terms of a compaction potential ψ , which takes into account that the potential gravitational energy of the system decreases when the water pores are progressively replaced by the overlaying solids (Abril, 2003, 2011):

$$\frac{\partial \rho}{\partial t} = -\frac{\partial w}{\partial z}; w = \rho(v + q); \rho q = -K(z) \frac{\partial \psi}{\partial z} \quad (3)$$

In Eq. (3) v is the velocity at which the SWI displaces up due to sediment accretion, and q is the mean velocity of the solids due to early compaction. ψ [L] has units of energy per unit weight, and $K(z)$ [$\text{ML}^{-2}\text{T}^{-1}$] can be interpreted as a *conductivity* function. The natural boundary condition for Eq. (3) in the SWI is the continuity of the mass flow, w_0 . The fundamental differences of this formulation with respect to the classical diagenetic equations of Berner (1980) are discussed in Abril (2003).

Equation (1) is often simplified by assuming steady state bulk density ($\frac{\partial \rho}{\partial t} = 0$; and thus, $w(z) = w_0$), which allows rewriting it in terms of a mass depth scale (Abril, 2003). All the radiometric dating models for recent sediments are particular solutions of this simplified Eq. (1), with the consistently simplified boundary condition of Eq. (2). The most widely used ^{210}Pb -based models assume $D = 0$ (see an updated summary of these models in Lurian et al., 2021).

The above approach has been applied in a huge number of scientific studies to date. However, concerns about the potential mobilization of pollutants through the pore water in marine and lacustrine sediments also have a long track. Scholkovitz and Mann (1984) first reported empirical studies on the pore water chemistry of $^{239,240}\text{Pu}$ and ^{137}Cs in marine sediments. Comans et al. (1989) reported *in situ* k_d values (the ratio of tracer concentrations in solids and pore water) for ^{137}Cs in lacustrine sediments affected by the Chernobyl accident, providing convincing evidence for post-depositional mobilization of particle-bound ^{137}Cs . Benoit and Hemond (1991) carried out similar studies reporting evidence for diffusive redistribution of ^{210}Pb in lacustrine sediments.

Although being elegant and convenient from a mathematical viewpoint, in some cases Eq. (2) may not be a reliable description of the microcosms in the SWI region. Thus, in some lacustrine and marine sediment cores sampled shortly after the Chernobyl accident in areas affected by its radioactive fallout, it was observed that ^{134}Cs had penetrated into the sediment up to 10–20 cm depth (e.g., Petersen et al., 1990; Kramer et al., 1991; Robbins and Jasinski, 1995; Holby and Evans, 1996). Similar observations have been documented in some sedimentary systems affected by the Fukushima accident (e.g., Yoshimura et al., 2014; Otsuka et al., 2020). Diffusion models provided apparently satisfactory descriptions of the data, but in some cases, the required diffusion coefficients had unreliable values (Holby and Evans, 1996). Furthermore, when applying these diffusion models to a sequence of cores taken on different dates, it was necessary to use values for the mixing coefficient that decreased with time (Robbins and Jasinski, 1995).

Abril and Gharbi (2012) noticed that these observations represented

a failure of the boundary condition of Eq. (2). Reasons argued were a fast initial redistribution in depth of the radioactive fluxes when an important fraction of them was associated to the dissolved phase, which was referred to as non-ideal deposition (NID). They used a simple numerical model for the uptake kinetics in the porous media for concept demonstration. They then suggested a consistent adaptation of Eqs. (1) and (2) by introducing a depth-distributed source term and a practical formulae for its parameterization. This allowed a successful description of some empirical profiles of ^{137}Cs and unsupported ^{210}Pb . Although being a step in the right direction, a series of concerns remain regarding the conditions for its applicability to a wide variety of tracers and sedimentary conditions, and on the involved time scales and depth-distribution patterns.

Laboratory experiments studying the uptake of radiotracers by sediments from overlying water columns have shown quite limited penetration depths after several months of incubation (e.g., ~ 4 cm after 1 year of incubation for ^{134}Cs with lacustrine sediments, after Smith et al., 2000; and ~ 2 cm after 221 days for ^{133}Ba in experiments with estuarine sediments, after Barros et al., 2003, 2004). These results have been explained in terms of molecular diffusion through interstitial water and fast equilibrium in the partitioning, although inconsistencies due to the required time-dependent k_d have been highlighted, as in the cited references. Furthermore, these penetration depths are far from the 10–20 cm range above commented.

A good number of open questions remain unsolved, particularly identifying those factors linked to both the sedimentary system and the studied tracer elements that govern NID. How do different tracers behave under the same sediment environment? Can the behaviour of a given tracer change with depth or with time? What is the effect of varying porosity? How do percolation flows enhance the penetration depth of the tracers? What is the role of eddy diffusion? What is the effect of dynamic changes in tracer concentration in overlaying waters? How are the transient distributions and the involved time scales? When can be expected to occur pollutant desorption through the pore water? How generalized can NID be to represent a serious correction to existing radiometric dating models?

The above questions can be faced by using reactive transport models, which have been a fruitful research approach for the Earth sciences during the last four decades. They combine the transport equations for one or multiple chemical species moving through a geophysical fluid with the physico-chemical reactions that they undergo; these last have been described with equilibrium and kinetics approaches (Steeffel et al., 2005; Berkowitz et al., 2016). Examples of applications are, among others, studies on radioactive waste disposal (e.g., Glassley et al., 2003), reactive transport in fractured rocks (e.g., MacQuarrie and Mayer, 2005), dispersion of reactive pollutants in the marine environment (e.g., Perianez, 2005), and geochemical reactions in petroleum subsurface reservoirs (e.g., Abd and Abushaikh, 2021).

This paper aims to obtain relevant insights into the processes that governs the dynamic of pollutants at the sediment-water interface by using a simple kinetic reactive transport model specifically adapted to this environment.

2. Methods

This section comprises a physical description of the SWI region, the mathematical approach used for the uptake kinetics, and the governing equations for the kinetic reactive transport in the porous media, along with the implementation of suitable boundary conditions for the mathematical problem.

2.1. The physical environment at the SWI region

Fig. 1 shows a sketch to support discussion. Stacked solids conform the structure of the porous medium, with the pore spaces occupied by water. The porosity, ϕ (the fraction of the bulk volume occupied by

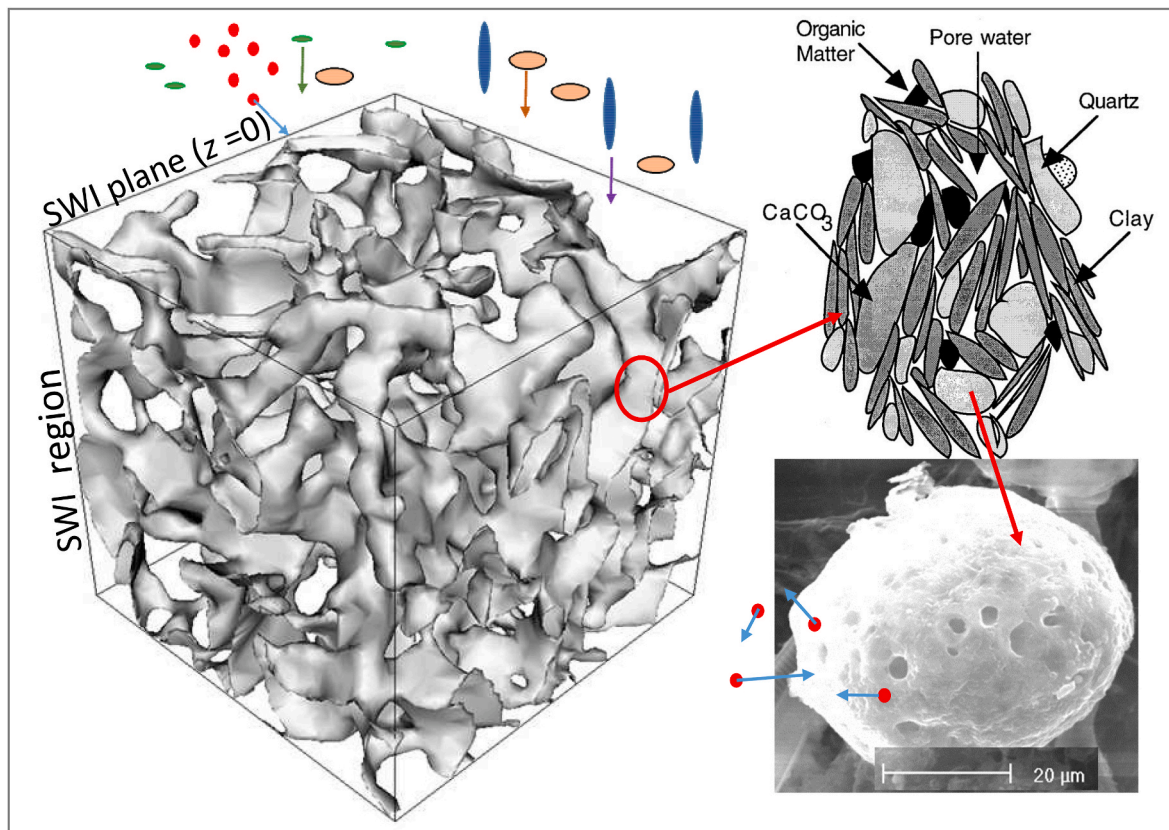


Fig. 1. Sketch illustrating the physical environment of the SWI region and the composite nature of the mass flows of solids and trace elements (see text). Dots represent ions, in a dynamical exchange among dissolved and solid-bound phases, and different geometric figures entering the SWI represent different carriers conforming the composite flux of the tracer. The artwork uses a template from the Pore Network Comparison Forum (ANU) – the structure of the porous media (left), and the subfigure of the granular medium (Boudreau, 2000) –(right up).

pores), can be higher than 90% in some cases. Solids are of varying composition, shapes and sizes, and organic matter may be present (Boudreau, 2000). The bulk density relates with porosity, so that $\rho = \rho_s(1 - \varphi)$, where ρ_s is the density of solids.

Because of the stacking, a fraction of the free surface of solids remains inaccessible to pore water. Solid particles have rugose and porous surfaces where uncompensated electric charges and more specific reaction sites are distributed (Eisma, 1993). The uptake of trace elements from the dissolved phase is a kinetic process that can be described by a set of parallel and consecutive reversible reactions, along with some irreversible components (Barros and Abril, 2008).

The SWI is not a mathematical planar surface, but an irregular, rugose, and porous interface. The trace elements reaching the SWI can be associated with a large diversity of carriers. A fraction of them can be free ions in solution, while other fractions can be bound to solid particles of different compositions and sizes. Tracers in solids may have reversible and irreversible bound components. Due to the previous history, these composite fluxes are tracer-specific and may show short- and long-term temporal variability (Abril and Brunskill, 2014).

The sediment structure is dynamically rearranged in a gravity field, with solids replacing underlying water pores. This process is known as early compaction and makes porosity asymptotically decrease over a certain depth interval in the sediment to reach a virtually uniform value (Abril, 2003). Early compaction is driven by overbounding pressure and mechanical perturbations such as pressure waves, micro-earthquakes, etc. It can progress as a uniform decrease in porosity without perturbing the isochronous horizons or with a differential translocation of particles of different sizes.

In dynamical sedimentary scenarios the friction stress of water currents at the SWI can lead to sediment resuspension, with episodic or

periodic (e.g. in tidal systems) destruction and re-composition of the upper SWI region. The threshold friction stress for resuspension is a function of particle size and the roughness length. Typical values of 0.06 Pa are required for the clay fraction, which roughly corresponds to depth-averaged water currents of 5 cm s^{-1} (Eisma, 1993). Higher values are required for larger particle sizes.

The diffusion term in Eq. (1) accounts for sub-grid scale advection. This is, displacements of solids up and down a horizontal planar surface, in such a way that there is no net mass transport, but the concentration of the tracer changes when there are spatial gradients. These null net mass flows do not affect the bulk density, so diffusion is absent in Eq. (3). The physical reworking of solids against the gravity field requires a forcing agent, such as bioturbation. Differential translocation of solids by early compaction can represent a tiny contribution (of the order of $10^{-9} \text{ cm}^2 \text{ h}^{-1}$ after a Fermi estimate, based upon a Reynolds approach). The resuspension and deposition cycles could support in some cases a mathematical description as equivalent diffusion. All the above processes are clearly depth dependent.

The chemical environment progressively changes with depth towards anoxic conditions and with varying concentrations of competing ions, such as NH_4^+ (Comans et al., 1989).

2.2. Uptake kinetics in a porous media

The scientific literature reports numerous results from experimental and modelling studies on the uptake of radionuclides and other trace elements by natural aqueous suspensions. Some examples are shown in Fig. 2, and they are briefly explained in the figure caption. The time series of tracer concentrations in the dissolved phase can be mathematically fitted to an analytical function involving a set of exponentials

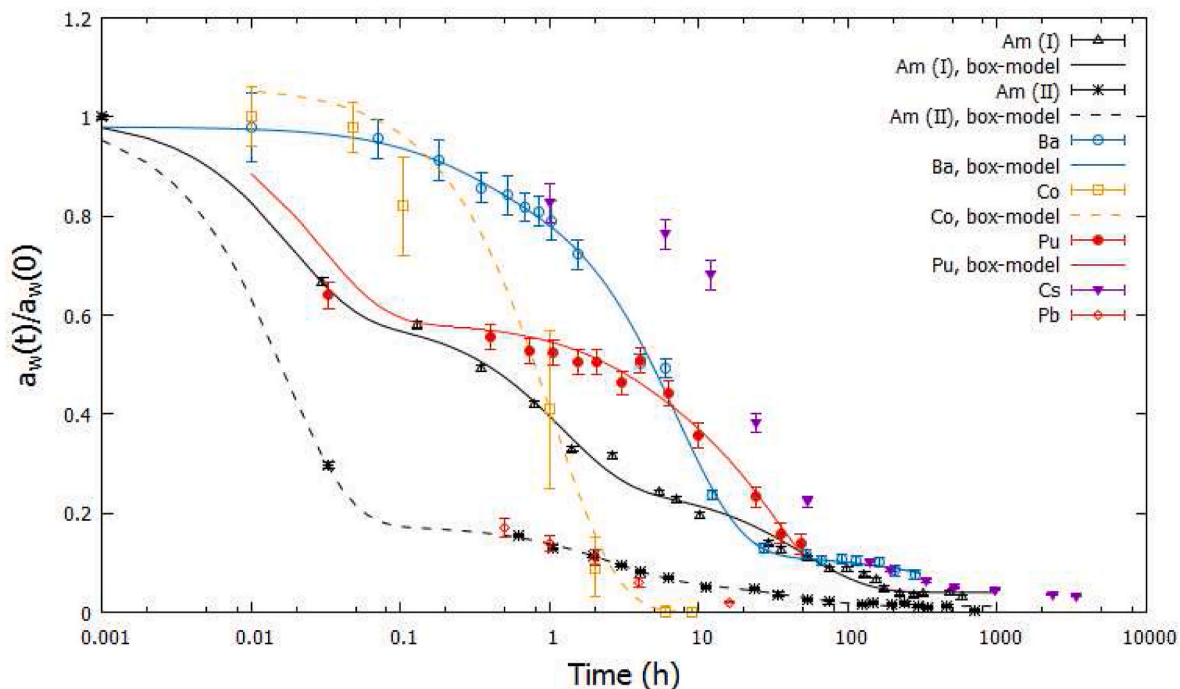


Fig. 2. Experimental data and fitted curves with box models (see Fig. S1, in ESM) for a set of adsorption experiments taken from the scientific literature. The tracer is added to the solution and the remaining fraction in this phase is plotted versus the contact time. Am (I) and Am (II) correspond to the uptake of ^{241}Am by aqueous suspensions from the Guadalquivir River (SW Spain) of 43 and 172 ppm with external SSA of $1.33 \text{ m}^2 \text{ g}^{-1}$ (experimental data from El-Mrabet et al., 2004, and box models from Barros and Abril, 2005). Ba corresponds to the uptake of ^{133}Ba by suspended estuarine sediments of 20 g l^{-1} with an external SSA of $0.010 \text{ m}^2 \text{ g}^{-1}$ (experimental data from Barros and Abril, 2004). Co corresponds to the uptake of ^{60}Co by marine sediments (2 g underlying 20 mL of seawater) with a SSA by the BET method of $13 \text{ m}^2 \text{ g}^{-1}$ (experimental data from Børretzen and Salbu, 2000, and box model from Barros and Abril, 2008). Pu corresponds to the uptake of ^{239}Pu by natural aqueous suspension from the Guadalquivir River of 12.6 ppm with external SSA of $1.63 \text{ m}^2 \text{ g}^{-1}$ (experimental data and box model from El-Mrabet et al., 2001). Cs corresponds to the uptake of ^{134}Cs by marine sediments (2 g underlying 20 mL of seawater) with a SSA by the BET method of $13 \text{ m}^2 \text{ g}^{-1}$ (experimental data from Børretzen and Salbu, 2002). Pb corresponds to the uptake of ^{210}Pb by suspended marine sediments of 52.6 ppm and size $<63 \mu\text{m}$ (experimental data from Wang et al., 2019).

that are associated with different characteristic times in the uptake, ranging from minutes up to weeks (Barros and Abril, 2005). This function arises as the mathematical solution of box models involving the dissolved phase and up to three different reaction sites within the particle. They are connected by parallel or consecutive reversible reactions, or by a mixture of them, which are described by constant kinetic coefficients. Some examples of box models are shown in Fig. S1, in the electronic supplementary material (ESM). In some cases, models include some irreversible reactions and saturation terms (e.g., El-Mrabet et al., 2001).

It has been shown that the above empirical data do not allow unambiguously identifying the involved processes in terms of parallel or consecutive reactions, since it is always possible to find the same analytical solution using any possible variation of the reactions schemes (Barros and Abril, 2004, 2005).

The factors affecting the kinetic coefficients and the partitioning at equilibrium have been profusely studied from both experimental and theoretical approaches. Abril (1998a; 1998b) presented a basic microscopic theory for the uptake kinetics of trace elements by suspended particulate matter. The direct transfer coefficient is proportional to the free surface of solids per unit volume of solution and to a geometric probability of reaction. Thus, its value depends on the experimental setup (e.g., on the volumetric concentration and the granulometric and mineralogical characteristics of suspended solids). The more physically significant proportionality factor could be isolated, but there is no unified approach to estimate the specific surface area (SSA) of solids. Some works use the so-called external SSA, estimated from the size spectrum and the assumption of spherical shapes. Other works report SSA measured by gas adsorption using the BET isotherm, which accounts for non-spherical shapes, and the rugose and porous surfaces, leading to

much larger values than the above method (see examples in the references cited in the caption of Fig. 2). The geometric probability of reaction depends on the surficial concentration of reaction sites but also on the concentration of competing ions into solution, which explains the dependence of k_d with pH, salinity, and NH_4^+ (Abril and Fraga, 1996; Comans et al., 1997). The coefficients for reverse reactions are related to the probability of rupture of the unions, which can be mediated by the composition of the aqueous solution and the temperature, but they do not depend on SSA. As the uptake is a genuine surface phenomenon, the inner portion of the solids are prevented for any sorption or desorption, which leads to the well-known particle size effects in k_d (Abril and Fraga, 1996).

Because of the mathematical equivalence of models, in this work we have adopted for simplicity a scheme of consecutive reactions (case A in Fig. S1, in ESM) that for two components in the solids can be written as follows:

$$\begin{aligned}
 \frac{da_w}{dt} &= -k_{11}a_w + k_{21}a_{s,1} \\
 \frac{da_{s,1}}{dt} &= k_{11}a_w - (k_{21} + k_{12})a_{s,1} + k_{22}a_{s,2} \\
 \frac{da_{s,2}}{dt} &= k_{12}a_{s,1} - k_{22}a_{s,2}
 \end{aligned} \tag{4}$$

In Eq. (4), a_w is the volumetric concentration of the tracer in dissolved phase, while $a_{s,1}$ and $a_{s,2}$ are their volumetric concentrations in reaction sites 1 and 2 in the solids; k_{1i} and k_{2i} ($i = 1, 2$) are the kinetic coefficients for direct and reverse reactions, with units of inverse time. It is worth noting that the radioactive decay constant for radionuclides does not need to be explicitly included in Eq. (4) when half-lives are much longer than the duration of the experiment. More complex

reaction schemes are possible, but Eq. (4) accounts for the major features of the uptake kinetics and is versatile enough for the present goals. For the simplest case of constant coefficients, the partition coefficient at equilibrium (the time derivatives in Eq. (4) become null) is:

$$k_d = \frac{k_{11}(k_{22} + k_{12})}{k_{21}k_{22}m_s} \quad (5)$$

where m_s is the concentration of suspended solids (kg/L) and the density of the water (1.0 kg/l) is implicitly included, without corrections in volume because m_s , which are assumed to be small.

Equation (4) can be locally adapted to the porous sediment medium, assuming homogeneity of concentrations in a region characterized by a porosity φ , a mean density of solids, ρ_s , and in absence of advective-diffusive transport. The volumetric concentrations in Eq. (4) can be expressed in terms of their corresponding mass concentrations (denoted with upper $\hat{\cdot}$): $a_w = \rho_w \varphi \hat{a}_w$; $a_{s,i} = \rho_s(1-\varphi)\hat{a}_{s,i}$ (ρ_w is the density of the pore fluid). Solving for k_d :

$$k_d = \frac{k_{11}(k_{22} + k_{12})}{k_{21}k_{22}} \frac{\rho_w \varphi}{\rho_s(1-\varphi)} \quad (6)$$

From the above discussion, the state-of-the-art does not allow a priori reliable estimates of the kinetic coefficients for the trace elements of interest. They will take site-specific values that capture the physico-chemical properties of the solid and aqueous phases, and they will vary with space and time as such properties do. Therefore, transient stages are expected to be ubiquitous.

The previous presentation focused on sorption experiments. There is wide experimental evidence that after long contact times, an important fraction of the tracer becomes irreversibly bound to the solids. As an example of these studies, [Børretzen and Salbu \(2000\)](#) conducted desorption experiments with Cd and Co in marine sediments. They used a sequence of reagents having increasing displacement and dissolution power. Seawater only could desorb about 10% of Cd and a negligible amount of Co.

The selected approach for this study uses a set of synthetic kinetic coefficients that define several classes of trace elements with increasing affinity for solids ([Table 1](#)). These values are inspired in experimental data (e.g., classes A and B are adaptations from experiments with ^{133}Ba reported in [Fig. 2](#), while class D uses results from ^{241}Am). [Table 2](#) summarises the recommended k_d values for a set of elements in various aquatic environments. In each case of interest, the behaviour of the target element can be considered to be close to one of the classes in [Table 1](#).

Increasing k_d values are often associated with a faster uptake kinetics, as shown in [Fig. S2](#) (in ESM) and [Table 1](#). Different equilibrium times are possible for a given k_d , as illustrated in [Fig. S2](#) and [Table 1](#) with tracer A*. This last uses the set of kinetic coefficients of tracer A, but multiplying k_{22} and k_{12} by a factor ($\frac{1}{4}$), what leaves invariant the k_d (Eq. (6)). The effects of irreversibility and saturation will be incorporated some further as a modification of data in [Table 1](#).

It is worth noting that for all the tracers in [Table 1](#), after equilibrium more than 99.8% of the tracer was associated to solids. Within solids, sites 2 stored approximately 98% of tracer A and 99.99% of tracer D.

Table 1
Kinetic transfer coefficients defining various categories of trace elements used for the numerical modelling of reactive transport in the SWI region.

Class	k_{11} (h ⁻¹)	k_{21} (h ⁻¹)	k_{12} (h ⁻¹)	k_{22} (h ⁻¹)	k_d	t_{eq} (h)
A	12.5	1.0	0.25	0.005	1.0·10 ³	50.5
A*	12.5	1.0	0.0625	0.00125	1.0·10 ³	120
B	25.0	2.0	0.5	0.001	1.0·10 ⁴	31.0
C	200	6.0	1.0	0.0005	1.1·10 ⁵	15.0
D	500	10.0	1.3	0.0001	1.0·10 ⁶	11.0

k_d values estimated from Eq. (6) with $\varphi = 0.8$, $\rho_s = 2.5 \text{ g cm}^{-3}$ and $\rho_w = 1.0 \text{ g cm}^{-3}$. Equilibrium times from [Fig. S2](#) (ESM).

2.3. Constituent equations for the kinetic reactive transport of trace elements in the SWI region

The conceptual model tries to capture the essential processes described above while keeping complexity at a minimum, but with flexibility for necessary extensions.

The first point is to solve the velocity field for the physical fluid carrying the tracers studied. On the time scales of interest, both the aqueous and solid phases of the sediment can undergo transport processes. A steady state will be assumed with a mass flow w_o , and percolation velocities, $v_{p,0}$, imposed as boundary conditions at the SWI. Then, Eq. (3) allows estimating the accretion and compaction velocities from the empirical bulk density profile.

The reactive transport model will be formulated for a single component that is presented in dissolved form and in two reaction sites in solids, connected by consecutive reversible reactions. Some flexibility will be necessary to include irreversibility in the uptake.

The transport equations for the tracer use the velocity field of the physical medium and incorporate a diffusion term in the fluid phase, along with the terms describing the kinetics of the uptake. The kinetic coefficients in [Table 1](#) are assumed to account for the effective surface area of solids accessible to the dissolved phase.

A first goal is studying the conditions that can lead to a rapid initial redistribution over large depths of trace elements that reach the SWI into the dissolved phase. When the involved time scales are of the order of few days to few weeks, sediment accretion can be neglected, and radioactive decay is negligible in most cases. The equations for the reactive transport can then be written as follows:

$$\begin{aligned} \frac{d(\rho_w \varphi \hat{a}_w)}{dt} &= -k_{11} \rho_w \varphi \hat{a}_w + k_{21} \hat{a}_{s,1} \rho_s (1-\varphi) + \frac{\partial}{\partial z} \left(D_{eff} \rho_w \varphi \frac{\partial \hat{a}_w}{\partial z} \right) - \frac{\partial}{\partial z} (v_p \rho_w \varphi \hat{a}_w) \\ \frac{d}{dt} (\hat{a}_{s,1} \rho_s (1-\varphi)) &= k_{11} \rho_w \varphi \hat{a}_w - [(k_{21} + k_{12}) \hat{a}_{s,1} + k_{22} \hat{a}_{s,2}] \rho_s (1-\varphi) \\ \frac{d}{dt} (\hat{a}_{s,2} \rho_s (1-\varphi)) &= [k_{12} \hat{a}_{s,1} - k_{22} \hat{a}_{s,2}] \rho_s (1-\varphi) \end{aligned} \quad (7)$$

In Eq. (7), v_p is the percolation velocity, and D_{eff} is an effective diffusion coefficient. This last can be written in terms of the molecular diffusion, D_m , corrected by the tortuosity of the porous media (the factor φ^n , with n in the range 1–2 is a practical empirical correction – see [Krezoski et al., 1984](#); [Barros et al., 2004](#)), and it may include a term for eddy diffusivity D_e , as discussed further below:

$$D_{eff} = D_e + \varphi^n D_m \quad (8)$$

At the SWI ($z = 0$), a flux of tracers, F_w , is entering into the dissolved phase, fulfilling the boundary condition

$$F_w(t) = -D_{eff} \rho_w \varphi \frac{\partial \hat{a}_w}{\partial z} \Big|_{z=0} + v_{p,0} \rho_w \varphi \hat{a}_w(0, t) \quad (9)$$

Any analytical function or numerical time series can be imposed as $F_w(t)$. Alternatively, it can be estimated as the advective-diffusive transport with an overlaying water column where the concentration of dissolved tracers is known as a function of time, $\hat{a}_{0,w}(t)$.

This work will show that, in some cases, transient stages persist from several months up to more than one year. Thus, sediment accretion and radioactive decay must be explicitly included in the equations. The last is a trivial task. For the former, a simplified approach will assume a constant mass sedimentation rate, w , and a steady state bulk density profile with a known early compaction limit with bulk density ρ_∞ . The SWI displaces up, due to sedimentation, with a linear velocity $v = \frac{w}{\rho_\infty}$. From a reference frame anchored to this SWI, the velocity of solids, v_s , and pore water, v_w , at depth z are, respectively ([Abril 2003, 2011](#)):

$$v_s(z) = v + q = \frac{w}{\rho(z)} \quad (10a)$$

Table 2Recommended k_d values for some trace elements in aquatic environments.

Environment	Co	Ce	Cs	Ba	Pb	U	Pu	Am
Open ocean [1]	5·10 ⁷	7·10 ⁷	2·10 ³	9·10 ³	1·10 ⁷	5·10 ²	1·10 ⁵	2·10 ⁶
Ocean margin [1]	3·10 ⁵	3·10 ⁶	4·10 ³	2·10 ³	1·10 ⁵	1·10 ³	1·10 ⁵	2·10 ⁶
Freshwater [2]	4.3·10 ⁴	2.2·10 ⁵	9.5·10 ³	2·10 ³	1.1·10 ⁵	-	7.9·10 ⁴	2.1·10 ⁵

[1] Data from IAEA (2004); [2] data from IAEA (2010) but for Pb, which is reported from Mudbidre et al. (2014).

$$v_w(z) = v_p(z) + v - q'; \quad q' = q \frac{1 - \varphi(z)}{\varphi(z)} \quad (10b)$$

In Eqs. (7) and (9) v_p must be replaced by $v_w(z)$, and an advective term must be added to Eq. (7) for $\hat{a}_{s,i}$ ($i = 1, 2$):

$$-\frac{\partial}{\partial z} [v_s \rho_s (1 - \varphi) \hat{a}_{s,i}] \quad (11)$$

At the SWI the flux of tracer associated to the reaction sites in solids must be specified:

$$F_{s,i}(t) = v_s(0) \rho_s [1 - \varphi(0)] \hat{a}_{s,i}(0, t) \quad (12)$$

The system of Eqs. (7)–(12) conforms a model being general enough as to account for composite fluxes with dissolved and particle-bound fractions. Eq. (12) allows one to impose any degree of transient partitioning among phases. The occurrence of an irreversibly bound fraction in the mass flow reaching the SWI can be included as a third reaction site in solids, $\hat{a}_{s,3}$, that only undergoes accretion (Eq. (11)) and radioactive decay. This third reaction site can be connected to sites 2 as a possible formulation to model the progression of irreversibility.

For numerical solutions, we used an upwind finite-difference scheme, corrected by numerical dispersion when relevant. The spatial discretization, Δz , and the time step, Δt , are selected to meet the criteria for numerical stability (Perianez, 2005). The lower boundary is positioned deep enough so that the used boundary conditions (continuity of gradients) have negligible effects on the solution. The quality of the solution is checked by monitoring the mass balance of the tracer over time.

Nyffeler et al. (1986) used a similar modelling approach including basic processes in the overlaying water column and a diffusion term for solids, but in most of the applications the contribution of $\hat{a}_{s,2}$ was neglected. Robbins (1986) presented a two-phase model for radionuclide transport within sediments assuming instantaneous equilibrium between the dissolved and particle bound phases. The same approach appears in the work by Smith et al. (2000). The previous work by Smith and Comans (1996) included sediment accretion and physical diffusion affecting both aqueous and solid phases, and a k_d value scaled by the depth-dependent concentration of NH_4^+ . More recently, a multi-fractional sediment transport module similar to Eq. (7) has been incorporated into a more general 3D radioactivity transport model coupled with multiscale circulation (Maderich et al., 2017).

3. Results and discussion

3.1. Contact time

The following setup has been selected for studying the effect of increasing contact times in the absence of sediment accretion: Uniform value of porosity, $\varphi = 0.8$, kinetic coefficients for classes A and C (Table 1), $v_p = 0$; $\rho_w = 1 \text{ g cm}^{-3}$; $\rho_s = 2.5 \text{ g cm}^{-3}$; molecular diffusion (Eq. (8)) with $D_m = 0.05 \text{ cm}^2 \text{ h}^{-1}$ (Smith et al., 2000) and $n = 1.75$. As the boundary condition (Eq. (9)), $F_w(t)$ was analytically formulated as a Gaussian pulse that peaks at $t = 15 \text{ h}$ and with $\sigma = 4 \text{ h}$. The total amount of tracer injected was 100, in arbitrary units (a.u.). The simulation times were set as 5 d, 10 d, and 15 d. The core length was 10 cm for tracer A and 5 cm for tracer C.

The results are shown in Fig. S3 (in ESM). The aggregated amount of

tracers per unit dry mass (a.u. g^{-1}), $A(z)$, has been selected as the meaningful magnitude, since it would correspond to the empirical value measured in a real sediment core after slicing and drying.

The kinetic reactive transport driven by molecular diffusion allows a depth distribution of the Gaussian pulse of tracers. After 5 days, the remaining amount of tracer in water is unable to promote any further redistribution for tracer C, with a higher nominal k_d value (Table 1), while some tinny evolution can be observed for tracer A (Fig. S3, ESM). The penetration depth is defined here as the depth above which 99% of the inventory is located. It is 0.18 cm for tracer C and 0.70 cm for tracer A after 10 d.

The *in situ* k_d , locally estimated from the ratio of mass concentrations of the tracer in solids and pore water, changed with depth and time (Fig. S3, ESM). Unlike in the absence of transport processes (Eq. (6)) the tracer concentration in dissolved phase changes with time because uptake by solids, diffusion, and the time-dependent fluxes at the SWI. As a result, k_d reflects transient stages. A similar decrease in *in situ* k_d with depth has been described for lacustrine sediments by Benoit and Hemond (1991).

3.2. Porosity and percolation

The numerical setup is as the one described in the previous section, but using different values for the porosity. The simulation time was set to 10 d. In all cases, the depth distribution of $A(z)$ was similar to that shown in Fig. S3 (ESM). For the sake of brevity, only the penetration depth is reported in Table 3.

Porosity, through the parameterization of tortuosity, affects the magnitude of the effective diffusion coefficient (Eq. (8)). A second effect is that higher porosities enhance the role of the dissolved phase. In the absence of percolation, increasing porosities promote slightly larger penetration depths for tracer A, but their effects become negligible for tracers with higher nominal k_d values. Even with very high porosities, the solid phase acts as an effective filter trapping the high particle-reactive tracers in a few millimetres.

Percolation velocities through sediment to the groundwater table usually take low values. In their study, Benoit and Hemond (1991) reported measured values of 0.6 mm/day. Here we explored the effect of a higher value of 3.0 mm/day, and the extreme case of 3 cm/day. The effect in the penetration depth is negligible, but for tracer A, with increments of 1.3% and 27%, respectively (Table 3). This happens again because the solids act as an efficient filter, retaining the particle-reactive tracers. The performance of the numerical scheme has been tested for a

Table 3

Penetration depth (given in cm) of different tracers for varying uniform porosities and percolation velocities (v_p , in mm/day). Results from numerical simulations with the model setup of section 3.1

Tracer	$v_p = 0$			$\varphi = 0.90$	
	$\varphi = 0.65$	$\varphi = 0.80$	$\varphi = 0.90$	$v_p = 3$	$v_p = 30$
A	0.59	0.70	0.78	0.79	0.99
B	–	0.43	0.47	0.48	–
C	–	0.18	0.19	0.19	0.20

Gaussian pulse for $F_w(t)$; $D_m = 0.05 \text{ cm}^2 \text{ h}^{-1}$ and $n = 1.75$. Simulation time 10 days.

conservative tracer (what can be achieved setting $k_{11} = 0$ in Eq. (7)). In this case, the centroid of the pulse of concentration in the pore fluid displaced down with the prescribed percolation velocity.

The tiny role of v_p when compared against molecular diffusion can be understood by handling the concepts of mixing length and mixing velocity. Thus, in the numerical scheme, with spatial discretization Δz , diffusion through a planar surface can be seen as the result of two opposite mass flows with a mixing velocity $v_D \sim \varphi^n D_m / \Delta z$ (Abril and García-Lón, 1991). For $\Delta z = 0.1$ cm, $v_D \sim 96$ mm d⁻¹, which is much higher than v_p .

It is worth noting that with this boundary condition, where $F_w(t)$ is prescribed, v_p only affects the transport of the tracer. For boundary conditions providing the tracer concentration in the overlaying water column, v_p will also affect to the flux entering through the SWI (see Eq. (9)). This second configuration is studied in Section 3.4.

3.3. Eddy diffusivity

The above results suggest that molecular diffusion cannot explain large penetration depths even when porosity and v_p take very high values (Table 3). It is worth noting that experimental studies on depth distribution of tracers in sediments use typical slicing resolutions of the order of 1 cm.

Eddy diffusivity is generally used for representing the nonlinear turbulent advection of scalar properties of the fluid. The vertical eddy diffusivity coefficient in water bodies can be estimated from time series of temperature vs depth profiles (e.g., Li, 1973; Salas de León et al., 2016). It largely depends on the depth of the water and on the season. For lacustrine environments, empirical values have been reported within the range 10^{-8} to 10^{-3} m²s⁻¹ (e.g., see Salas de León et al., 2016, and references therein). In marine environments the vertical eddy diffusivity can take larger values (of the order of 10^{-2} m²s⁻¹), which can be estimated as a function of the water current, the water depth, and the bed friction coefficient (Lane, 2005).

The vertical eddy diffusivity in the bottom boundary layer is still several orders of magnitude higher than the molecular diffusion (Wakata, 2018). Thus, assuming a sharp drop from eddy diffusivity above the SWI to only molecular diffusion just below it may not be a realistic description of the natural world. A smooth transition can be more realistic in some cases. Displacements of a large collective of molecules can occur in the pore fluid in the SWI region induced, among other factors, by bottom friction, heat transfer between solids and water, early compaction, and biological activity. The first two factors are favoured in shallow waters. Extreme cases of energy dissipation in the SWI can involve sediment resuspension. In this work, we hypothesize that the energy dissipation in the overlying water column excites the pore water below the SWI, generating an eddy diffusivity that progressively declines with depth.

For a first assessment of the effect of eddy diffusivity, the coefficient D_e in Eq. (8) has been parameterized as follows:

$$D_e = D_{e,0} e^{-\beta z} \quad (13)$$

The following simulation setup is as in Section 3.1, with $v_p = 0$, $\varphi = 0.90$, and a simulation time of 10 days. In addition to molecular diffusion, two formulations of eddy diffusivity have been studied: E1 uses $D_{e,0} = 3$ cm²h⁻¹ ($8.3 \cdot 10^{-8}$ m²s⁻¹) with $\beta = 2.0$ cm⁻¹ and E2 uses $D_{e,0} = 6$ cm²h⁻¹ with $\beta = 1.0$ cm⁻¹. The results for tracers A and C are shown in Fig. S4 (ESM). Tiny eddy diffusivity in the SWI region has a major effect on the penetration depth of particle-reactive tracers, including those with high k_d values.

3.4. Boundary conditions with a constant tracer concentration in the overlaying water column

In the numerical scheme, $F_w(t)$ in Eq. (9) is now estimated as

advective-diffusive transport with an overlaying water column where the concentration of dissolved tracers, $\hat{a}_{0,w}$, remains constant over time. The simulation setup uses $v_p = 0$, $\varphi = 0.80$, $\hat{a}_{0,w} = 100$ a.u.g⁻¹, $D_e = 0$, and varying contact times of 1, 5, 10, and 20 days. The results are summarized in Fig. S5 (ESM).

Total inventory and the penetration depth increased with time (Fig. S5, ESM). Analytical solutions assuming instantaneous partitioning can be obtained as follows: In Eq. (7), the second reaction is neglected ($\hat{a}_{s,2} = 0$, and $\hat{a}_{s,1}$ is denoted as \hat{a}_s), $v_p = 0$, porosity and D_{eff} are assumed to be constant in time and uniform with depth. Summing the two equations and using that $k_d = \frac{\hat{a}_s}{\hat{a}_w}$ lead to:

$$\frac{\partial \hat{a}_s}{\partial t} = D_a \frac{\partial^2 \hat{a}_s}{\partial z^2}; \quad D_a = \frac{D_{eff}}{1 + k_d \frac{\rho_s(1-\varphi)}{\rho_w \varphi}} \quad (14)$$

For initially clean sediments with a boundary condition at the SWI of constant $\hat{a}_{0,w}$, the analytical solution is (Krezoski et al., 1984):

$$\hat{a}_s(z, t) = \hat{a}_{0,w} k_d \operatorname{erfc}\left(\frac{z}{2\sqrt{D_a t}}\right) \quad (15)$$

In Eq. (15) *erfc* is the complementary error function. Taking into account the typical large values of k_d , $A(z) \cong \hat{a}_s(z, t)$. Fig. S5 (ESM) plots the analytical solution for tracer A at $t_s = 20$ d with a fitted value of $k_d = 750$. The agreement seems quite reasonable, but doing the same for other contact times requires different fitted values for k_d , namely 75, 300 and 500 for 1, 5 and 10 days, respectively. Similar results are found for tracer C, with fitted k_d values of 400, 1800 and 3300 for contact times of 1, 5 and 10 days, respectively. The failure of Eq. (15) because the needed time-dependent k_d has been previously reported (e.g., Barros et al., 2003). The uptake kinetics is not an instantaneous process, and sharp gradients appear in the liquid phase at the SWI because solids continuously adsorb the tracer. The *in situ* k_d estimated by the model reflects transient stages, which follow a trend of decrease with depth similar to that shown in Fig. S3 (ESM).

The calculated penetration depths for tracers A and C, at $t_s = 10$ d, were very close to the values reported in Table 3 (for $\varphi = 0.80$). A variant of this model setup is found in the laboratory experiments reported by Barros et al. (2003, 2004), where the concentration in the overlaying water column varied with time but asymptotically tended towards a constant value. With water at rest and at constant room temperature, eddy diffusivity is absent, and after several months of contact time, the penetration of tracers of type A was of a few cm, as previously commented.

The effects of percolation on inventories and penetration depths have been assessed for tracer A, as summarized in Table 4. These magnitudes are enhanced only by a $\sim 3\%$ for $v_p = 3$ mm d⁻¹, a representative value for environmental conditions.

The results shown in Fig. S5 (ESM) are in arbitrary units for the tracer concentration, but the use of constant kinetic coefficients in Eq. (7) implicitly assumes that such concentrations are far from producing any significant saturation of the reaction sites in solids. In case of planned or accidental releases resulting in high concentrations of the tracer, the saturation effect can promote larger penetration depths. A saturation of the second reaction sites can be modelled by using a concentration-dependent kinetic coefficient for the second direct reaction:

Table 4

Inventories and penetration depths computed for tracer A after $t_s = 20$ d using the model setup of Fig. S5 (ESM), but with varying percolation velocities.

	$v_p = 0$	$v_p = 3$ mm/d	$v_p = 30$ mm/d
Inventory (a.u. cm ⁻²)	6222	6456	8866
Penetration depth (cm)	0.74	0.76	0.93

$$k_{12} = k_{12}^0 \left(1 - \frac{\hat{a}_{s,2}(t)}{\hat{a}_{s,2}^S} \right) \quad (16)$$

k_{12}^0 is the initial value of the coefficient (Table 1), and $\hat{a}_{s,2}^S$ is the saturation concentration at reaction sites 2. Note that Eq. (16) has a local effect, keeping high the uptake kinetics in the front of the cloud of tracers in the dissolved phase.

The simulations of Fig. S5 (ESM) have been replicated for tracer C using Eq. (16) with $\hat{a}_{s,2}^S = 50,000$ a. u. g^{-1} (a tentative value that is $\sim 16\%$ of the maximum concentration found without saturation for $t_s = 10$ days). The following effects are observed when compared with the absence of saturation: i) The total uptake (i.e. the inventory in the sediment) is initially favoured (by a factor 1.5 in the first day), but then it is reduced by a factor 0.64 and 0.49 after 5 and 10 days, respectively. ii) The shape of $A(z)$ flattens in the upper layers and the penetration depth slightly increases. Similar results have been found for tracer A.

Saturation must be understood in the context of the coexisting major ions in solution that compete for the reaction sites in the solids. El-Mrabet et al. (2001) reported a fitted value of $6.5 \cdot 10^5$ Bq/kg for the saturation concentration of Pu in suspended sediments from a reservoir. This value corresponds to about $\sim 10^{-4}$ meq/100 g, which is six orders of magnitude lower than the typical cation exchange capacity of soils and sediments.

3.5. Uptake kinetics at the SWI region in real scenarios (I): Lake Sniardwy, Poland

The above results show how low k_d tracers can undergo ideal deposition in some sedimentary scenarios, while in others they can show large penetration depths. As an example close to the first situation, Tylmann et al. (2016) reported the ^{137}Cs profile in a varved sediment core from Lake Zabinskie, Poland, sampled at 40 m water depth. The water column is stratified during most of the year with a well-isolated and anoxic hypolimnion, allowing the formation and preservation of annually laminated sediments. Although porosity was high ($\sim 90\%$), eddy diffusivity is presumed to be absent. The ^{137}Cs profile was perfectly consistent with the history of atmospheric deposition, without signs of depth penetration, and with its first traces consistently dated by varve counting to AD 1952–1957 (Tylmann et al., 2016). More properly, below this age interval, there was a last measurement in a sediment slice of 1.8 cm thickness, yielding 6.1 ± 1.6 Bq kg^{-1} . The varve date interval was 1949–1952 AD (see their Fig. 4 and data in the supplementary material). This small penetration depth is what can be expected from molecular diffusion (Sections 3.2 and 3.4).

This section studies an example for the second situation, with the relatively well-documented case of the Chernobyl fallout radionuclides in Lake Sniardwy (Robbins and Jasinski, 1995). Within four months of the fallout, ^{134}Cs had penetrated down to about 10 cm in a sediment core. In cores collected from three sites a year later, ^{134}Cs had penetrated from 14 to 24 cm.

3.5.1. Sedimentary environment and data summary

All the information summarized below comes from the work by Robbins and Jasinski (1995). Sniardwy is a shallow lake (5.8 m and 23.1 m of mean and maximum depths, respectively), where frequent vertical mixing occurs favoured by wind-driven currents. The high concentration of suspended solids (annual mean of 230 mg l^{-1}) is maintained primarily by resuspension of sediments.

The authors reported data for a set of six cores sampled at three sites: one core at site I, three at site II, and two at site III. They were sampled at elapsed times of 0.31–2.12 years after the Chernobyl accident. Depths at the sampling sites were not reported. They measured activity concentrations versus depth profiles for the Chernobyl fallout radionuclides ^{134}Cs , ^{137}Cs and ^{144}Ce . In all cases, they could disaggregate the contribution of ^{137}Cs from atmospheric nuclear weapon tests (NWT). For the

core from site I (core I 8/87, sampled 1.34 years after the accident), they provided information on porosity and depth profiles of ^{210}Pb and ^{226}Ra . In this core, porosity was very high and fitted the analytical function

$$\varphi(z) = (\varphi_0 - \varphi_f) e^{-\beta z} + \varphi_f \quad (17)$$

with $\varphi_0 = 0.978$, $\varphi_f = 0.941$ and $\beta = 0.038$ cm^{-1} . Sediments were relatively homogeneous, with a mixture of clay-silt (70%), fine sand (15%) and coarse materials (15%). They showed a high content of organic matter (39% of dry weight in the surficial sediments and 27% at a depth of 20 cm). The last affects the mean density of solids, which has been set at 2.0 g cm^{-3} for the present work. The authors reported a total biomass at 9–10 m water depth of 3.5 g m^{-2} referring to studies carried out at the end of the 1970s.

The authors conducted laboratory experiments to study the uptake of Cs in aqueous suspensions of fresh, sieved (<125 μm), surface sediments, periodically mixed by mechanical agitation. They reported k_d values of $(4.3 \pm 0.3)10^3$ for a contact time of 130 days for conditions reproducing the surficial sediments. This can represent an over-estimation because of the sieving (which excluded larger particle sizes) and the mechanical agitation (which prevents the loss of free surface because of permanent contact among solids). With concentrations of 230 mg l^{-1} of suspended solids, the authors found that within about a week, short-term equilibration was nearly complete.

Robbins and Jasinski (1995) reported few data on ^{137}Cs concentrations in the water column at six different dates, and used a simple batch reactor model for reconstructing time series of concentrations over the entire range of interest. They neglected the anomalous extreme concentration of 3.1 kBq m^{-3} found on May 4th 1986. Here we adopted the same criteria and used a simple analytical fit to the data for defining a suitable $\hat{a}_{0,w}(t)$ function. From $t = 0$ (April 28th, 1986) until $t = 10.5$ d it fits a Gaussian function, and after that it follows an exponential decline (in units of Bq l^{-1} and with time in days):

$$a_{0,w}(t) = \frac{7}{\sqrt{2\pi} 3.3} e^{-\frac{(t-10.5)^2}{2 \cdot 3.3^2}} ; t < 10.5 \text{ d} \quad (18a)$$

$$a_{0,w}(t) = 0.763 e^{-0.071(t-10.5)} ; t \geq 10.5 \text{ d} \quad (18b)$$

The maximum concentration of 0.846 Bq l^{-1} occurs at $t = 9$ d, and is 0.044 Bq l^{-1} at $t = 50.5$ d. The simple batch reactor model and the analytical function of Eq. (18) are both oversimplifications. Abril et al. (2004) presented a numerical simulation of the kinetic reactive dispersion of Pu in a lacustrine environment, following a hypothetical atmospheric deposition event. With typical water currents of the order of cm/s and a varying bathymetry, large spatial gradients in concentrations may persist over time scales of several days up to a few weeks.

Robbins and Jasinski (1995) used a diagenetic model assuming instantaneous equilibrium between dissolved and particle-bound fractions, described by a uniform and constant k_d value. The model included sediment accretion, molecular diffusion, a depth-dependent physical mixing (affecting both solid and dissolved phases), and radioactive decay. Accretion was described in terms of the theory by Berner (1980), which was latter revisited by Abril (2003, 2011). In a simplified version of the model, they neglected accretion and molecular diffusion and assumed a uniform value for the mixing coefficient. The full model was solved for Cs using a simple Gaussian pulse to describe the Chernobyl input, and for ^{210}Pb , assuming a steady-state profile. This modelling approach could provide an apparently acceptable description for most of the data set, although it left several inconsistencies and open questions:

- i) Support for the postulated physical mixing. The occurrence of sediment resuspension in shallow areas of the lake does not prove its occurrence at the sampling sites. It has not been quantitatively shown how a sequence of resuspension and deposition events could result in an almost uniform value of the mixing coefficient over a 15 cm depth interval. Bioturbation was also argued as an

involved mechanism, although the empirical support is weak. However, it remains unexplained how physical mixing affects Cs and Pb, but not Ce, at sampling sites II and III.

- ii) ^{134}Cs profiles in the sequence of cores from site II. A model with equilibrium k_d and physical mixing could explain the shape of these profiles, but this required a value of the mixing coefficient which decreased with time. The reasons for this remained unexplained.
- iii) The treatment of ^{210}Pb data cannot be seen to be conclusive. Reasons are discrepancies at the top layers, as noticed by the authors, the large involved analytical uncertainties, and the use of Berner's equations for sediment accretion. A different treatment of the data will be shown later.
- iv) In all the cases the model failed to simultaneously explain the NWT ^{137}Cs data.

The application of the kinetic reactive transport model to this data set, although limited to a semi-quantitative analysis, will provide a quite different view of the involved processes, as shown below.

3.5.2. ^{137}Cs profile in core I 8/87

The kinetic reactive transport model has been applied for tracer A (Table 1), used as a proxy for Cs, with boundary conditions given by Eqs. (9) and (18). Porosity is described by Eq. (17), and the bulk density estimated with $\rho_s = 2.0 \text{ g cm}^{-3}$, because the high percentage of OM in these sediments. Although a varying porosity $\varphi(z)$ implies changes in the mass of solids and their exposed surfaces (likely linked to tortuosity), both affecting the kinetic coefficient k_{11} , a constant value has been adopted for simplicity. The effect of varying concentrations of competing ions has also been neglected because of lack of data. The core was sampled after an elapsed time of 1.34 years. Consequently, and accordingly with the empirical evidence (e.g. Børretzen and Salbu, 2000), the role of irreversibility in the uptake must be explicitly considered. A possibility is to include a third reaction site in solids, as previously commented. An alternative and simpler modelling approach is modifying in Eq. (7) the coefficient for the reverse second reaction:

$$k_{22} = k_{22}^0 e^{-\gamma t'} \quad (19)$$

k_{22}^0 is the initial value (Table 1) and γ is a scaling factor that reduces the desorption rate to its half after a certain elapsed time of the order of 50–100 days. Ideally, the clock for measuring t' should be activated at a given depth, z , when the concentration at sites 2 within the solids reached a certain threshold value. Here, for the sake of simplicity, the clock is simultaneously activated in the entire core taking $t' = t$.

The co-occurrence of high porosity in the sediment and the turbulent mixing by wind-driven currents in this shallow lake allows hypothesizing a certain contribution of eddy diffusivity in the interstitial water, which has been parameterized as follows:

$$D_e = \frac{D_{e,0}}{1 + e^{\alpha(z-z_a)}} \quad (20)$$

Note that this does not require any sediment resuspension. Eq. (20) has similar characteristics to the parameterization used by Robbins and Jasinski (1995): it allows for an almost constant value of eddy diffusivity in the range of depths from 0 to z_a , followed by a smooth decline to zero (scaled by the coefficient α) below z_a . For the sake of simplicity, D_e is a function only of z , but not of the time, so it is intended to represent the average sedimentary and hydrodynamic conditions.

The sediment accumulation rate estimated by the authors from excess ^{210}Pb returned a value of $0.12 \text{ g cm}^{-2}\text{y}^{-1}$ when excluding flattening in the upper layers (mainly due to early compaction). The figure is $0.17 \text{ g cm}^{-2}\text{y}^{-1}$ after a CF-CS model applied to the entire dataset using the mass depth scale (see details further below). The core length is too short to reach the early compaction limit, so only an upper limit can be estimated for the linear accretion velocity of the SWI using φ_f from Eq.

(17) (see Abril, 2003), which yields $v < 1.4 \text{ cm y}^{-1}$. Note that this value is much lower than the $>2.5 \text{ cm y}^{-1}$ estimate by the authors above from Berner's diagenetic equations. As the present interest is exploring the effects of the uptake kinetics, we used Eq. (7) without including sediment accretion. This avoids the need of additional assumptions for implementing the boundary conditions for reaction sites in solids (Eq. (12)). The percolation velocity has been set to zero. Radioactive decay was equally neglected for ^{137}Cs ($T_{1/2} = 30.17$ years).

Several numerical experiments have been conducted with different parameter values. RUN-1 uses $D_{e,0} = 5 \text{ cm}^{-2}\text{h}^{-1}$, $z_a = 4.5 \text{ cm}$, $\alpha = 0.7 \text{ cm}^{-1}$, and $\gamma = 0.01 \text{ d}^{-1}$. The model used a spatial discretization of $\Delta z = 0.25 \text{ cm}$ and a time step of 0.003 h , which met the criteria for numerical stability. The depth profiles of activity concentrations, $A(z)$, have been evaluated at different elapsed times after April 28th, 1986. The results are summarized in Figs. 3 and 4.

The temporal sequence of $A(z)$ profiles (Fig. 3) shows that total inventories (roughly proportional to the net area under the curve $A(z)$) first increased ($t_s = 10 \text{ d}$ and $t_s = 20 \text{ d}$) and then decreased over time ($t_s = 30 \text{ d}$ and further). Although the tracer concentration in the overlaying waters remained higher than that of the pore fluid at the SWI, there was a net diffusive flux entering the sediment (positive values in Fig. 4), but the flux reversed when the concentration in the overlaying waters became lower (negative values in Fig. 4).

Note that the concentrations in the overlaying water were prescribed from empirical observations. They were the likely result of a complex reactive transport of Chernobyl fallout radionuclides in the lake, including sorption and desorption from sediments. While the flux remained positive, $A(z)$ showed an exponential pattern, with penetration depths of about 8 cm. After reversal, the concentration in the pore-fluid decreased in the upper sediment, resulting in desorption from solids, while in the deeper layers the diffusive transport progressed with adsorption. As a result, $A(z)$ progressively flattened and developed a subsurface maximum. The prescribed irreversibility in the second reaction (Eq. (19)) reduced desorption and stabilized the $A(z)$ profile. Thus, after 300 days, the changes became negligible.

This numerical experiment highlights the importance of desorption through pore water. The maximum transient inventory in the sediment was 595 Bq cm^{-2} and was achieved at $t = 28.7$ days. After desorption, the inventory stabilized around 225 Bq cm^{-2} (data for $t = 400$ days).

Sensitivity tests have been conducted to assess the effect of eddy diffusivity and the scaling time in irreversibility. RUN-2 uses $D_{e,0} = 3 \text{ cm}^{-2}\text{h}^{-1}$, $z_a = 6.5 \text{ cm}$, $\alpha = 0.5 \text{ cm}^{-1}$, and $\gamma = 0.007 \text{ d}^{-1}$. RUN-3 uses $D_{e,0} = 2 \text{ cm}^{-2}\text{h}^{-1}$, $z_a = 8.0 \text{ cm}$, $\alpha = 0.5 \text{ cm}^{-1}$, and $\gamma = 0.007 \text{ d}^{-1}$. RUN-2* is as RUN-2, but using the kinetic coefficients of tracer A* (Table 1). The results are summarized in Fig. 5, where the computed $A(z)$ profiles after one year are compared against the empirical data. These last refer to the ^{137}Cs from Chernobyl. It is worth noting that increasing z_a does not have a direct effect on the depth of penetration. The magnitude of eddy diffusivity dynamically interplays with the uptake kinetics and the time scale of irreversibility.

The goal here was not determining the best set of parameter values that describe the empirical profile, but just getting insights about the relevant basic processes at the SWI region. Fig. 5 suggests that the uptake kinetics coupled to the molecular and eddy diffusivity in the pore fluid can account for the main features of the empirical profile without invoking the physical mixing of solids. Major discrepancies are the scaling factor for concentrations with tracer A and the tail beyond 12 cm depth. Such discrepancies can be at least partially explained by the series of simplifying assumptions included in the model setup. Including accretion can increase the depth of penetration by $\sim 1.5 \text{ cm}$, as commented on above. Analytical description of the tracer concentration in the water column (Eq. (18)) is a likely oversimplification. The set of kinetic coefficients for tracer A does not exactly correspond to that for Cs in this lake, which seems to be better described by tracer A*. The dependence of these coefficients with depth has not been considered. A decreasing

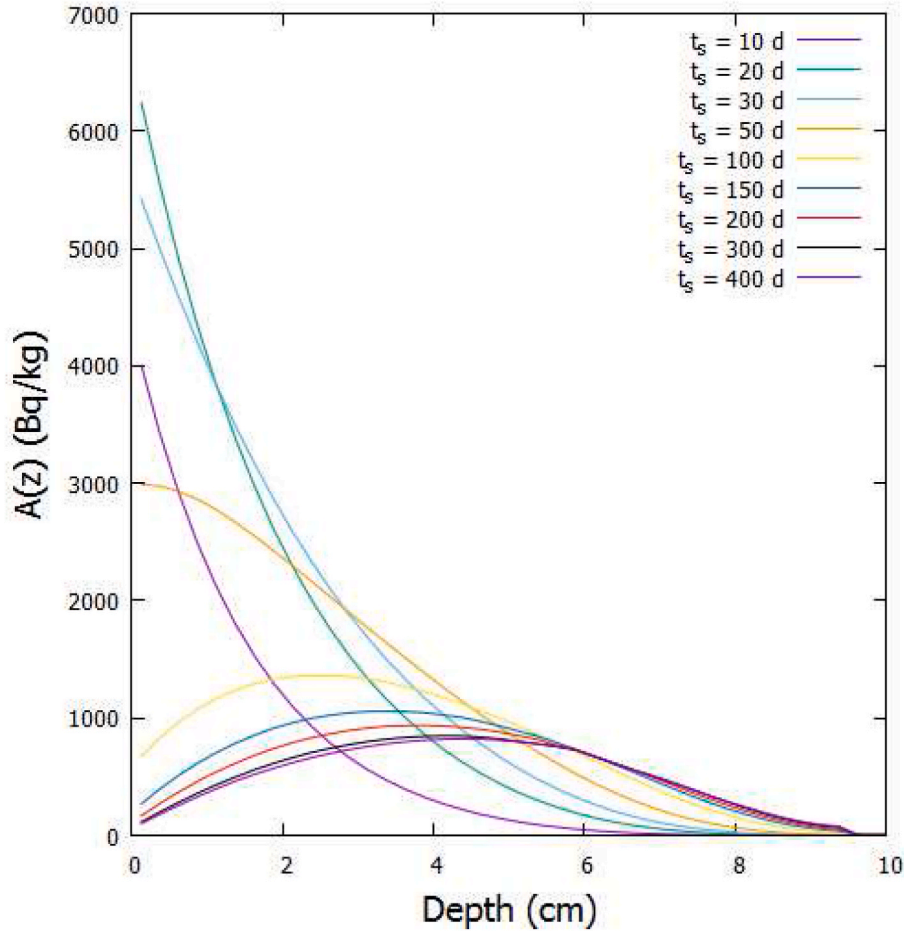


Fig. 3. Computed $A(z)$ for tracer A (Table 1), used as a proxy of ^{137}Cs from Chernobyl fallout in Lake Sniardwy, Poland. The simulation uses Eq. (7) with the particular environment described by Eqs. (17)–(20) and the parameter values of RUN-1 (Section 3.5.2). The elapsed time (t_s , in days) is measured after April 28th 1986.

value of k_{11} with depth (due to both, the hiding of particle surfaces because of aggregation and the increase concentrations of competing ions) could favour diffusive transport. The simultaneous activation of irreversibility limits the desorption from intermediate depths and, consequently, the chance for diffusive transport. Diffusive transport could also be enhanced by a time-dependent eddy diffusivity taking high values during episodic conditions of strong winds, heavy rains, etc. Slower kinetics with larger penetration depths could be also achieved by including in the model formulation a colloidal fraction, following essentially the same advective-diffusive transport as the dissolved phase, but having high tracer loads at the SWI and slow desorption kinetics. The role of colloids increasing the mobility of highly particle-reactive tracers, such as Pu, has been already reported in the scientific literature (e.g., Novikov et al., 2006). Finally, the contribution of some factors other than the kinetic reactive transport cannot be discarded. The potential contribution of bioturbation and the role of sediment accretion will be discussed in further detail below.

3.5.3. ^{134}Cs profiles in three cores sampled at site II

Further insights can be obtained by analyzing the ^{134}Cs profiles in three cores sampled at site II in Lake Sniardwy after elapsed times of 0.31, 1.34, and 2.12 years after the Chernobyl accident. They are reproduced in Fig. 6. These profiles can be explained as the transient stages of the kinetic reactive transport, as already shown in Fig. 3. Thus, Fig. 6 compares the empirical profiles against the model output for RUN-3 by using the same source term and porosity than for site I. A global scaling factor has been used to fit the numerical solution after three

months to the empirical data of the core sampled in 1986. Then this scaling factor has been corrected by radioactive decay ($T_{1/2} = 2.07$ years for ^{134}Cs) for the other cores, which are compared with the already stabilized numerical solution after one year of reactive transport (see Fig. 3 and related discussion).

It is worth noting the subsurface maximum appearing at 1.5 cm depth in both the numerical simulation and the empirical profile at the elapsed time of 0.31 y. It is clearly the effect of desorption through the pore water and not the result of sediment accretion at a rate of ~ 4.8 cm y^{-1} .

3.5.4. ^{144}Ce in cores from sites I, II and III

In freshwater sediments ^{144}Ce ($T_{1/2} = 284.9$ d) has a reference k_d value of $2.2 \cdot 10^5$ (see Table 2), so tracer C (Table 1) could be used as a proxy to model its kinetic reactive transport in the SWI region. The time series of its concentrations in the water column was not reported. Most likely, it was scavenged faster than Cs. Nevertheless, the analytical function of Eq. (18) can be used (now with arbitrary units) to assess how differently behaves ^{144}Ce because of its genuine uptake kinetics. The model setup for RUN-2 has been selected to define the eddy diffusivity and the characteristic time for irreversibility. The spatial resolution was 0.15 cm and the time step was set at 0.001 h. The computed $A(z)$ profiles after increasing the elapsed times are shown in Fig. S6 (ESM).

The depth of penetration was much shorter in this case, and the pattern remained exponential-like after 150 days. Since the partitioning among solid-bound and dissolved phases has a higher coefficient, reverse diffusive flows appeared later, when the concentration in the

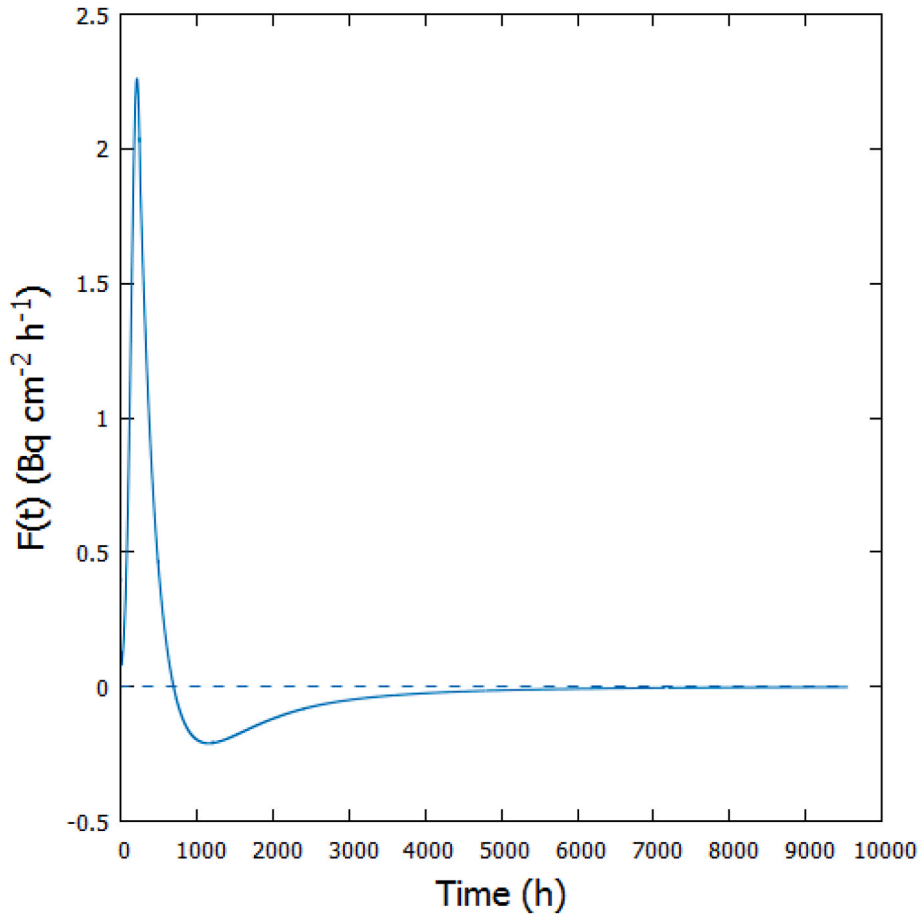


Fig. 4. Computed time series of the flux of tracer A through the SWI (Eq. (9)) with the model setup of RUN-1 (Section 3.5.2). Tracer A is used as a proxy for ^{137}Cs from Chernobyl fallout in Lake Sniardwy, Poland. Time is measured after 0:00 h on April 28th' 1986.

water column dropped below that of the pore fluid at the SWI. This happened after an elapsed time of 55 days. At this time, the transient inventory was at its maximum. After that, a tiny desorption was observed, and it reduced the inventory by 16% after 95 days.

The above approach does not consider sediment accretion, which could result in the addition of a new sediment layer of about 1.5 cm thick for core I (see estimates further below) carrying a certain concentration of scavenged ^{144}Ce . The depth of penetration estimated by the model is in reasonable agreement with the empirical observations at sites II and III in Lake Sniardwy (Robbins and Jasinski, 1995). This was not the case for site I. For this core, the authors reported an erratic profile reaching up to 10 cm depth that was not interpretable in terms of their model. They attributed this erratic behaviour to the association of this radionuclide with discrete 'hot' (nuclear fuel) particles emitted from the Chernobyl accident. Even being this the case, a physical mechanism is required to transport such particles to those depths. In this case, sampling artefacts or the role of a colloidal fraction and/or some degree of bioturbation coexisting with the kinetic reactive transport cannot be discarded (see data provided by the authors on the total biomass and the biota communities in these sediments).

3.5.5. Unsupported ^{210}Pb profile in core I 8/87

^{210}Pb is a natural occurring radionuclide ($T_{1/2} = 22.3$ years). In freshwater environments, Pb has a reference k_d value of $1.0 \cdot 10^5$ (Table 2), so tracer C (Table 1) could be used as a proxy to model the kinetic reactive transport in the SWI region of the unsupported (or excess) ^{210}Pb ($^{210}\text{Pb}_{\text{exc}}$ hereafter). This fallout radionuclide can reach the SWI in the dissolved phase and/or already attached to structural solids (see Fig. 1). Here, we are first concerned on the behaviour of the

dissolved fraction. Its concentration in the water column can vary over time as result of the varying weather conditions, but a constant value can be a reasonable approach for the present goals. We used the above settings of RUN-2 with a constant value of $\hat{a}_{0,w}(t) = 1.0$ in arbitrary units. Sediments are considered being initially free of $^{210}\text{Pb}_{\text{exc}}$.

The uptake kinetics progressed pursuing that the concentration in the interstitial water at the SWI equilibrates with that of the overlying water column. The computed $A(z)$ profiles followed a pattern similar to that of Fig. S6 (ESM). After contact times of 90 and 120 days, they fitted an exponential decline function with scaling factors of 2.66 cm^{-1} and 2.62 cm^{-1} , respectively ($R^2 = 0.9997$ in both cases). When plotted versus the mass depth scale, the exponential fit had a scaling factor of $52.0 \text{ cm}^2 \text{ g}^{-1}$ ($R^2 \approx 1.000$). This function can be used as the depth-distributed source in the model of non-ideal deposition (NID) by Abril and Gharbi (2012), allowing for its analytical solution for the steady-state profile. The results are shown in Fig. 7, where they are compared with the CF-CS model (see Abril, 2020, for an updated discussion on the fundamentals and performance of this model).

The CF-CS model assumes ideal deposition, non-postdepositional redistribution, and constant flux and sedimentation rates (SARs). It also works with varying fluxes and SARs when such variability is randomly sorted in time (Abril, 2020). This model produced a reasonable fit to the data capturing the mean values of the SAR and $^{210}\text{Pb}_{\text{exc}}$ fluxes onto the SWI of $0.17 \pm 0.02 \text{ g cm}^{-2} \text{ y}^{-1}$ and $840 \pm 100 \text{ Bq m}^{-2} \text{ y}^{-1}$, respectively ($p < 0.0001$). This estimate of the flux is much higher than the known range of atmospheric deposition ($50\text{--}200 \text{ Bq m}^{-2} \text{ y}^{-1}$, see Appleby, 1998). This suggests that an important fraction of the flux was already attached to the solids with different provenances when reaching the SWI. This seems to be a quite common case, in agreement with the

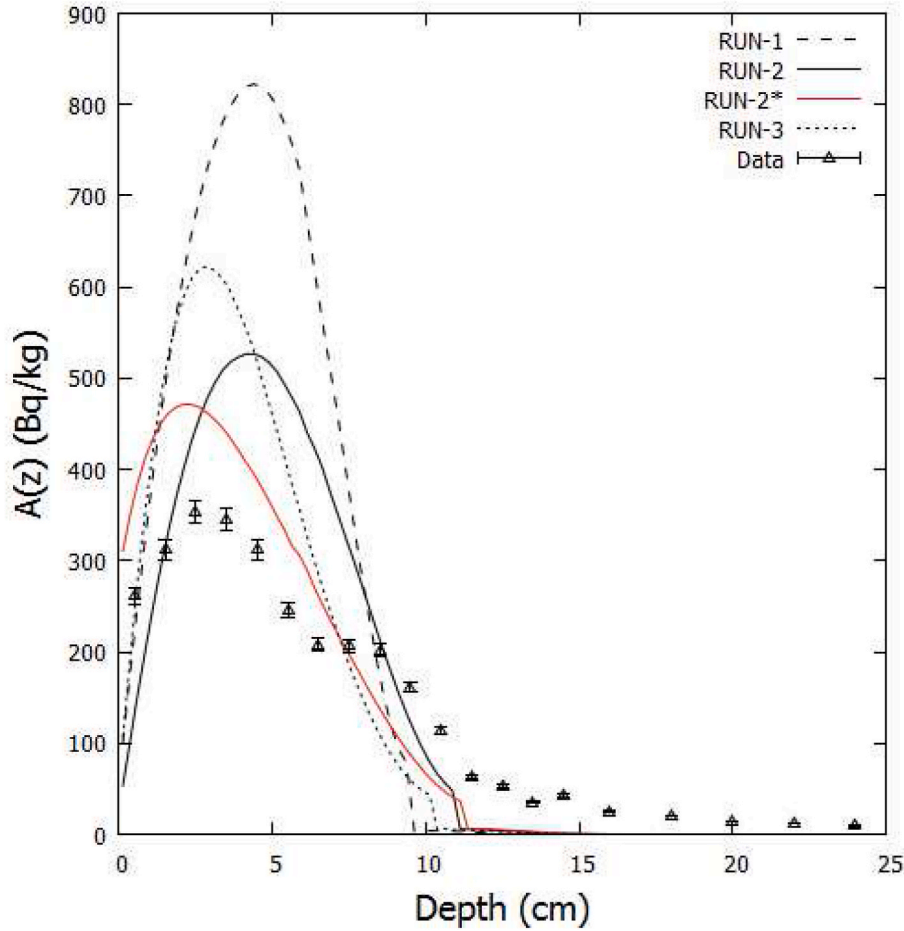


Fig. 5. Computed $A(z)$ for tracer A (Table 1), used as a proxy of ^{137}Cs from Chernobyl fallout in Lake Sniardwy, Poland. The simulation time is 400 days for RUN-1 and 360 days for RUN-2 and RUN-3 (see the text in Section 3.5.2). RUN-2* is as RUN-2 but using tracer A* (Table 1). The empirical profile shows the ^{137}Cs from Chernobyl at site I, as reported by Robbins and Jasinski (1995). The core was sampled after an elapsed time of 1.34 years.

empirical evidence reported by Abril and Brunskill (2014) in their statistical study with varved sediments.

In the NID model, the parameter g is the fraction of the $^{210}\text{Pb}_{\text{exc}}$ flux that can penetrate below the SWI (essentially the dissolved fraction), while the fraction $1-g$ is associated with structural particles that are ideally deposited at the SWI. Fig. 7 shows the analytical solutions of the NID model for $g = 0.3$ and $g = 0.5$, with the flux and SAR values inferred from the CF-CS model. The NID model improves the description of the two first centimetres of the core, being coincident with the CF-CS model in the rest. Due to the large uncertainties in the data, a more refined parameter fitting is not justified here.

3.5.6. NWT ^{137}Cs in core I 8/87

In Lake Sniardwy, eddy diffusivity in the upper regions of the sediment can explain the large penetration depths of type A tracers (with k_d values of the order of 10^3) under transient pollution events. It also explains the desorption through pore water and transient $A(z)$ profiles and inventories. Within the same physical scenario, the surficial sediments are efficient filters that retain those tracers of type C (with k_d values of the order of 10^5) in a thin surficial sediment layer. In particular, the $^{210}\text{Pb}_{\text{exc}}$ profiles can be explained without the need for physical mixing.

With the above ^{210}Pb -based SAR values, the deepest sediment slice in this core has an age of 12.0 ± 1.5 years. After the cessation of the atmospheric NWT in 1963, the ^{137}Cs reaching the SWI is expected to be mostly bound to the solids in the mass flows, and then it would have experienced ideal deposition. Therefore, the almost constant NWT ^{137}Cs profile observed in this core reflects the contribution of the irreversibly

particle-bound fraction linked to mass flows, with provenances in the catchment and in shallower transient sedimentary deposits. The 1963 peak may be far beyond the sampled depth. This view allows us to surpass the inconsistencies noticed by Robbins and Jasinski (1995) between the Chernobyl and NWT ^{137}Cs .

3.6. Uptake kinetics at the SWI region in real scenarios (II): ^7Be in sediments from the Tema harbour (Ghana)

Here we study the activity concentration vs depth profile of ^7Be (cosmogenic, $T_{1/2} = 53.3$ d) in a sediment core from Tema Harbour, Ghana. Data are from Botwe et al. (2017), their core D. The profile showed an exponential-like pattern, with ^7Be well above the detection limit at the 4–6 cm sediment slice (Fig. 8). The tides in the study area have a range of approximately 1.6 m, with tidal currents of $0.1\text{--}0.5$ m s^{-1} in the immediate coastal waters. In the harbour, the maximum cross-sectional averaged water current was about 6 cm s^{-1} at the main entrance, taking lower values within it. Therefore, sediment resuspension forced by tides can be expected only for clays and fine silts at the entrance. However, from aerial photographs, it is evident that ship traffic and particularly the manoeuvres of large cargos and drilling ships can cause remobilization of large amounts of sediments. Ship traffic usually follows well-defined tracks. Sedimentary conditions within the harbour were also impacted by dredging and the construction of new structures.

The authors discarded erosion and mixing at the core site D, among other reasons, because of the well-defined exponential profiles found for

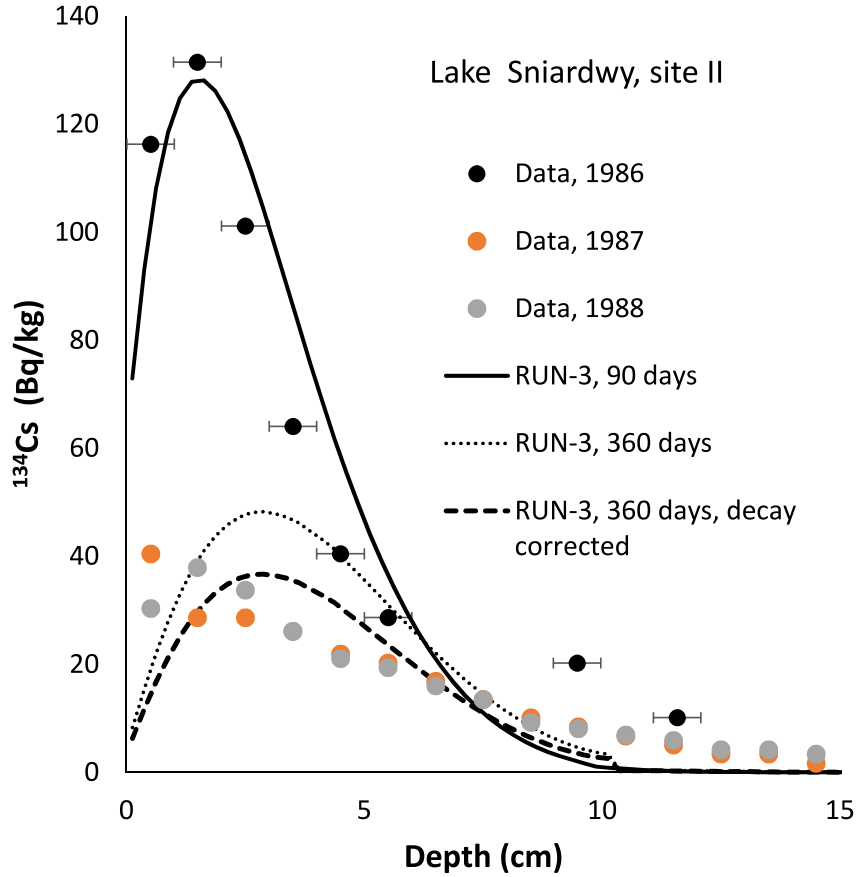


Fig. 6. Computed $A(z)$ profiles for tracer A at different times with the configuration of RUN-3 (Section 3.5.3). It is used as a proxy for ^{134}Cs from Chernobyl fallout in Lake Sniardwy, Poland. They are compared against empirical data for three cores sampled at site II at different elapsed times (data by Robbins and Jasinski, 1995; horizontal bars define the depth interval for the measured sediment slices, only depicted for the 1986 core).

^7Be and the excess ^{234}Th . This complex sedimentary scenario could be decoded by applying the ^{210}Pb -based TERESA model (Abril, 2016). For core D, the sedimentation rates showed very large temporal variations, with an arithmetic mean value (for all slices) of $4.0 \text{ g cm}^{-2} \text{ y}^{-1}$. This value was about half that of the one derived from the application of the CF-CS model to the ^7Be profile. The authors explained this apparent contradiction by arguing non-ideal deposition for ^7Be , assuming that about 50% of the ^7Be flux at the SWI underwent a fast exponential distribution in depth. This assumption is revisited here in light of the numerical simulations of the kinetic reactive transport in the SWI region.

Taylor et al. (2017) have reported results from sorption experiments with ^7Be in synthetic aqueous suspensions of selected soils. BeCl_2 salt was dissolved in ultra-pure water at a concentration of 1 mg l^{-1} . The soil:solution ratio was 1:10. They found a k_d value of $1.6 \cdot 10^3$ and a fast uptake kinetics. The k_d value is expected to be lower in marine environments because of the competing ions. From the involved theory (Abril, 1998a) we know that the kinetic coefficients for direct uptake reactions depend, among other factors, on the available free surface, the concentration of reaction sites, and the competing ions. For the present goals, tracers A and A^* (Table 1) can be used as proxies to model the behaviour of ^7Be in the studied sediment core.

The model setup used a constant concentration in the water column, $\hat{a}_{0,w} = 1.0$ in a. u., along with a global scaling factor inferred from the comparison of the model results with the empirical profile. This may be an oversimplification because of the short half-life of ^7Be , and the variability of its wet atmospheric deposition; but more sophisticated estimations are not supported by empirical data.

Preliminary runs with the simplified Eq. (7) revealed the need to include the eddy diffusivity, which seems feasible for this energetic tidal scenario. Reaching penetration depths of six cm required transient stages lasting several months, and involved a relatively slow uptake kinetics, such as of tracer A^* (Table 1). Another straightforward consequence is that radioactive decay must be explicitly included into equations, and the so high sedimentation rate must be equally considered. Thus, the full set of model equations (7)–(12) has been used here, including sediment accretion under steady state early compaction.

From data reported by Botwe et al. (2017), in the range 0–10 cm porosity in core D was reasonably described by the linear function $\varphi(z) = 0.822 - 0.018z$. For the sedimentation rate, we used the mean value derived from the TERESA model, $w = 4.0 \text{ g cm}^{-2} \text{ y}^{-1}$, with a bulk density at the early compaction limit of $\sim 1 \text{ g cm}^{-3}$ (this is a simplifying approach, since the core D showed in its intermediate portion a mixture of solids from different provenances, as discussed by Botwe et al., 2017). Percolation flows were not considered.

For the sake of brevity, only simulations with tracer A^* (Table 1) are reported here. Saturation and irreversibility have been neglected in these simulations. In the boundary conditions for the reaction sites in solids (Eq. (12)) we assumed, for simplicity, that the solids reached the SWI in dynamic equilibrium with the overlaying aqueous phase and with the relative proportion in sites 1 and 2 found in the numerical simulations shown in Fig. S2 ($f_1 = 0.02$ and $f_2 = 0.98$), so that $\hat{a}_{s,i}(0,t) = k_d \hat{a}_{w,of_i}$. Eddy diffusivity has been formulated following Eq. (20), with $D_{e,0} = 1.0 \text{ cm}^2 \text{ h}^{-1}$, $z_a = 3 \text{ cm}$ and $\alpha = 1.0 \text{ cm}^{-1}$. These values were selected as the best choice within a limited set of trials. Because of the early compaction, the advective flows had a variable velocity, but the

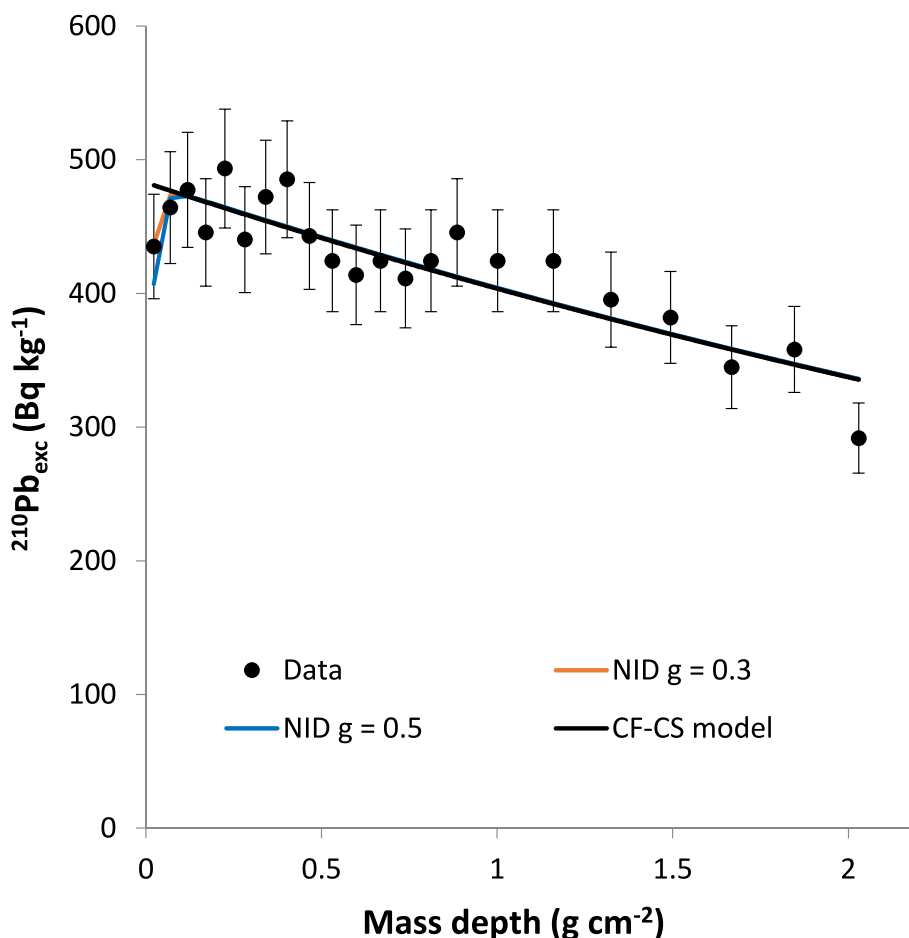


Fig. 7. $^{210}\text{Pb}_{\text{exc}}$ versus mass depth profiles for core I 8/87 in Lake Sniardwy (data from Robbins and Jasinski, 1995). Continuous lines correspond to the analytical fits provided by the CF-CS and the NID models, the latter using two values of the parameter g , giving the fraction of the $^{210}\text{Pb}_{\text{exc}}$ flux that can be distributed below the SWI.

involved numerical dispersion remained below 0.3% of the value for molecular diffusion, so no explicit corrections have been introduced in the code. The numerical scheme used $\Delta z = 0.2$ cm and $\Delta t = 0.01$ h, which met the criteria for numerical stability.

$A(z)$ profiles were generated for a sequence of contact times. They showed transient stages that progressively evolved towards a steady-state solution in which the global ^7Be flux at the SWI, forced by the spatial gradients of concentrations in the interstitial water, was compensated by radioactive decay (see Fig. 8).

Despite all the simplifications involved, Fig. 8 provides a reliable description of the empirical data. Again, the depth distribution of the tracer is not the result of physical mixing, nor of a fast sedimentation rate, but of the combined effect of accretion and the kinetic reactive transport with eddy diffusivity.

4. Conclusions

A kinetic reactive transport model for the SWI region has been developed by merging early diagenetic processes and box models for the uptake kinetics with tracer and site-specific transfer coefficients. The constituent equations have been numerically solved for a wide set of simplified scenarios and for real case studies, with a focus on the fate of fluxes at the SWI linked to the dissolved phase. Later applications included fluxes at the SWI attached to solids as exchangeable and irreversibly bound fractions. This allowed for getting some relevant conclusions:

- i) A series of factors dynamically interplay to govern the final fate of tracers in the SWI region: a) the composite nature of fluxes; b) the affinity of the tracer for occupying reaction sites in solids; c) the structure, texture and composition of sediments (described by porosity, tortuosity and bulk density, and being embedded into the locally adapted values of the kinetic transfer coefficients); c) the details on the transition from eddy diffusivity in the water column to molecular diffusion in the water pores; e) sediment accretion and early compaction. This leads to a large variability of behaviours. Thus, low k_d tracers can undergo ideal deposition in some sedimentary scenarios, while in others they can show large penetration depths.
- ii) The kinetic reactive transport resulting from molecular diffusion can explain a depth of penetration of the order of a few cm for low k_d elements, whereas for those elements with high k_d , the porous media is an efficient filter trapping the tracer in a much thinner surficial layer. Percolation of the pore fluid at typical environmental rates plays a minor role in the penetration depth of the tracers.
- iii) In situ k_d values showed transient stages, which poses under question the models using the simplifying assumption of a fast equilibrium and a constant and uniform k_d .
- iv) The large depths of penetration, of the order of or greater than 10 cm, observed in real cases, such as the Chernobyl ^{134}Cs and ^{137}Cs fallout in Lake Sniardwy, can be explained as a result of kinetic reactive transport when including a term of eddy diffusivity in the upper regions of the pore fluid. This is physically feasible in some

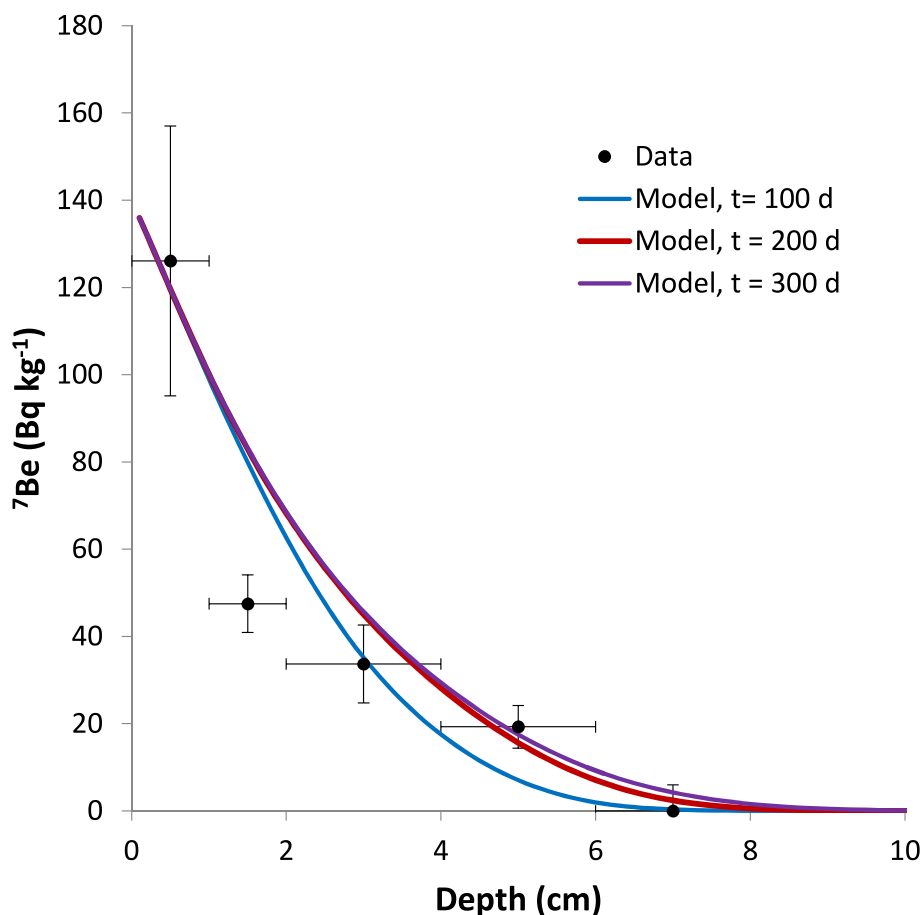


Fig. 8. ^7Be activity concentration versus depth for core D sampled in the Tema harbour, Ghana (data from Botwe et al., 2017). Horizontal bars define the slice interval, and the vertical ones are 1σ analytical uncertainties, but for the 6–8 cm slice, where the method detection limit is represented. Continuous lines are the numerical solutions from the kinetic reactive transport model at different times, and using the set of parameter values defined in Section 3.6 with a global scaling factor of $1/7$.

energetic scenarios. It can consistently explain a set of observational data that was beyond the capabilities of models involving the physical mixing of solids and equilibrium k_d .

- v) The sequence of ^{134}Cs profiles in Lake Sniardwy can be explained as transient stages involving desorption through the pore water. This surpasses the need of using mixing coefficients with values decreasing with time. Desorption from sediments occurs when the tracer concentration in the overlying water drops below that of the pore water at the SWI. This can lead to $A(z)$ profiles with subsurface maxima that are not related to sediment accretion.
- vi) Under the same physical scenario that allows large depths of penetration for low k_d tracers (e.g., ^{134}Cs , ^{137}Cs in Figs. 5 and 6), high k_d tracers can be retained in much shorter thickness, as shown for Ce and Pb in Lake Sniardwy.
- vii) Other relevant conclusions from the studied application cases are as follows:
 - a) The tiny penetration depth of $^{210}\text{Pb}_{\text{exc}}$ in these sediments, as estimated from the numerical model, can be used as a depth-distributed source to find out the analytical solution of the NID model. The $^{210}\text{Pb}_{\text{exc}}$ profile can be explained consistently without invoking the physical mixing of solids.
 - b) While fresh ^{137}Cs fallout from Chernobyl and NWT can reach the SWI mostly into the dissolved phase, after time lapses of several years, most of the ^{137}Cs fluxes still reaching the SWI are irreversibly bound to solids of different provenances, so they are not affected by the kinetic reactive transport.

c) Kinetic reactive transport with eddy diffusivity, sediment accretion under steady state compaction, and radioactive decay, can explain the exponential-like depth distribution of ^7Be observed in the coastal sediments of the Tema harbour. The use of ^7Be as a dating tool ignoring its kinetic reactive transport is discouraged.

- vii) Current knowledge does not allow considering NID as a widespread limitation in the radiometric use of ^{210}Pb and other tracers with high k_d values (e.g. $^{239,240}\text{Pu}$, ^{241}Am).

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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