

1 **Evaluating the environmental adaptability of a nearly zero energy retrofitting**
2 **strategy designed for Dutch housing stock to a Mediterranean climate.**

3
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14
15 **Abstract**

16
17 Users' behaviour and indoor climate are two leading aspects that must be taken into account if
18 we want the retrofitting of the housing stock to contribute to CO₂ reduction, comfort
19 improvement and reduction of living costs. The integrated facade module evaluated in this
20 paper, which constitutes an approach to zero energy renovation, includes a preliminary study for
21 the identification of target occupants and their characteristics and requirements that will guide
22 the design decisions. The proposed strategy primarily focuses on the case of social rental multi-
23 family housing stock in the Netherlands, but should provide insights in the application of the
24 concept in Europe. This paper presents the analysis of the adaptability of this solution to the
25 Mediterranean climate, taking into account the specific characteristics of the occupants of this
26 climatic zone.

27

28 The results showed an improved performance of building after the application of the evaluated
29 solution in southern Spain, but with lower savings on the energy demand than in the
30 Netherlands, so the economic investment should be reduced in this case. Also, the inclusion in
31 the solution of some variables, such as the forced night-time ventilation for passive cooling and
32 the insulation thickness reduction, were tested and proved to be an optimisation of its
33 performance in the Mediterranean climate. Overall, the study concluded that the proposed
34 refurbishment strategy has the potential to be implemented in different climates, particularly if
35 certain modification in the facade operation are considered.

36

37 **Keywords:** social housing stock; building retrofitting; user patterns; energy performance;
38 building simulation.

39

Nomenclature	
PPD	Predicted percentage of dissatisfied [%]
T _{co}	Optimum comfort temperature [°C]
T _{ext, ref}	Mean outdoor dry bulb temperature [°C]
ACH	Air changes per hour
PMV	Predicted mean vote

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41

42 **1. Introduction**

43

44 In recent decades, the energy efficiency of the building sector has become a common goal for
45 all European countries [1], highlighting the retrofitting of the existing residential building stock
46 in order to turn it into a ‘nearly zero energy consumption stock’. In Europe there is an important
47 amount of housing estates built during the post-war period. In the cases of the Netherlands and
48 Spain, the existing housing stock built during this period accounts for 33% [2] and 46% [3]
49 respectively of total one. In both cases, social housing represents a significant portion of the
50 residential building stock.

51

52 This part of housing stock is in need for energy retrofitting because at the time of construction
53 energy-performance related building regulations were very limited or non-existing [4-6], and
54 hence, it mostly does not have any specific thermal insulation measure in its envelope.
55 Furthermore, only 5% of the multi-family, social houses built before 1980 in southern Spain
56 have centralised heating system, and 13% have individual one [3]. This data shows that in
57 southern Spain a considerable number of dwellings does not have the proper specifications to
58 reach current standards of indoor thermal comfort conditions. This situation, in addition to the
59 low energy performance of its envelope and financial constraints of many households, increases
60 the risk of fuel poverty [7]. For this large part of the housing stock, the main aim of the
61 retrofitting should focus on the improvement of the indoor thermal comfort conditions of the
62 dwellings instead of on energy saving alone [8], without raising of the living costs.

63

64 While there are evident differences between the Dutch and southern Spanish climate, important
65 similarities between their housing stock have been found. This differences and similarities were
66 the main reason to focus this analysis on those countries. Among these similarities standouts:
67 the representativeness of the low-rise multi-family residential buildings with a linear typology
68 with two dwellings per floor and the predominance of two leaves of brick constructive system
69 [9, 10]. However, in the case of the Netherlands the percentage of glass on the facade is quite
70 higher than in southern Spain. Also some others differences were found due to the severity of
71 the Dutch climate, regarding the national regulations for the insulation exigencies and the
72 comfort ranges [11, 12].

73

74 Analysing the energy performance of building retrofitting measures has been the subject of
75 several studies in the scientific literature. Some of them evaluate the energy saving potential of
76 the existing residential stock [13-17] or develop a decision support tool able to detect the cost-
77 optimal retrofitting solution for a building category [18-20]. Also another researches are focused
78 on the evaluation, in a particular case study, of the energy performance of retrofitting measures

79 such as the envelope insulation improvement (including windows substitution) [21, 22], the
80 inclusion of heat recovery systems in mechanical ventilation [23], or a deep renovation [24].

81

82 The retrofitting solution which is evaluated in this paper (an integrated facade module) was
83 initially developed for the case of social rental multi-family housing stock in the Netherlands.

84 The following blend of characteristics make the solution stands out among others already
85 mentioned:

86 - It is a retrofitting strategy that integrates in the envelope of the building the mechanical
87 ventilation and energy generation systems.

88 - It is a retrofitting strategy that takes into account the influence of occupants' behaviour in
89 the design of the solution, to reduce the uncertainties related to energy savings and payback
90 periods [25, 26].

91 - It is a prefabricated façade module, which make it a good solution for mass implementation
92 and minimum user disturbance.

93

94 Taking as a starting point the constructive compatibility of the proposed integrated facade
95 module (due to the similarities found between the Dutch and southern Spanish housing stock),
96 the main aim of this research is to compare its performance in two different climates: Rotterdam
97 (Netherlands) and Seville (southern Spain). The main originality of this research consists on the
98 evaluation of the influence of several real user profiles on the energy performance of the
99 retrofitting solution, instead of just applicate standardised or particular profiles. The results
100 show the great influence of the users' behaviour on the energy saving potential of the proposed
101 strategy. As a second step, the optimisation of the performance of the proposed integrated
102 facade module for the warmer climate is also evaluated.

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107 **2. Methodology**

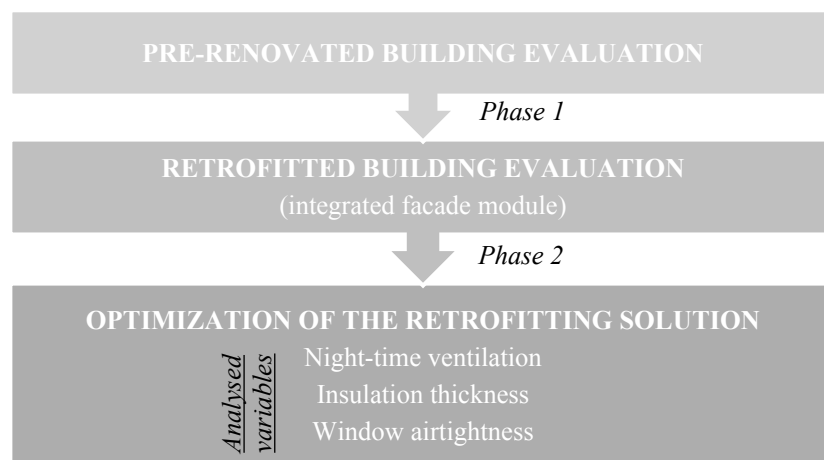
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109 In order to carry out an environmental assessment of the proposed integrated facade module,
110 energy models that incorporate that retrofitting strategy were developed and located in the
111 Netherlands and southern Spain. Also different real user profiles were applied to the models in
112 order to evaluate its influence on the energy performance of the retrofitting solution. These
113 energy models take as their starting point the energy model of an existing dwelling placed in
114 Seville in its original condition, previously described and calibrated by an annual monitoring of
115 the environmental and energetic variables [7]. The results of the energy and environmental
116 performance assessment, regarding both demand and comfort, are obtained from a comparative
117 analysis between the pre- and post-renovated models.

118

119 After analysing the results of this environmental assessment, a second phase of the study was
120 developed. It consists on the modification of different variables (such as forced night-time
121 ventilation, insulation thickness and airtightness) in the energy models, in order to evaluate its
122 effect on the energy performance of the retrofitting solution. The final aim is to find ways to
123 optimise the energy reduction and reduce the investment of the proposed integrated facade
124 module in both climates (Figure 1).

125



126

127

Figure 1. Methodology scheme.

128 The software used was Design Builder version 4.7.0.027 [27], whose Energy Plus simulation
129 engine enabled the authors to obtain precise data on annual, monthly, and hourly demands, as
130 well as indoor temperature values. The energy model recreates the whole dwelling as a single
131 thermal zone. This model also includes its boundary conditions, in terms of heat transfer and
132 shading. The climate data used for the energy simulation were taken from the EnergyPlus
133 database [28], generated by Seville and Amsterdam Schiphol (50 km from Rotterdam) weather
134 stations. The constructive definition of the envelope (Section 2.1 for the retrofitted models and
135 2.2. for the pre-renovated ones), user profiles and occupancy patterns (Section 2.3) were also
136 included in the models generation.

137

138 *2.1. The integrated facade module*

139

140 The proposed integrated facade module arises from a research project developed in the TU
141 Delft, as part of the European BTA-Flagship Program of the Climate KIC [29]. The main aims
142 of this solution are to reach zero on the meter dwellings and to limit the nuisance for the
143 occupants. The retrofitting strategy (Figure 2) consists on a pre-fabricated building envelope
144 that can be installed in a short period of time, including: insulation sandwich panels to increase
145 the thermal resistance; windows replacement; mechanical ventilation pipes integration (with a
146 heat recovery system); energy generation through PV panels installed on the roof; and also
147 heating and cooling systems depending on the situation [30].

148

149 The installation sequence of this retrofitting strategy on an existing building starts with the
150 attachment of the substructure to the existing structure (slab). The second phase is the
151 attachment of the central panel for the opaque facade and the panels including the windows to
152 the substructure. The ventilation pipes and the windows will be integrated to the panels in the
153 factory. The external cladding can or cannot be prefabricated, depending on the material choice.
154 Some finishing will probably be required on site, depending of the cladding material selection.

155 The installation of the panels can be done by two people, with the support of cranes to lift and
156 place the panels.

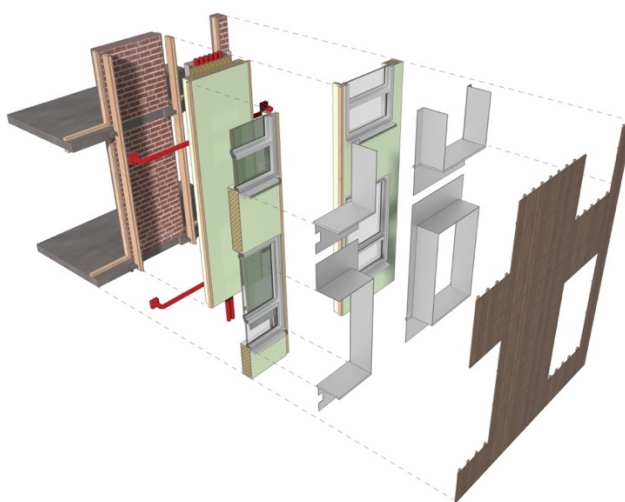
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158 Furthermore, the challenge of this solution consists in taking into account the influence of
159 different user profiles and occupants' behaviour in the performance of the building in order to
160 eliminate the uncertainties between the expected and the actual energy savings. This is a great
161 advantage over most of proposals that only aimed at a standard occupancy [31].

162

163 Table 1 summarise the main thermal and technical characteristics of the envelope and the
164 building services provided by the integrated facade module.

165



166

167 Figure 2. Exploded view of the façade module components ©2ndSkin, TU Delft.

168

169 Table 1. Main characteristics of the integrated facade module developed for the Dutch housing stock.

Parameters	Value	Unit	
Mechanical ventilation with heat recovery	7	l/s*person	
U-Value	Roof	0.22	W/m ² K
	Facade	0.15	W/m ² K
	Glazing	0.80	W/m ² K
	Window frames	0.80	W/m ² K
	Ground floor	0.29	W/m ² K
Airtightness	0.4	l/s*m ²	
Facade depth	30	cm	
Solar protection	Roller solar screen		

170

171 2.2. Case studies

172

173 In general terms, the target group for this research are the tenement apartment blocks massively
 174 built in the post-war period not only in the Netherlands and Spain, but also throughout Europe.

175 Table 2 summarises the main characteristics of the Dutch and southern Spanish building stock.

176 Initially, the proposed integrated facade module was designed for a reference building located in

177 Rotterdam (table 3), which was selected as the most common type in the area of investigation

178 while having typical characteristics found in the building stock analysis [29]. This building

179 (Figure 3a) is characterised as a mid-rise apartment block with central staircase, two apartments

180 per floor, and massive brick wall with cavity and no insulation.

181



182 Figure 3. Case studies. 3a. Rotterdam building (left). 3b. Seville building (right).

183 Table 2. Main characteristics of the Dutch and southern Spanish building stock.

		Netherlands [9, 11]	Southern Spain [10, 12]
Post-war dwellings in building stock		33%	46%
First thermal comfort regulation (year)		1975	1979
Morphological typology	Lineal	34%	44%
	Others	66%	56%
Predominant pre-renovated constructive systems		2 leaves of brick 1 leaf of prefabricated wall and 1 leaf of brick	2 leaves of brick 1 leaf of brick
% glazing on facade		42	19
Facade U-value exigency (W/m ² K)		0.22	1.25 – 0.55
Comfort standard	Winter	20 - 24 °C	17 - 20 °C
	Summer	23 – 26 °C	25 - 27 °C

184

185 Table 3. Annual standard climate values, period 1981 – 2010.

	Rotterdam [32]	Seville [33]
Elevation (in meters above sea-level)	4	34
Latitude	51° 57' 00'' N	37° 25' 0'' N
Longitude	4° 26' 00'' E	5° 52' 45'' W
Average temperature (°C)	10.4	19.2
Average maximum daily temperature (°C)	14.0	25.4
Average minimum daily temperature (°C)	6.4	13.0
Average relative humidity (%)	83.1	59
Average rainfall (mm)	855.6	539
Average n° days of rainfall \geq 1 mm	132	50.5
Average hours of sunlight	1624	2917

186

187 Table 4. Main typological and constructive characteristics of the case studies.

	Rotterdam case study	Seville case study
Tenure type	Tenants	Owners
Year of construction	1965-1974	1964
Typology	Apartment block; central staircase; two apartments per floor	Apartment block; central staircase; two apartments per floor
Nr. stores	4 (no elevator)	5 (no elevator)
Roof	Gravel, concrete (15 cm). (U-value = 2.5 W/m ² K)	Tile, coal dust and roof structure (20 cm). (U-value = 1.72 W/m ² K)
Facade	Brick (8 cm), air cavity and prefabricated wall (11 cm). (U-value = 1.7 W/m ² K)	Brick (11 cm), air cavity and brick (4 cm). (U-value = 1.53 W/m ² K) *Under windows just brick (11 cm). (U-value = 2.91 W/m ² K)
Window frame	Wooden (U-value = 2.2 W/m ² K)	Aluminium (U-value = 5.7 W/m ² K)
Glazing	Double (U-value = 4.3 W/m ² K)	Single (U-value = 7.7 W/m ² K)
Solar protection	None	Blinds

188

189 This research aims at evaluating the effect of the proposed facade retrofitting solution, which
 190 was designed for the Northern European Climate, on a building located in southern Spain
 191 (Mediterranean climate). Table 3 compares the climate characteristics. To be able to identify the
 192 effect of the climate differences, a building located in Seville, with very similar typological and
 193 constructive characteristics to the Rotterdam reference building, has been selected [7]. As
 194 already mentioned, this typology is also well-represented within the southern Spanish housing
 195 stock (table 2). It is a multi-family building of social housing built in the 60's (Figure 3b), with
 196 two apartments per floor of 58 m² each, and massive brick wall with cavity and no insulation.

197

198 Table 4 shows the similarities between the main typological and constructive characteristics of
 199 both case studies. As usual in southern Spain, the case study has only local cooling and heating

200 systems (in two of the three bedroom), with a sporadic use of them. This research focuses on the
201 energy behaviour assessment of a representative dwelling located in an intermediate floor of the
202 building.

203

204 *2.3. User profiles and occupancy patterns for energy simulations*

205

206 In a previous research phase, an intensive user analysis was carried out in parallel to the
207 technical design of the retrofitting solution, in order to feed back the users preferences in the
208 design and to reduce the pre-bound effect [31]. When real consumptions are much lower than
209 estimated ones, usually because users spend far less time in the dwellings than the time
210 established by the standardised use patterns, it is called pre-bound effect [26].

211

212 As a result of that user analysis, eight Dutch user profiles were developed based on a statistical
213 evaluation of the WoON dataset 2012 [34] (table 5). This research made use of those Dutch user
214 profiles and its occupancy patterns in the models developed for the energy simulations. The
215 effect of these patterns is evaluated in Rotterdam and Seville, in order to analyse and
216 differentiate the influence of the users' behaviour and the location in the energy performance of
217 the solution.

218

219 Given that there is no a statistical dataset about energy use preferences in Spain, four
220 representative profiles of social housing users were set up according to the analisys developed
221 in a previous research [7]. This user profiles are based on the cross-referenced of qualitative
222 data obtained from user surveys and quantitative data measured in some dwellings in this
223 climate (temperature, CO₂ concentration and electric consumption). These profiles represent
224 four use-intensity levels of the thermal conditioning systems (table 6):

225 - High intensity: standardised pattern, based on the Spanish regulation [12] but far from
226 the real situation of social housing in southern Spain.

227 - Medium intensity: nuclear family pattern.

- 228 - Low intensity: 2 adults pattern.
- 229 - Null intensity: 1 senior pattern, which are the users in fuel poverty. This pattern is not
- 230 contemplated in the case of Netherlands.

231

232 Table 5. Winter Dutch user profiles and occupancy patterns [31].

User Profile	Occupancy	Temperature	Night-time ventilation
1 Senior	Mon-Wed 1p 0-23h; Thu 1p 15-12h 0p 12-15h; Fri 1p 18-9h 0p 9-18h; Sat-Sun 1p 23-6h 0p 6-23h	24°C 18-23h; 20°C 23-18h	NO
2 Seniors	Mon-Thu 2p 0-23h; Fri 2p 18-9h 0p 9-18h; Sat 2p 23-9h 0p 9-23h; Sun 2p 23-6h 0p 6-23h	23°C 18-23h; 19°C 23-18h	NO
1 Adult	Mon-Tues 1p 0-23h; Wed 1p 15-9h 0p 9-15h; Thu 1p 18-9h 0p 9-18h; Fri-Sat 1p 23-6h 0p 6-23h; Sun 0p 0-23h	17°C 18-23h; 10°C 23-18h	NO
2 Adults	Mon-Wed 2p 0-23h; Thu-Fri 2p 18-9h 0p 9-18h; Sat-Sun 2p 23-6h 0p 6-23h	20°C 18-23h; 15°C 23-18h	NO
3 Adults	Mon-Wed 3p 0-23h; Thu 3p 15-9h 0p 9-15h; Fri 3p 18-9h 0p 9-18h; Sat-Sun 3p 23-6h 0p 6-23h	20°C 18-23h; 17°C 23-18h	NO
Single-parent	Mon-Tues 3p 0-23h; Wed 3p 15-12h 0p 12-15h; Thu 3p 15-9h 0p 9-15h; Fri 3p 18-9h 0p 9-18h; Sat-Sun 3p 23-6h 0p 6-23h	20°C 18-23h; 15°C 23-18h	NO
Nuclear family	Mon-Wed 3p 0-23h; Thu 3p 15-9h 0p 9-15h; Fri 3p 18-9h 0p 9-18h; Sat 3p 18-6h 0p 6-18h; Sun 3p 23-6h 0p 6-23h	20°C 18-23h; 18°C 23-18h	NO
Standardised	Mon-Wed 3p 0-23h; Thu 3p 15-9h 0p 9-15h; Fri 3p 18-9h 0p 9-18h; Sat 3p 18-6h 0p 6-18h; Sun 3p 23-6h 0p 6-23h	<i>Living room:</i> 21°C 7-23h; 15°C 23-7h <i>Bedrooms:</i> 18°C 7-16h; 15°C 16-7h	NO

233

234 Table 6. Winter southern Spanish user profiles and occupancy patterns [7].

User Profiles	Presence	Temperature	HVAC	Night-time ventilation
1 Senior	Mon-Fri 1p 17-10h 0p 10-17h; Sat-Sun 1p 0-23h	NO use	<i>Living room:</i> NO <i>Bedrooms:</i> NO	NO
2 Adults	Mon-Fri 2p 21-8h 1p 8-12h 0p 12-21h; Sat-Sun 2p 0-23h	20°C 21-23h	<i>Living room:</i> NO <i>Bedrooms:</i> YES	NO
Nuclear family	Mon-Fri 4p 21-8h 1p 8-14h 2p 14-21h; Sat-Sun 4p 21-10h 2p 10-21h	21°C 21-23h; 21°C 7-9h	<i>Living room:</i> YES <i>Bedrooms:</i> YES	NO
Standardised	Mon-Fri 4p 0-8h 1p 8-16h 2p 16-0h; Sat-Sun 4p 0-23h	17°C 0-8h; 20°C 8-0h	<i>Living room:</i> YES <i>Bedrooms:</i> YES	NO

235

236 Table 7. Summer southern Spanish user profiles and occupancy patterns.

User Profiles	Presence	Temperature	HVAC	Night-time ventilation
1 Senior	Mon-Fri 1p 17-10h 0p 10-17h; Sat-Sun 1p 0-23h	NO use	<i>Living room:</i> NO <i>Bedrooms:</i> NO	4 ach 21-11h
2 Adults	Mon-Fri 2p 21-8h 1p 8-12h 0p 12-21h; Sat-Sun 2p 0-23h	26°C 21-23h; 26°C 15-18h	<i>Living room:</i> NO <i>Bedrooms:</i> YES	4 ach 0-11h
Nuclear family	Mon-Fri 4p 21-8h 1p 8-14h 2p 14-21h; Sat-Sun 4p 21-10h 2p 10-21h	26°C 21-23h; 26°C 15-18h	<i>Living room:</i> YES <i>Bedrooms:</i> YES	4 ach 0-9h
Standardised	Mon-Fri 4p 0-8h 1p 8-16h 2p 16-0h; Sat-Sun 4p 0-23h	27°C 0-8h; 25°C 15-0h	<i>Living room:</i> YES <i>Bedrooms:</i> YES	4 ach 0-9h

237

238

239 In this last intensity pattern, the building's performance after the facade module application was
240 evaluated in terms of indoor temperature and not of energy demand, due to the absence of
241 energy consumption for heating and cooling. In order to evaluate if the indoor conditions are
242 adequate, two comfort temperature bands were defined as a good reference for the analysis of
243 the results. When assessing the quality of thermal environments, the main international
244 standards of comfort refer to Fanger studies [35], which defined two main indices: the Predicted
245 Mean Vote (PMV) and the Predicted Percentage of Dissatisfied (PPD). This methodology has
246 been incorporated in the standard EN ISO 7730 [36], in which the first temperature comfort
247 band of this research is based. The following conditions were set:

- 248 - Category of thermal environment: B (which means a PPD < 10%).
- 249 - Metabolic rate: 1.2 met.
- 250 - Clothing level: 1.0 clo (winter); 0.3 clo (summer).

251

252 There are also several studies considering that, when analysing comfort in buildings with no
253 active HVAC systems, adaptive standards are more reliable than the standard PMV index [37-
254 39]. This is mainly because in this kind of buildings users can modify their clothing insulation
255 or open and close windows depending on the outdoor conditions, so that is very difficult to

256 predict and set these variables. For this particular conditions, the ASHRAE Standard-55
257 described an optional method for determining acceptable thermal conditions [40], in which the
258 second temperature comfort band of this research is based. This methodology applies only to
259 spaces where the occupants are engaged in near-sedentary physical activities, with metabolic
260 rates ranging from 1.0 to 1.3 met. Also accounts for people's clothing adaptation and local
261 thermal discomfort effects in typical buildings, so it is not necessary to address these factors
262 when using this option. This method establishes an optimum comfort temperature (Equation 1)
263 and two acceptability ranges. In this research, the acceptability range corresponding to 90% of
264 satisfied occupants (which means a PPD < 10% and is defined by a temperature interval of ± 2.5
265 °C) was applied.

266

$$267 \quad T_{co} = 0.31 \times T_{ext,ref} + 17.8 \quad (1)$$

268

269 For the evaluation of the retrofitting solution during the summer period, the user profiles
270 maintain the same occupancy pattern, but the set-point temperature and the use of the
271 ventilation vary (table 7). In the Netherlands, no user profile contemplates the use of cooling
272 systems, as they are not common in the residential sector. In this case, the building's
273 performance after the integrated facade module application is evaluated in terms of comfort and
274 not demand. The night-time ventilation defined in Table 7 refers to the habit of users opening
275 the windows during the night, in order to dissipate the heat accumulated inside during the day.
276 To include night-time ventilation in the energy models, a 4 ACH rate of 'Natural Ventilation'
277 has been associated to the dwelling, activating it during the established schedule.

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284 3. Results

285

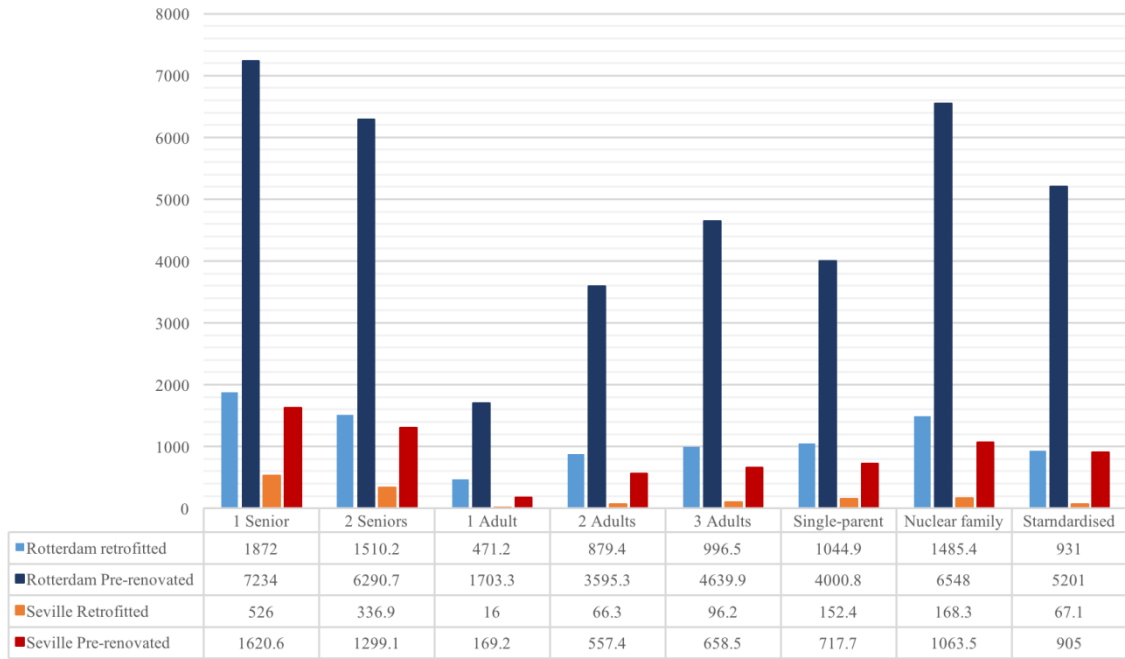
286 3.1. Winter analysis: heating demand and comfort conditions

287

288 The first step of this research is a heating demand analysis of the case study comparing the
289 results of the pre-renovated dwelling and the one incorporating the proposed integrated facade
290 module. Both energy models were located in Rotterdam and Seville and also simulated applying
291 the user profiles defined in the section 2.3 for the Netherlands (Figure 4) and southern Spain
292 (Figure 5). In the case of the southern Spanish patterns, the demand of ‘1 senior’ was not
293 analysed because it does not contemplate the use of heating systems.

294

295 As expected, the results show higher heating demands when we locate the model in Rotterdam
296 than in Seville. The retrofitting solution means very important savings in heating demand in
297 both cases. In Rotterdam, all the user profiles result in savings between 70 and 80%. Also in
298 Seville, savings between 70 and 90% are achieved. Even though the percentage of the savings in
299 Seville and Rotterdam are similar, net energy savings are lower in Seville due to the low heating
300 demands because its warmer climate. For example, with the Dutch standardised user profile, the
301 annual energy save in Rotterdam is around 4300 kWh while in Seville is around 800 kWh
302 (Figure 4). Similar differences are found when analysing different user profiles in the same
303 location. For example, in Rotterdam, with the highest intensity profile (‘1 senior’) the annual
304 energy save is around 5400 kWh while with the lowest intensity profile (‘1 adult’) is around
305 1200 kWh (Figure 4).

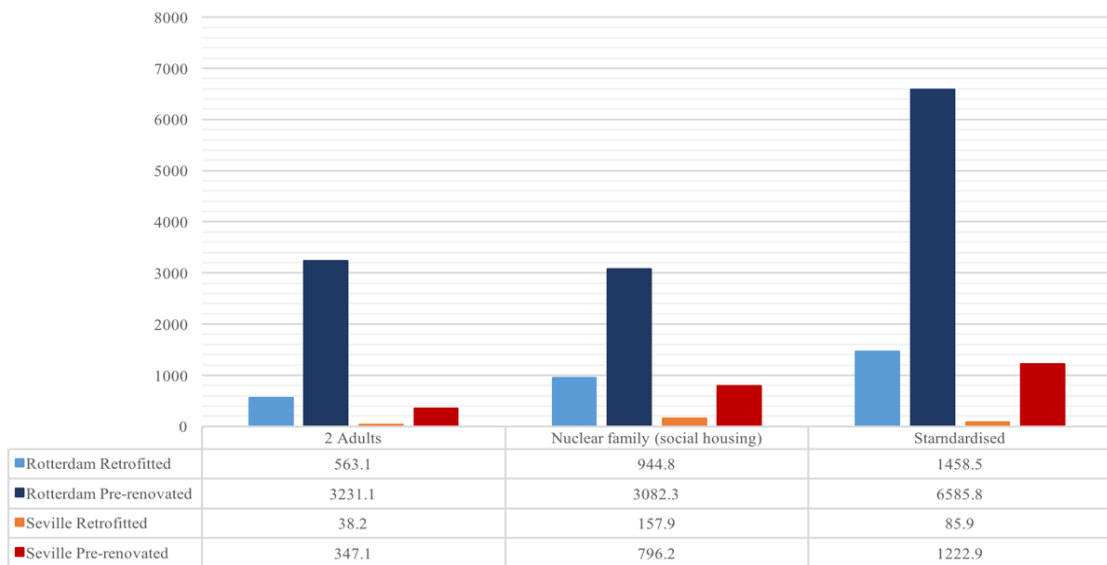


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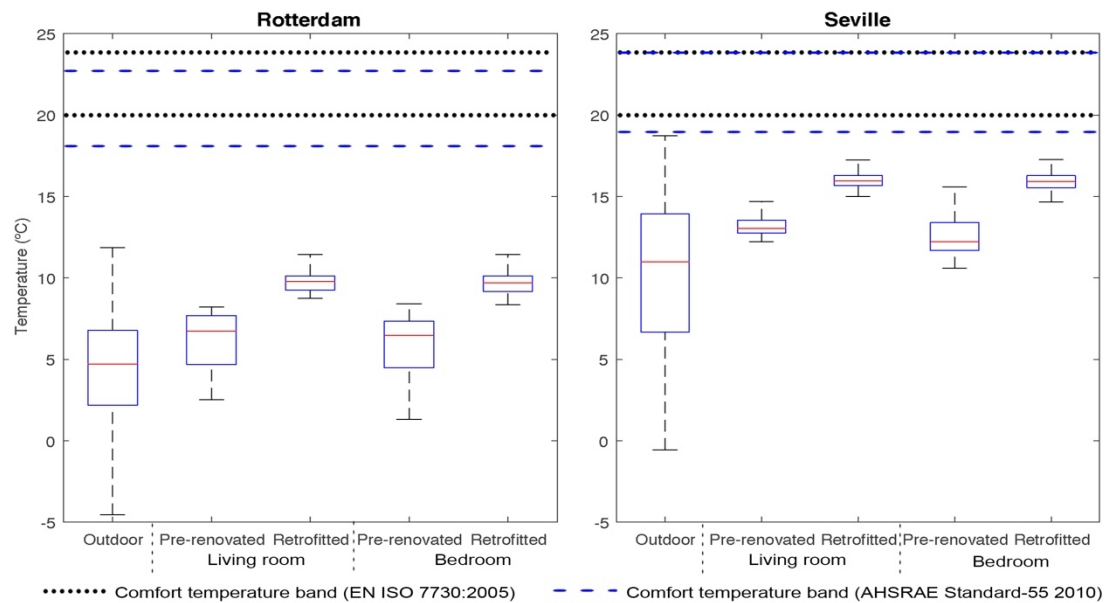
Figure 4. Heating demand (kWh/year). Dutch user profiles.



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310

Figure 5. Heating demand (kWh/year). Southern Spanish user profiles.



311

312

Figure 6. Temperature evolution (January). Spanish 1 senior (no additional heating used).

313

314 To evaluate the building's performance after the retrofitting solution application for the
 315 southern Spanish user profile with no any heating equipment ('1 senior'), the indoor
 316 temperature evolution was analysed developing a free-running simulation during the month of
 317 January. The results show that the retrofitting solution results in an internal temperature increase
 318 of up to 6 °C in Rotterdam and up to 5 °C in Seville (Figure 6). The lower the outdoor
 319 temperatures are, the higher the impact on indoor temperature produced by the insulating effect
 320 of the proposed integrated facade module.

321

322 Without using any heating system, the average indoor temperature in the retrofitted case study
 323 would be around 10 °C in Rotterdam and 16 °C in Seville. Despite the good performance of the
 324 building after applying the retrofitting solution regarding improved the indoor temperature, the
 325 thermal comfort conditions established by the EN ISO 7730 and the ASHRAE-55 Standard are
 326 not reached. In the case of Seville, with a warmer climate, the retrofitted dwelling gets closer to
 327 the comfort temperature band, but still without reaching it.

328

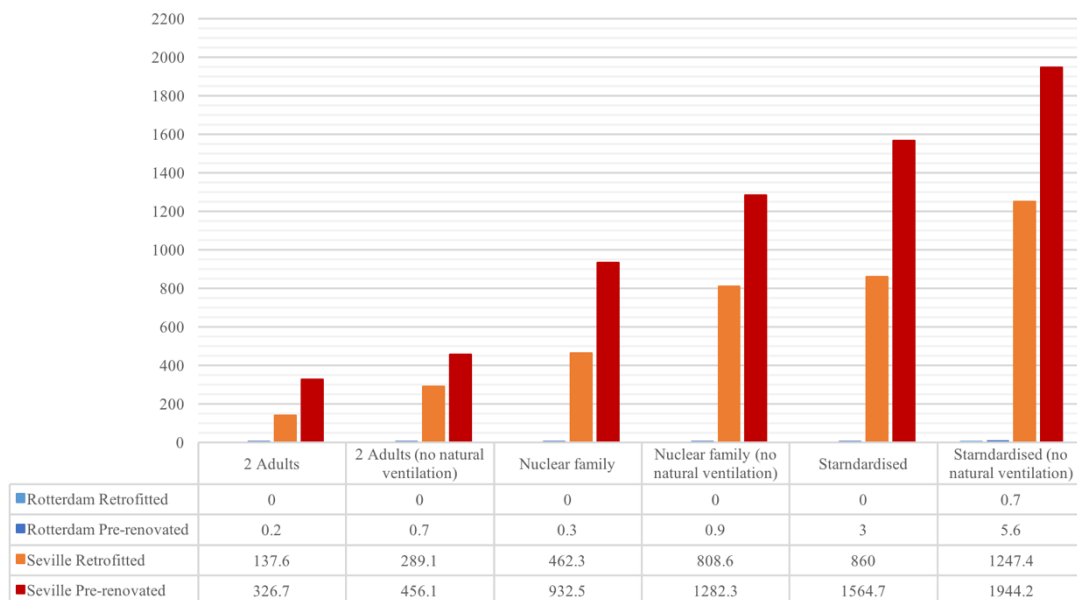
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330 3.2. Summer analysis: cooling demand and comfort conditions

331

332 To develop a cooling demand analysis, the same process described in the previous section for
 333 the heating demand was used. Energy models were simulated applying the user profiles defined
 334 for social housing in southern Spain (Table 7), since in the Netherlands the use of cooling
 335 systems in residential sector is not common. These profiles include the use of natural night-time
 336 ventilation for passive cooling, as it is a majority action in these location. Nevertheless, there
 337 are other users that do not ventilate during the nights, that is why the building’s performance
 338 after the facade module application was also evaluated in this case.

339



340

341 Figure 7. Cooling demand (kWh/year). Southern Spanish user profiles.

342

343 As expected due to its high temperatures during summer, the results show the largest cooling
 344 demand when we locate the model in Seville, while when we do in Rotterdam the cooling
 345 demand is almost zero (Figure 7). If the user does not contemplate the night-time ventilation,
 346 the cooling demand increases by around 30%. In Seville, the renovation facade module results
 347 in important savings in the cooling demand (50% in the user profiles with night-time ventilation
 348 and around 35% in the user profiles without it). Meaningful differences are found in net energy

349 savings when analysing different user profiles in Seville. For example, with the highest intensity
350 profile ('Standardised') the annual energy save is around 700 kWh while with the lowest
351 intensity profile ('2 adults') is around 200 kWh (Figure 7).

352

353 Assuming that the users originally did not ventilate the dwelling on their own and that the
354 ventilation system included into the retrofitting solution force the night-time ventilation, we
355 could associate to it a cooling demand savings of up to 70%. Therefore, in order to optimise the
356 proposed integrated facade module, at least in the case of southern Spain, its ventilation system
357 should ensure night-time air renewal for passive cooling, preventing excessive heat
358 accumulation.

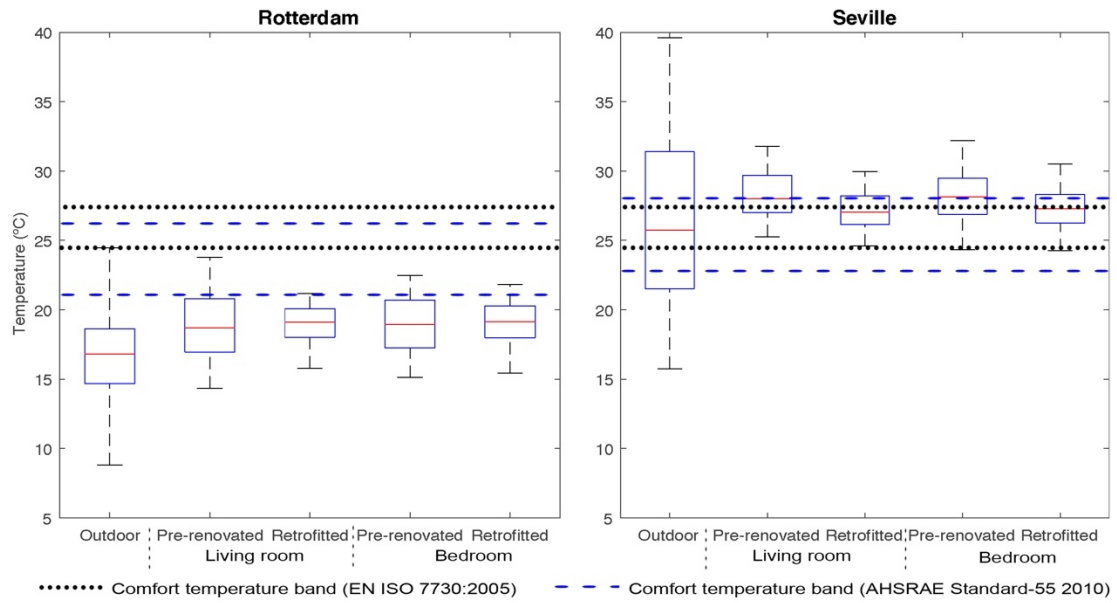
359

360 For the evaluation of the building's performance after the application of the retrofitting solution
361 when cooling equipment is not used, the indoor temperature evolution was analysed with a free-
362 running simulation during the month of August. The user profiles with the minimum (Spanish
363 '1 senior') and the maximum intensity of use and occupation (Dutch 'Nuclear family') were
364 selected. The results show that the retrofitting solution decreases the indoor temperature
365 maximum 2 °C both in Rotterdam and in Seville, coinciding with the maximum outdoor
366 temperature. However, the insulation effect fades away when the outdoor temperature
367 decreases, causing even increases of the indoor temperature due to heat accumulation in some
368 punctual cases.

369

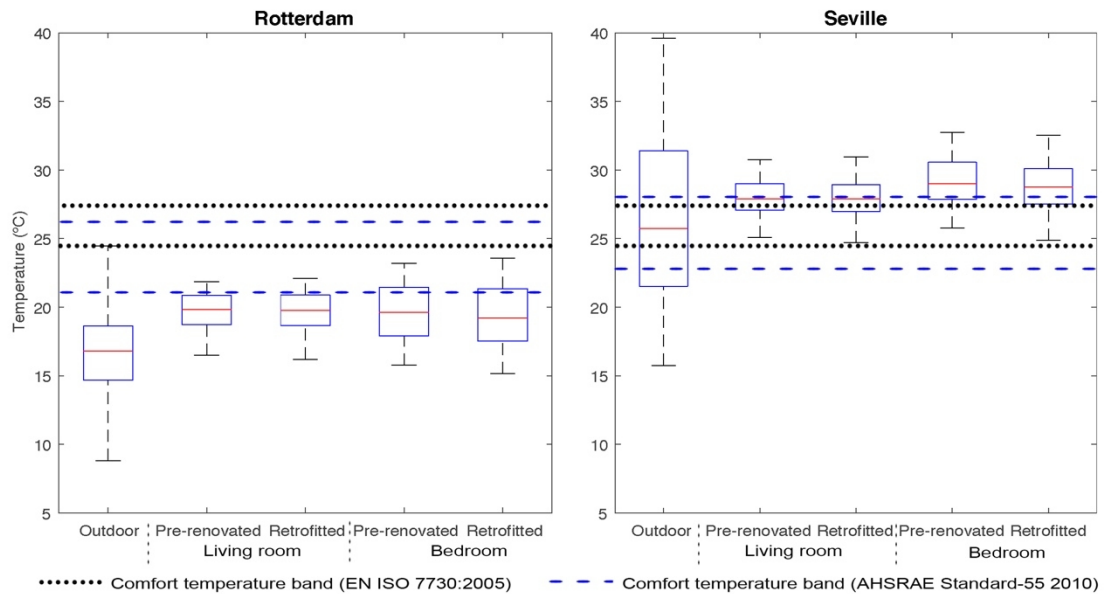
370 Without cooling system, the average indoor temperature in the Dutch case study (both before
371 and after being retrofitted) would be between 19 °C ('1 senior', Figure 8) and 20 °C ('Nuclear
372 family', Figure 9) and between 28 °C ('1senior', Figure 8) and 29 °C ('Nuclear family', Figure
373 9) in Seville. In the case of Rotterdam, the indoor temperature never exceeds the upper limits of
374 the comfort conditions established by the EN ISO 7730 and the ASHRAE-55 Standard. In the
375 case of Seville, the retrofitting solution leads to a decrease of more than 20% of hours of
376 discomfort (according to the ASHRAE-55) both with the Spanish '1 senior' user and the Dutch

377 'Nuclear family'. However, still after the retrofitting, the results show a high percentage of
 378 hours of discomfort: 35% ('1 senior') and 57% ('nuclear family'). During the summer, a higher
 379 occupation means worse indoor conditions, but the same effect of the proposed retrofitting
 380 solution.
 381



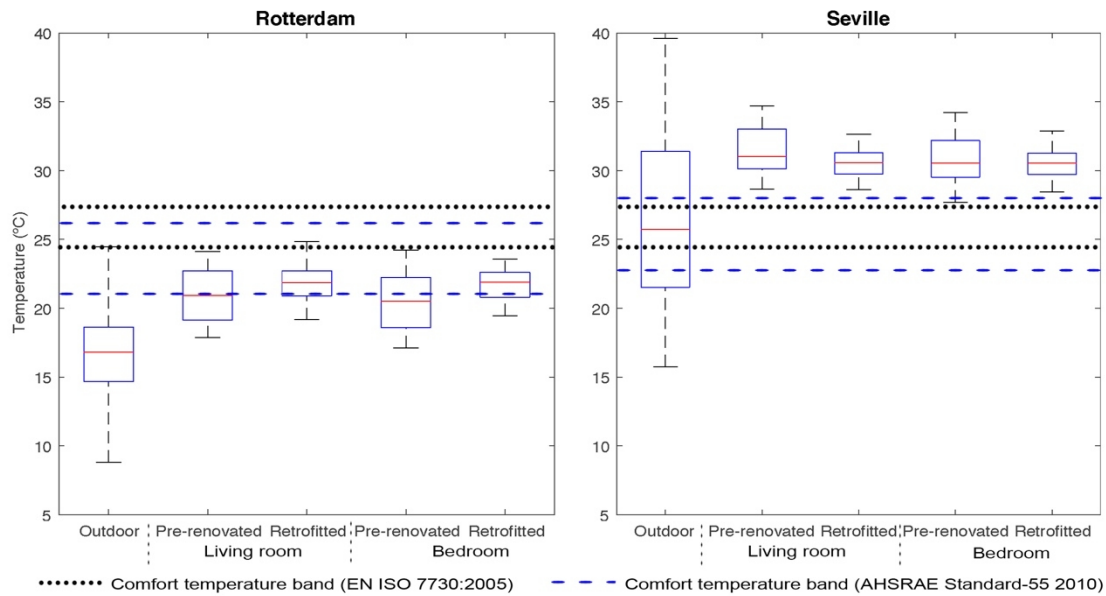
382
 383
 384

Figure 8. Temperature evolution (August). Spanish 1 senior.



385
 386

Figure 9. Temperature evolution (August). Dutch nuclear family.



387

388

Figure 10. Temperature evolution (August). Nuclear family with no night-time ventilation.

389

390 As it was done in the cooling demand analysis, the building's performance after the facade
 391 module application was also evaluated using a free-running simulation in the case of users who
 392 do not ventilate during the nights. Figure 10 shows the temperature evolution for the user
 393 profile with maximum intensity of use (Dutch 'Nuclear family').

394

395 It is observed that when removing the night-time ventilation function, indoor temperature
 396 increases in both locations, reaching an average indoor temperature in the retrofitted case study
 397 of around 22 °C in Rotterdam and 31 °C in Seville (Figure 10). Despite the increase of the
 398 indoor temperature, the model located in Rotterdam still does not exceed the upper limits of
 399 thermal comfort. However, for the model located in Seville, the absence of ventilation during
 400 nights means that 100% of the hours fall within discomfort temperature, even after the
 401 renovation. This results make evident that the proposed retrofitting solution for southern Spain
 402 climate, should ensure night-time air renewal for passive cooling preventing an excessive heat
 403 accumulation.

404

405

406 3.3. Annual analysis

407

408 After analysing the retrofitted building’s energy performance separately during both winter and
 409 summer season, its annual behaviour was evaluated. Also, in the second phase of the research,
 410 the variables described in figure 1 are introduced to the models in order to show how the
 411 retrofitting solution could be optimised according to the location. For this analysis, the results
 412 for the user profile with intermediate demand from both the Netherlands and southern Spain
 413 (Dutch ‘3 adults’ and Spanish ‘Nuclear Family’) are shown.

414

415 Table 8 shows a compilation of the results obtained in the previous sections from the models
 416 with the average user profile for the location of Rotterdam and Seville. As it can be observed,
 417 the annual percentage of savings is lower in the southern Spanish user profile, since the
 418 performance of the proposed integrated facade module is lower during the summer. As far as
 419 the total demand savings in absolute value are concerned, the saving of the model located in
 420 Rotterdam with the average Dutch user profile is 3.3 times higher than in the one located in
 421 Seville with the average southern Spanish user profile. This comparison makes evident that in
 422 the case of southern Spain it would be essential to reduce the economic investment of the
 423 retrofitting solution, because the annual demand savings are much lower than in the Netherlands
 424 and the payback time would be decompensated.

425

426 Table 8. Compilation of the demands and savings due to the retrofitting.

		Pre-renovated					Savings (Pre-renovated → retrofitted)			
User Profile	Location	Heating demand	Cooling demand	Cooling (no night vent.)	Total demand	Total (no night vent.)	(%)	(kWh)	No night vent. (%)	No night
3 Adults	Rotterdam	4639.9	-	-	4639.9	-				
Nuclear family	Seville	796.2	932.5	1282.3	1728.7	2078.5				
		Retrofitted								
User Profile	Location	Heating demand	Cooling demand	Cooling (no night vent.)	Total demand	Total (no night vent.)	(%)	(kWh)	No night vent. (%)	No night
3 Adults	Rotterdam	996.5	-	-	996.5	-	78.5	3643.4	-	-
Nuclear family	Seville	157.9	462.3	808.6	620.2	966.5	64.1	1108.5	53.5	1112

427

428

429 In order to identify how the performance of the proposed integrated facade module can be
430 optimised, the effect on the energy demand of another two variables added to the forced night-
431 time ventilation were analysed. The two characteristics of the facade module with the most
432 influence on the thermal energy demand were selected: insulation thickness and airtightness
433 [41].

434

435 Originally, the designed solution has an insulation thickness of 20 cm, which results in a
436 considerably higher thermal conductivity coefficient U-value compared to Spanish requirements
437 [12]. The Spanish regulation establishes a U-value requirement of 1 W/m²K for the Seville
438 climatic zone, while the proposed integrated facade module provides a U-value of 0.15 W/m²K.
439 Therefore, the performance of the same solution but with an insulation thickness of 10 cm was
440 evaluated, thereby increasing the U-value of the facade to 0.28 W/m²K, still far below the
441 Spanish requirements.

442

443 The results show that by reducing the insulation level both the heating and cooling demand
444 increase in all cases (table 9). But it is important to analyse this demand increase in absolute
445 value, because while in the model located in Rotterdam with the average Dutch user profile this
446 increase is 190.3 kWh per year, in the model located in Seville with the average southern
447 Spanish user profile is only 75.6 kWh per year.

448

449 The investment cost of wall insulation is set equal to 7.5 €/m² per each 10 cm of thickness [42].
450 So in this case, the reduction of the insulation level would save 270 €/dwelling in the initial
451 investment cost of the retrofitting. The actual cost of electricity use in Spain is 0.22 €/kWh
452 [43], so reducing the insulation level would make tenants pay 6.65 € more per year in the case
453 of Seville. The payback period in this case is more than 40 years, so for southern Spain it is not
454 worth investing in 20 cm insulation thickness because 10 cm is enough. A more detailed
455 economic study is outside the scope of this article.

456

457 Also, the originally designed solution has an airtightness of 0.65 ACH, while ASHRAE-119
458 Standard [44] establishes that a dwelling with a normalized leakage (NL) greater or equal to 0.4
459 ACH is permeable enough to not require additional mechanical ventilation systems in mild and
460 medium climates. Therefore, taking into account that the proposed solution includes a
461 mechanical ventilation system that ensure a good air quality, the performance of the same
462 window solution but with an airtightness of 0.4 ACH was evaluated.

463

464 The results show that by increasing the airtightness of the solution both the heating and cooling
465 demand decrease in all cases (except the cooling demand when night-time ventilation is not
466 considered, due to that this sealing excess causes heat accumulation) (table 10). This
467 airtightness improvement means a decrease of the total demand of 485.5 kWh per year in the
468 model located in Rotterdam with the average Dutch user profile and 164.4 kWh per year in the
469 model located in Seville with the average southern Spanish user profile.

470

471 Table 9. Compilation of the demands and savings due to the insulation thickness variation.

User Profile	Location	Facade module less insulation: U = 0.28 W/m ² K (10 cm insulation)					Savings (Original facade module U = 0.15 W/m ² K → less insulation)			
		Heating demand	Cooling demand	Cooling (no night vent.)	Total demand	Total (no night vent.)	(%)	(kWh)	No night vent. (%)	No night vent. (kWh)
3 Adults	Rotterdam	1186.8	-	-	1186.8	1186.8	-19.1	-190.3	-	-
Nuclear family	Seville	211.9	483.9	821.4	695.8	1033.3	-12.2	-75.6	-6.9	-67

472

473 Table 10. Compilation of the demands and savings due to the airtightness.

User Profile	Location	Facade module more airtight: 0.4 ACH					Savings (Original facade module: 0.65 ACH → more airtight)			
		Heating demand	Cooling demand	Cooling (no night vent.)	Total demand	Total (no night vent.)	(%)	(kWh)	No night vent. (%)	No night vent. (kWh)
3 Adults	Rotterdam	511	-	-	511	-	48.7	485.5	-	-
Nuclear family	Seville	8.9	446.9	849.6	455.8	858.5	26.5	164.4	11.2	108

474

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478 3.4. Total energy performance

479

480 In this section we integrate the results of the energy simulations, together with an estimation of
481 energy demand for hot water, domestic appliances and artificial lighting. Furthermore the
482 renewable energy generation that would be necessary to achieve nearly zero energy
483 consumption is calculated. In the case of the Netherlands, the estimation of energy demand for
484 hot water, appliances and artificial lighting was obtained from calculations based on Dutch
485 regulations and on the statistical profiles established from the WoON dataset [45]. In the case of
486 southern Spain, the estimation of energy demand for hot water was calculated from the demand
487 established by the Spanish regulations [12] and for the appliances and artificial lighting it was
488 based on the statistical data obtained in the SECH-SPAHOUSEC project [46]. The necessary
489 PV panels to cover the renewable energy generation according to the building characteristics
490 were calculated with the PVsyst 6.4.9. software [47].

491

492 Table 11 shows the results obtained from the model with the average Dutch user profile ('3
493 adults') located in Rotterdam and the model with the average southern Spanish user profile
494 ('Nuclear family') located in Seville. As it can be observed, the total demand is a 13.4% lower
495 in Seville than in Rotterdam. When this is added to a highest solar radiation in southern Spain
496 than in the Netherlands, it translates into a need of a half of the PV panels surface in the model
497 located in Seville with respect to the one located in Rotterdam. As a result, the possibility of
498 reaching the nZEB in the model located in Seville is in the building itself, whereas in the model
499 placed in Rotterdam an extra surface to install more PV panels would be required, since the case
500 study building has a roof area around 150 m². This aspect significantly reduces the economical
501 investment of the proposed integrated facade module in southern Spain with respect to the
502 Netherlands.

503

504

505

506 Table 11. Compilation of the demands and necessary PV area, to cover the demand.

User Profile	Location	Heating	Cooling	Hot water	Appliances	Total	m ² PV (per dwelling)	m ² PV (building)
3 Adults	Rotterdam	996.5	0	1680.8	3222	5899.3	35	350
Nuclear family	Seville	157.9	462.3	1430	3060	5110.2	17	170

507

508

509 4. Conclusions

510

511 The paper presented a study that compared the resulting energy performance and optimisation
 512 potential of an integrated facade renovation module with different climates and user profiles.
 513 Relevant typology similarities have been detected between the Dutch and the southern Spanish
 514 housing stock, which makes possible the analysis of the adaptability of the proposed integrated
 515 facade module (originally designed for the Dutch stock) to the southern Spanish climate. Also
 516 important constructive similarities have been found, which shows that at least initially the
 517 proposed solution can be built over the Spanish buildings envelope.

518

519 After the retrofitting solution performance analysis (both in terms of demand and thermal
 520 comfort), the following conclusions have been drawn:

521

- 522 - The proposed solution achieves heating demand savings between 70 and 90% in both
 523 Rotterdam and Seville models, and increases of the indoor temperature up to 6 °C in
 524 Rotterdam and 5 °C in Seville when the house is free-running during the winter.
- 525 - Even though the percentage of the savings in Seville and Rotterdam are similar, the
 526 same does not happen when we analyse net energy savings. A difference of 3500 kWh
 527 is found between the heating demand reduction due to the retrofitting in Rotterdam
 528 and Seville (for the Dutch user profile with intermediate demand). Something similar
 529 happen when we analyse the influence of the user profile in net energy savings. A

530 difference up to 4200 kWh is found between the highest and lowest intensity Dutch
531 user profile.

532 - The proposed solution achieves cooling demand savings around 50% in Seville (with
533 night-time ventilation) and decreases of the indoor temperature up to 1°C when the
534 house is free-running during the summer. If it is considered that the original user did not
535 ventilate during the night and the facade module forces it, cooling demand savings of up
536 to 65% are obtained in Seville and decreases of the indoor temperature up to 5 °C when
537 the house is free-running. Thus, to optimize the originally proposed solution in the case
538 of southern Spain the ventilation system should ensure night-time air renewal for
539 passive cooling.

540 - As the cooling demand in the pre- and post-retrofitted models in Rotterdam is almost
541 zero, a difference of 470 kWh is found between the cooling demand saving in
542 Rotterdam and Seville (for the southern Spanish user profile with intermediate
543 demand). Also a difference up to 500 kWh is found between the highest and lowest
544 intensity southern Spanish user profile.

545 - The proposed solution works properly in southern Spain, but annual heating and cooling
546 demand savings in absolute value are 3.3 times lower than in the Netherlands (for a user
547 with intermediate use intensity). In southern Spain the economic investment of the
548 facade module should be reduced.

549 - If the insulation thickness of the proposed solution is reduced from 20 to 10 cm, heating
550 and cooling demand increase. But in absolute value, this increase in Seville is only 75.6
551 kWh per year. It is not worth investing in double insulation thickness because its
552 payback period would take more than 40 years.

553 - If we reduce the air permeability of the proposed solution from 0.65 to 0.4 ACH,
554 heating and cooling demand decrease. In absolute value, this decrease is 485.5 kWh per
555 year in Rotterdam and 164.4 kWh per year in Seville. It is worth investing in the

556 airtightness improvement (ensuring a good indoor air quality) because an important
557 improvement in savings would be obtained.

558 - When the building is retrofitted total demand is a 13.4% lower in Seville than in
559 Rotterdam. Due also to a highest solar radiation, in Seville the PV panels surface
560 necessity is half than in Rotterdam. This means an important reduction of the
561 economical investment to reach the nZEB in southern Spain with respect to the
562 Netherlands.

563

564 These results demonstrate a high influence of the user profile in the heating and cooling demand
565 saving, at the same level of importance that the location of the case study. Because of that, all
566 the retrofitting analysis should take into account real user profiles and not just the standardised
567 ones.

568

569 The next step of this research should be a more detailed economic analysis of the energy
570 savings and investment. The results on energy savings optimisation can support the financial
571 feasibility analysis. Moreover, the renovation of the building stock has social implications as the
572 residents are involved and need to accept the proposed interventions. As such the social
573 acceptance in southern Spain of the proposed integrated facade module should be evaluated.
574 Finally, the analysis of the political barriers to self-consumption and energy production would
575 be important to propose strategies to increase the renovation rates and support the european
576 decarbonisation goals.

577

578

579 **Acknowledgements**

580

581 This research was partially funded by the V Internal Research Plan of the Universidad de
582 Sevilla.

583

584 This research was carried out within the research projects: ‘2ndSkin’, funded by the Building
585 Technology Accelerator Flagship Program (BTA) of the European Climate KIC and by the
586 Dutch Top sector Energy (TKI); ‘Intervención en barriadas residenciales obsoletas: Manual de
587 buenas prácticas’ (ref. 2013-0000006939), funded by the Andalusian Regional Government;
588 and ‘REFAVIV: Rehabilitación energética de las fachadas de viviendas sociales deterioradas
589 aplicando productos innovadores nacionales (DIT) y europeos (DITE)’ (ref. BIA2012-39020-
590 C02-01), funded by the Spanish Government.

591

592

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