

Overview of the JET results

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Abstract

Since the installation of an ITER-like wall, the JET programme has focused on the consolidation of ITER design choices and the preparation for ITER operation, with a specific emphasis given to the bulk tungsten melt experiment, which has been crucial for the final decision on the material choice for the day-one tungsten divertor in ITER. Integrated scenarios have been progressed with the re-establishment of long-pulse, high-confinement H-modes by optimizing the magnetic configuration and the use of ICRH to avoid tungsten impurity accumulation. Stationary discharges with detached divertor conditions and small edge localized modes have been demonstrated by nitrogen seeding. The differences in confinement and pedestal behaviour before and after the ITER-like wall installation have been better characterized towards the development of high fusion yield scenarios in DT. Post-mortem analyses of the plasma-facing components have confirmed the previously reported low fuel retention obtained by gas balance and shown that the pattern of deposition within the divertor has changed significantly with respect to the JET carbon wall campaigns due to the absence of thermally activated chemical erosion of beryllium in contrast to carbon. Transport to remote areas is almost absent and two orders of magnitude less material is found in the divertor.

Keywords: JET, tokamaks, magnetic confinement

(Some figures may appear in colour only in the online journal)

1. Introduction

The European fusion programme is moving into the phase of implementation of its Roadmap [1] that foresees the use of JET in Horizon 2020 as the main risk-mitigation element for the preparation of ITER operation. In 2004 the JET programme in support of ITER was launched consisting of three main elements [2]: (i) the installation of an ITER-like wall (ILW) to reproduce the same material mix for the plasma-facing components (PFCs) of the nuclear phase of ITER; (ii) the development of plasma regimes of operation in the same configuration as ITER; and, (iii) a deuterium–tritium experiment to test the integrated regimes with the fuel mix of ITER. During the last couple of years, the ILW characterization has been almost completed. Significant progress has been made on scenario development and the preparation of the DT campaign has started.

In 2013 and 2014, JET carried out experimental campaigns in deuterium at plasma currents I_p up to 4 MA, magnetic field B_t up to 3.7 T and auxiliary power up to $P_{\text{NBI}} \sim 27$ MW, $P_{\text{ICRH}} \sim 7$ MW, $P_{\text{LHCD}} \sim 3$ MW. The upgraded components of the neutral beam system (the newly configured sources, the actively cooled ducts and the high voltage power supplies (HVPS)) have all separately achieved the design targets. However, problems with the old HVPS equipment and a major water leak in one injection box at the end of 2013 have prevented the achievement of the maximum neutral beam power needed for a full scenario optimization with the

ILW at plasma currents beyond 2.5 MA. Nevertheless, after three years of operation with ILW (referred to in the following as the JET-ILW configuration) the JET heating systems have improved on the performance achieved with the carbon wall (the JET-C configuration) (figure 1) The JET experience with the ILW shows the need of a careful preparation (as now integrated in the ITER research plan with the choice of the W divertor from the start of ITER operation) and a proper real-time protection system for the PFCs in order to achieve continuous improvement in the plasma performance.

During this period, the ILW characterization has focused on the consolidation of the basis for the ITER decision on the first divertor [3, 4] with a specific emphasis given to the bulk tungsten melt experiment to understand the effect of shallow melting due to transient events. For this purpose, a protruding divertor lamella has been installed in the most internal stack of the horizontal tile. A series of seven reproducible discharges produced shallow melting of tungsten and demonstrated the possibility of operating JET in these conditions without the occurrence of disruptions. The molten layer dynamics has been successfully modelled using the MEMOS code to validate the model and to allow a meaningful extrapolation to ITER. The results have been crucial for the final decision in favour of the tungsten divertor from the start of ITER operation.

In the first JET campaigns with the ILW [5–7] fuel retention and material migration studies had priority [8–11]. Now the focus of JET experiments has shifted towards integrated scenario development [12] to achieve low PFC heat loads [13–15] and avoid tungsten accumulation [16, 17] with

^a See the appendix.

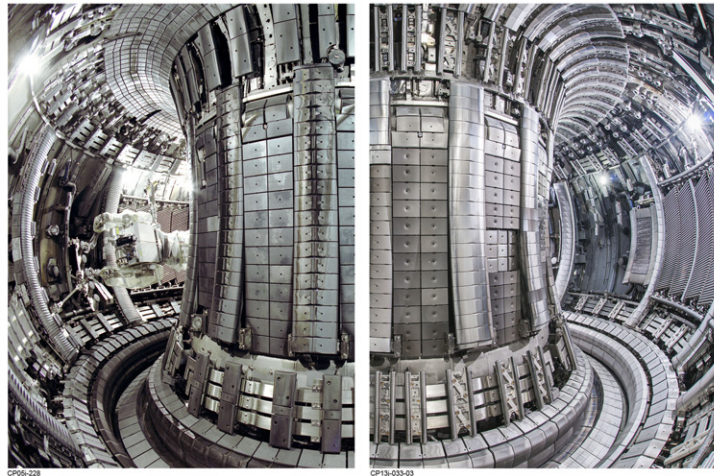


Figure 1. Picture of the interior of the JET vessel with an all carbon wall (JET-C) on the left and with the ITER-like wall (JET-ILW) with beryllium main chamber and tungsten divertor on the right.

the ultimate goal of achieving high performance plasmas [18, 19] in view of the DT experiment. Magnetic geometry, strike point location and divertor pumping were established as key aspects for achieving good H-mode confinement, leading to the re-establishment of long-pulse (~ 9 s) high-confinement H-modes at 2.5 MA. This had to be combined with the control of tungsten accumulation by central heating using ion cyclotron resonant heating (ICRH) and sufficient gas fuelling. Significant effort was devoted to the use of impurity seeding [20] to produce core-divertor compatible scenarios which are essential for ITER, as well as high radiative scenarios which are required for DEMO. Stationary discharges have been produced by nitrogen seeding with fully detached divertor legs and small edge localized modes (ELMs). The use of N-seeding clearly increases the pedestal pressure but the global confinement is still 15% below the IPB98(y,2) scaling.

Comparisons between baseline and hybrid plasmas have blurred the distinction between the two scenarios, which now appear on JET-ILW as a single operating domain. Dedicated power scans to elucidate the dependence on plasma beta of the energy confinement time have confirmed that on JET the power degradation is normally much weaker than the prediction of the IPB98(y,2) scaling.

Post-mortem analyses of the PFCs retrieved from the first ILW campaigns [21–24] have confirmed the previously reported low fuel retention obtained by gas balance, with the measured deuterium inventory below 0.25% of the injected amount of deuterium (a factor 16 below that for the carbon wall). These studies show that the reduced material erosion and migration lead to reduced trapping of fuel in deposited beryllium layers which incorporate less fuel in comparison with carbon layers. In addition, the pattern of deposition within the divertor has changed significantly with the ILW in comparison with the JET carbon wall [25] due to the lower level of re-erosion. Transport to remote areas is almost absent, with the only significant beryllium deposits ($\sim 15 \mu\text{m}$) found on the apron of the inner divertor. Overall, one order of magnitude lower deposition rate is found in the divertor compared to the carbon wall, with deposits in the floor of less than $2 \mu\text{m}$ compared with more than $200 \mu\text{m}$ thick deposits found after

the last JET carbon-wall campaign due to long range migration via chemical erosion. These results are well reproduced by the WallDYN code. The WallDYN extrapolation to ITER shows a reduction in the retention by more than a factor ten and implies that at least 3000 full power DT discharges could be produced on ITER before reaching the T-inventory limit. This is comparable with the time estimated to obtain a substantial erosion of the divertor.

The investigation of effective runaway electron (RE) beam mitigation methods has continued. Spontaneous generation of REs is not normally observed in JET-ILW. Runaways can be generated through massive Ar injection and accelerated up to 20 MeV with the production of runaway currents up to 1.2 MA. On JET, runaways can be suppressed by D_2 injection provided injection takes place before the thermal quench. Thereafter, runaway suppression using high-Z noble gases has been attempted but was found so far ineffective.

In section 2 we give an overview of all major results obtained with the ILW and the implications for ITER operation. In section 3 the development of ITER-relevant scenarios in the new all-metal environment is presented, along with confinement and edge pedestal physics results. Conclusions and perspectives are presented in section 4.

2. Operation of JET with the ILW

2.1. Bulk tungsten melt experiment

A dedicated experiment has been carried out in JET to address the uncertainties associated with predicting the impact of transient tungsten melting in ITER due to ELMs [26–29]. The horizontal tile of the JET divertor is made of solid tungsten arranged in four stacks of lamellae in order to minimize the electromagnetic loads during disruptions (figure 2). JET's large size makes it possible to produce repetitive ELMs with sufficient energy (~ 300 kJ per ELM) to melt tungsten. Deliberate shallow tungsten melting has been produced by operating with the outer strike point on one protruding lamella, intentionally modified and installed in one divertor module on the innermost stack as shown in figure 2 [29]. A series of seven identical 3 MA discharges with 23 MW of heating power

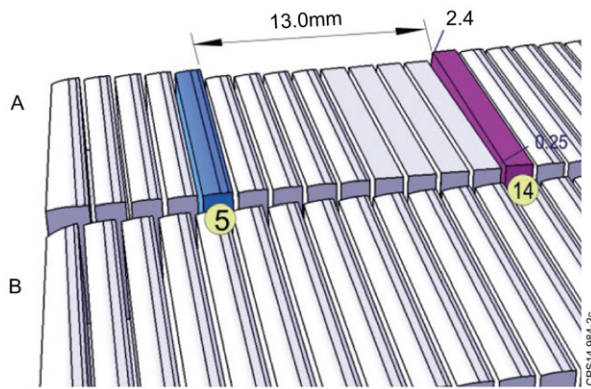


Figure 2. Schematic view of the lamella assembly in the modified stack.

were produced. Within 1 s the base temperature of the lamella was raised to a value well below the melting temperature, but sufficiently high to facilitate the shallow melting by ELMs with parallel power densities around 3 GW m^{-2} during a further 0.5 s. The temperature on the top-side of the protruding and normal lamellae is measured by the infrared cameras. The top view does not allow resolved measurements on the side of the special lamella and this has made the interpretation more complex. The temperature measurements from the normal lamellae do not suffer the same problems and are used to deduce incident power fluxes as input for a 3D modelling of the heat transport through the special lamella with the exposed edge. The results are consistent with melting by ELMs followed by re-solidification of tungsten in between events. The melting produced an enhanced tungsten source with occasional expulsion of small droplets ($80\text{--}100 \mu\text{m}$) which did not significantly impact the main plasma and caused no disruptions during the experiments or thereafter. Almost 1 mm depth (corresponding to a volume of $\sim 6 \text{ mm}^3$) was moved/removed from the edge by several hundred ELMs during these pulses. The temperature of the special lamella is shown in figure 3 [30] and compared with that of a standard lamella. The analysis confirms that transient melting during the ELMs occurs and not bulk melting that continues across the ELM cycle. From photographic evidence it is possible to say that most of the molten tungsten moved along the lamella edge although a precise mass balance will be possible only after post-mortem analysis. The propagation of molten material is consistent with a $\mathbf{j} \times \mathbf{B}$ driving force, where \mathbf{j} is the current density into the surface (mainly due to thermo-electronic emission) and \mathbf{B} is the local magnetic field [31]. Droplets on the lamella were seen to coalesce and grow, which increases the risk for longer pulse duration above the melt threshold. Nevertheless, the consequences of melting had no significant impact on JET operation.

The inferred power load on the side of the JET special lamella was substantially lower than expected. In order to match the IR measurements, the tungsten evaporation rate inferred from the $\text{W I } 400.88 \text{ nm}$ line and the Planck radiation, the side heat loads must be reduced by a factor 2.5 in these H-mode discharges (a larger reduction factor of about five is needed to match the measurements in L-mode). This result is not yet understood: simulations including the gyro-radius smoothing effects predict only a 20% reduction [32],

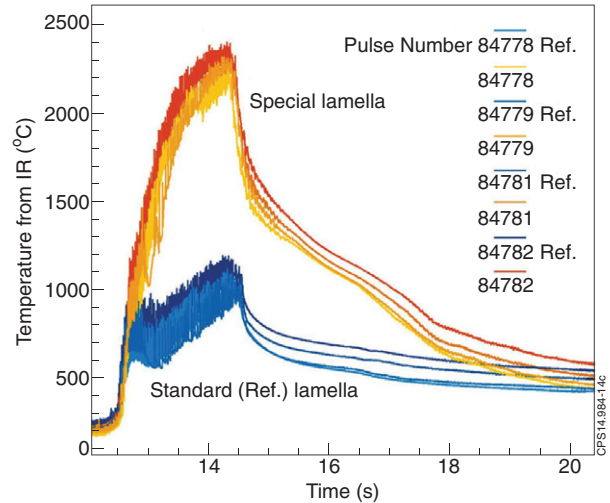


Figure 3. Temperature measurement for a few JET pulses used in the bulk tungsten melt experiment. Temperatures are shown for both the reference and the special lamella.

whereas the effect of vapour shielding may have contributed to the power load mitigation in H-mode where the surface temperature was near melting but could not explain the L-mode results where the surface is much colder. Although not understood, this finding has potentially positive implications for ITER, which may be less sensitive than previously feared to exposed edges created by chipping of mono-block edges or components outside tolerance.

JET results are consistent with simulations of tungsten melting and propagation using the MEMOS code [33], which has been used to inform decisions on the choice of tungsten as the material for the first divertor in ITER. The results have also given confidence that flash melting of the tungsten divertor elements by ELMs is relatively benign compared to bulk melting as reported in other experiments [34].

2.2. Material erosion and migration, fuel recycling and retention

The JET ILW experiment provided for the first time the opportunity to explore the coupling between tokamak plasma operation and plasma–surface interaction in the beryllium/tungsten material environment of ITER, complementing earlier experiments in other divertor tokamaks with metallic walls such as ASDEX Upgrade [35–39] and Alcator C-Mod [40–42]. These experiments are crucial in order to validate physics models and modelling tools for ITER with regard to material erosion and migration, fuel recycling and retention and impurity concentration and radiation.

The observed strong inter-connection of plasma–surface interaction with plasma–edge physics such as pedestal or divertor properties revealed that the impact of the first wall material on the plasma performance as well as the prominent role of chemical erosion of carbon in the main chamber and divertor was previously underestimated. The change in material migration with the JET-ILW can be seen as one key result as it impacts directly or indirectly on the majority of plasma–surface interaction processes mentioned above and contradicts partially the migration pattern predictions made

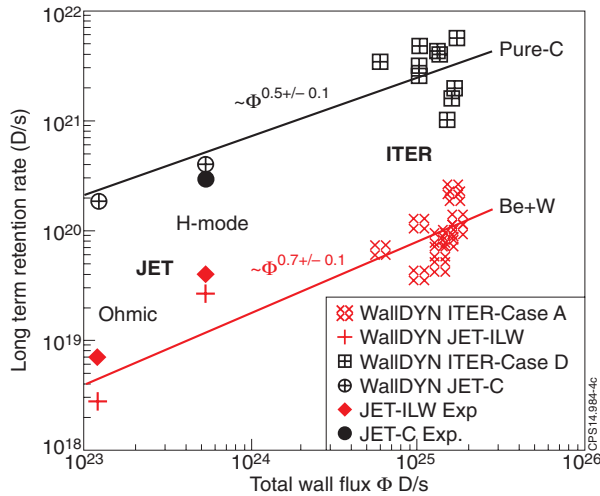


Figure 4. Long-term retention rate predictions for ITER made by WALLDYN [45].

for beryllium/tungsten PFCs on basis of migration physics deduced in JET-C including physical erosion characteristics of Be and W.

The primary source of Be sputtered in the Be main chamber wall is a factor of five lower than C sputtered in JET-C. The initial assumption that pure physical sputtering by energetic charge exchange neutrals is solely determining the main chamber source turned out to be invalid—low energetic ions reaching the first wall also sputtered chemically the C in JET-C. This chemical erosion at lowest energies (10 eV) is absent due to energetic physical sputtering thresholds for Be—even if chemical assisted physical sputtering has been found for Be [43]. As consequence of the lower initial impurity source, the inner divertor is only partially covered by Be and indeed intact W surfaces are found. The local Be flux balance at the strike-line area is in favour of Be reflection and re-erosion and due to the low incoming flux not in deposition.

Furthermore, the virtual absence of chemical sputtering of beryllium inhibits the cycle of multiple erosion/deposition cycles within the divertor observed with carbon PFCs. Instead beryllium remains deposited at the positions where it lands after reflection or a physical sputtering process above the energetic threshold. It should be noted that, due to the low deposition rate and the limited operational time on JET, the JET-ILW migration pattern could represent an intermediate state with respect to long-pulse operation. This is supported by the fact that two orders of magnitude less dust were recovered compared with the carbon wall.

A special effort was made to accurately quantify the reduction in long-term fuel retention with the JET-ILW, already measured in gas balance experiments, through post-mortem analysis. These results were used to validate the WALLDYN code [44] and to allow a meaningful extrapolation to ITER. The code simulations reproduce both the reduction in fuel retention and the observed migration pattern. The remaining long-term retention is caused by implantation and co-deposition with beryllium and residual impurities. Short-term retention gained relative importance with respect to the low level of long-term retention and impacts on the recycling properties of both beryllium and tungsten and local

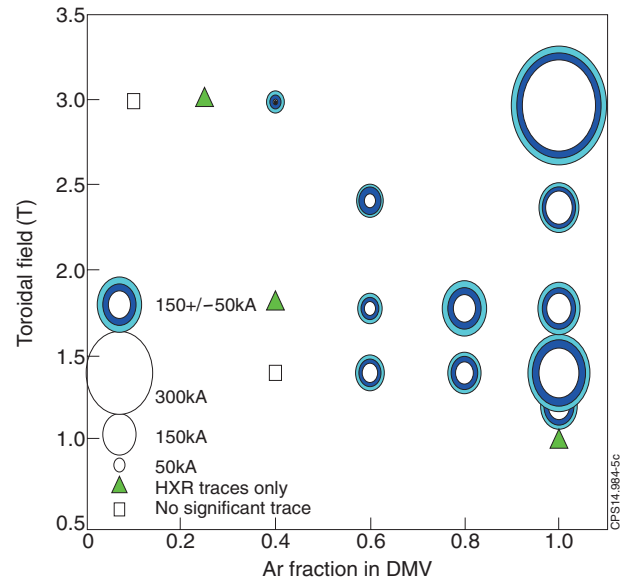


Figure 5. Operational domain for RE production in JET-ILW.

plasma properties. Predictions for ITER using WALLDYN (figure 4) [45] indicate that more than 3000 full power DT discharges are possible before reaching the fuel-inventory limit, an amount comparable with that estimated for significant divertor erosion. If confirmed, the need of frequent fuel removal will be avoided.

2.3. Disruptions and the generation of REs

Successful disruption mitigation [46–48] with massive gas injection of a mixture of argon and deuterium has been obtained and is now mandatory for JET operation above 2 MA. The radiation efficiency of massive gas injection using the disruption mitigation valve (DMV) on JET (using a mixture of 90% D₂+10% Ar) is $\geq 90\%$ at a low thermal energy fraction W_{th}/W_{mag} of < 0.3 (where W_{th} is the thermal energy and W_{mag} is the magnetic stored energy), and reduces to 70% radiation efficiency at $W_{th}/W_{mag} \sim 0.5$. In these discharges the thermal stored energy was in the range 2.5–3 MJ. This behaviour is independent of the amount of injected impurities as long as the number of radiating atoms is above some limit. The radiated energy shows a clear toroidal asymmetry caused by a pre-existing locked mode. This asymmetry changes phase when the mode is locked in a 90° rotated toroidal position. Massive gas injection into X-point and O-point of the locked-mode island results in strong changes of the toroidal radiation distribution. Future experiments with two DMVs will attempt to minimize the radiation asymmetry. It should be noted that typical values for the ratio W_{th}/W_{mag} in ITER will be $W_{th}/W_{mag} \sim 0.9$. Hence, upgrades to the DMV systems are being made in JET to increase the gas delivery capability, at different locations, and with the capability to optimize the gas mixtures. Furthermore, experiments on JET are being planned at higher W_{th}/W_{mag} values.

Although after the installation of the ILW REs [49, 50] are rarely generated during spontaneous disruptions, they can be generated, as in JET-C, using massive argon injection. Argon dominates the disruption plasma content,

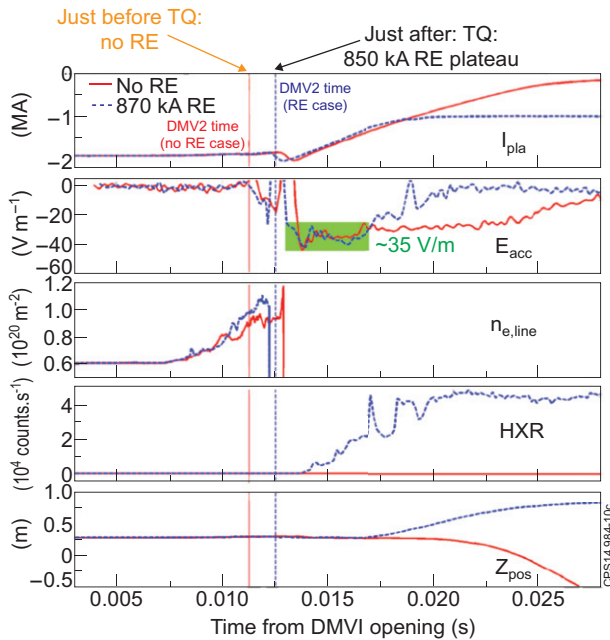


Figure 6. RE suppression by massive D_2 injection. The injection is effective only if the injected gas reaches the plasma before the thermal quench (red). A delay of about 2 ms results in the production of a 850 kA runaway beam.

as shown in figure 5 [51], thus decreasing the effect of the intrinsic impurities (carbon or beryllium) on the current quench dynamics. The conditions in which RE appear are similar between JET-C and JET-ILW: high toroidal field, high accelerating electric field and low densities (leading to lower critical electric field for RE generation) favour large RE currents. They also show a strong dependence on plasma initial shape and vertical stability.

Energies up to 20 MeV were measured for 200 to 380 kA RE beams. RE beams up to 1.2 MA at $I_p = 2$ MA have been produced by massive argon injection via DMV, leading to substantial damage of tiles due to localized and toroidally asymmetrical melting on the inner wall and upper beryllium limiters [51]. It is to be noted that, within the uncertainty of the time reference of the IR camera, the interaction between the tile and the RE beam starts before the RE current decay, possibly due to contact with the wall. After in-vessel visual inspection, the affected tile showed clear signs of melting and droplet ejection over an area of about 10 cm^2 .

Suppression of fully developed runaway beams up to 1.2 MA was attempted using massive high- Z gas injections (up to 45 bar l Kr or 24 bar l Xe). Although the fast camera showed that some gas arrived at the plasma, no useful mitigation was observed with no obvious change in hard ray emission or current decay rate. However, early massive deuterium injection was found to be efficient at totally suppressing the runaway beam provided that the gas reached the plasma before the mixing phase of plasma and incoming gas which occurs at the thermal quench (figure 6).

3. H-mode physics in an all-metal environment

The qualification of the ELMy H-mode and of the hybrid regime with the ILW has provided a number of results of direct

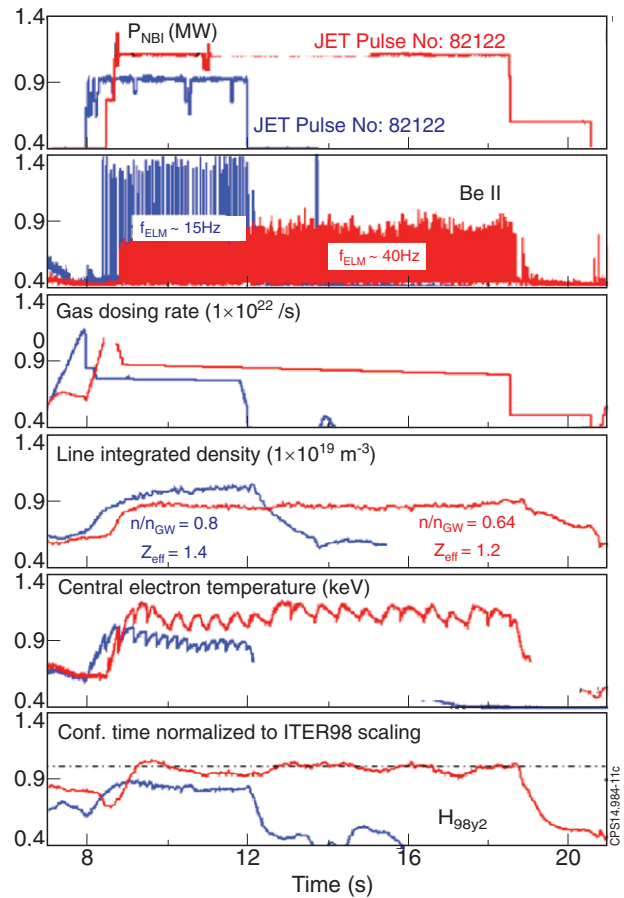


Figure 7. The optimization of the magnetic configuration led to the re-establishment of long-pulse, high-confinement H-modes (red). Shown in blue is the best discharge obtained in 2012 by controlled gas puffing to produce high-frequency ELMs and avoid W accumulation.

relevance for ITER. The baseline and hybrid scenarios have been progressed towards ITER dimensionless parameters in plasmas up to 4 MA, with Z_{eff} values as low as 1.1 and the domain of good confinement extended [52]. High performance scenarios are being successfully developed within the ILW constraints, namely the control of heat loads on the PFCs, the minimization of core tungsten concentration and disruption mitigation/avoidance.

3.1. Scenario development and optimization

H-mode and hybrid plasmas were obtained with energy confinement enhancement factors (H_{98}) in the range of 0.9–1.2 [53] when compared with IPB98(y,2) scaling law [54]. It was previously reported that stationary H-modes could be re-established with the ILW by avoiding W accumulation through the production of frequent ELM regimes by gas puffing [12]. This, however, had a detrimental effect on confinement, possibly due to the pedestal cooling by gas injection. During the last two years, stationary H-modes with confinement encompassing the ITER value ($H_{98} = 1$) have been produced by placing the divertor strike points such as to maximize pumping. In this way stationary, long-pulse (~ 9 s) H-modes have been produced at low value of Z_{eff} (figure 7). Interestingly, confinement times in line with or

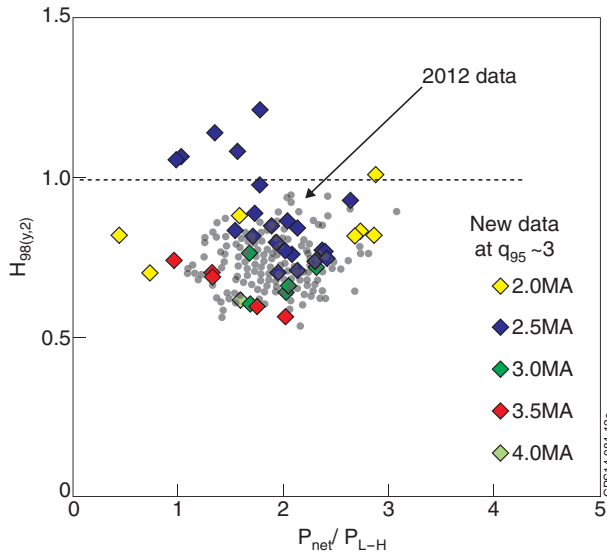


Figure 8. Achieved values of H_{98} as a function of the ratio between the power conducted through the magnetic separatrix and the L–H threshold power in the baseline scenario. The grey circles are the 2012 data. Diamonds are the results of the last two years. Optimization has been carried out so far only at 2.5 MA.

above the ITER98y2 scaling have been obtained also for values of the ratio $P_{\text{net}}/P_{\text{LH}}$ between 1 and 2, where P_{net} is the power conducted through the separatrix and P_{LH} is the LH threshold power (figure 8).

Comparisons between baseline and hybrid plasmas in the range of $3 \leq q_{95} \leq 4.3$ and $1 \leq \beta_N \leq 2.7$, for the same values of the toroidal magnetic field (B_T), plasma current (I_p), density (n_e) and heating power (P_{NBI}), have blurred the distinction between the two scenarios, which now appear as a single operating domain. Previously hybrid discharges at JET obtained $H_{98} \geq 1.1$ and $\beta_N \geq 2.5$ for $q(0)$ just above or near 1, while baseline discharges were restricted to $H_{98} < 1.1$ and $\beta_N < 2$ for fully diffused current profiles with $q(0) < 1$. Recent experiments have shown that at lower input power (or beta) hybrid discharges obtain lower H_{98} , while baseline discharges at high beta ($\beta_N \geq 2.5$) also have access to high confinement ($H_{98} \geq 1.1$). Small differences between the two scenarios remain: ion temperature profiles are more peaked and neutron rates are higher in the hybrid scenario.

Power scans were performed under well-controlled conditions in the hybrid scenario in order to elucidate the validity of the power degradation included in the IPB98(y,2) scaling. The results confirmed earlier observations that the JET-ILW H-mode confinement time can be increased with respect to the IPB98(y,2) scaling as the heating power, or beta, is increased [55] consistent with previous observations of weak beta scaling of confinement in ELMy H-modes in DIII-D and JET [56]. The new experiments show weak power degradation of confinement when low gas injection rates are used to avoid the high-frequency ELMs discussed above. In these conditions the power exponent is found to be in the range -0.2 to -0.4 , as shown in figure 9 [57], as compared with -0.69 for the IPB98(y,2) scaling. It should be noted that the JET-C high triangularity experiments were the only case, within these dedicated scans, to exhibit strong power degradation of confinement. It has been

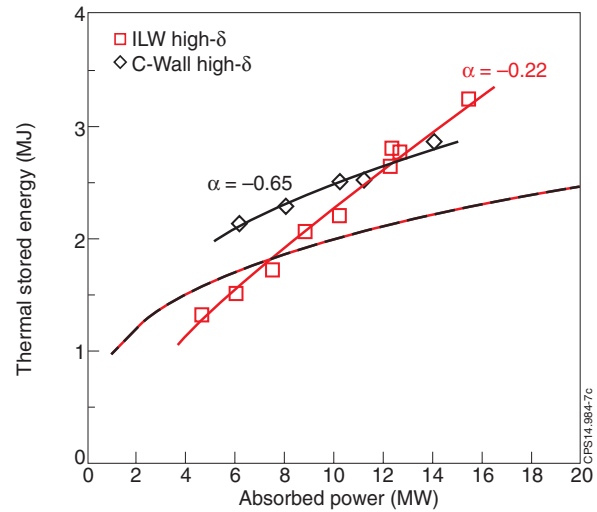


Figure 9. Plasma thermal stored energy as a function of absorbed heating power in the high triangularity configuration. The solid lines are fits to the data assuming a scaling of the form $W_{\text{th}} \sim P^{\alpha+1}$, where α is the exponent for the scaling for energy confinement time with power. The dashed line represents the dependence using the IPB98(y,2) scaling (i.e. $\alpha = -0.69$).

concluded [57] that these discharges are atypical of the confinement behaviour in JET in the controlled conditions of this experiment. This exceptional case appears to have been affected by variations in the neutral particle population in the main chamber [58], pointing out the role of neutral particles in plasma confinement [53]. This conclusion is supported by dedicated power scans in JET-ILW with higher gas injection rate, in which the observed confinement degradation with power is closer to the expectations of IPB98(y,2). The strong increase in plasma stored energy with power in the JET-ILW H-mode with low gas injection is associated with the increase in pedestal pressure and core pressure peaking and may be due to the interplay of different mechanisms: (i) the temperature peaking increase is qualitatively consistent with previously proposed mechanisms relying on plasma rotation or supra-thermal ion pressure [59, 60]; (ii) the correlation of density peaking with collisionality is consistent with previous observations and theory [61]; (iii) the increase in pedestal pressure with core plasma beta is consistent with modelling based on peeling–ballooning modes [62].

JET-ILW experiments confirmed also the importance of central electron heating for achieving high performance H-modes in devices with high-Z PFCs. ICRH has proven to be capable of mitigating core tungsten accumulation, in agreement with the expectation of neoclassical theory [63] in high power H-modes (with total auxiliary heating power $P_{\text{aux}} > 20$ MW) provided that the heating scenario is optimized and that the RF coupled power is high enough ($P_{\text{RF}} > 3$ MW), as shown in figure 10 [64]. Distributed main chamber gas injection (as opposed to the divertor gas fuelling usually adopted) achieved the best RF coupling, due to the increase of the local density in front of the ICRH antennas [65, 66]. The ICRF absorption and core electron heating were optimised by fine-tuning the resonance position and the minority hydrogen concentration. The best results were obtained with central ICRF power deposition ($r < 0.1$ m)

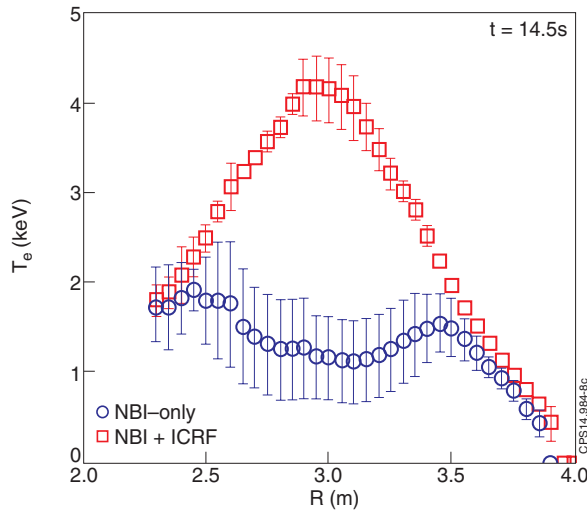


Figure 10. Comparison of the electron temperature profile at $t = 54.5$ s from the LIDAR diagnostic of two similar nitrogen-seeded discharges with NBI-only (JPN 85413) and NBI+ICRF (JPN 85412) with comparable total auxiliary power input.

and with low ($n_H/n_e \sim 5\%$) minority concentrations, both guaranteeing an efficient collisional transfer of the absorbed power to the electrons. A minimum ICRF power (4–5 MW) is necessary for achieving sufficiently peaked temperature profiles in typical H-mode plasmas at central densities $n_{e0} = (7 - 9) \times 10^{19} \text{ m}^{-3}$ for successful core impurity mitigation to take place. In most cases, a lower level (2–3 MW) is sufficient for avoiding radiative collapse.

3.2. Core-edge integrated scenario development with impurity seeding

Operational scenarios in ITER will require a significant fraction of the input/fusion power to be radiated ($f_{\text{rad}} > 0.5$) in order to generate tolerable PFC heat loads. This is even more important for DEMO, where it is expected that $f_{\text{rad}} > 90\%$ will be required. Demonstrating the combination of high radiation using extrinsic impurities with high fusion performance is thus an important part of developing integrated operating scenarios in JET and may be also needed in full performance JET discharges with a long steady-state phase. Stable discharges with radiation peaked around X-point have been obtained at JET using N_2 , Ne, Ar and N_2+Ne as seeding gasses. The maximum radiation achieved is 75% in all cases, and is independent of heating power over the range 14–28 MW. The physics reason for the limit at 75% radiation fraction is not yet understood [67]. In these conditions, tungsten concentrations are close to the detection limit and H-mode discharges up to 10 s have been produced, although at reduced confinement.

Nitrogen seeding has also been shown to increase the pedestal pressure by up to 40% in high triangularity and 15% in low triangularity plasmas, restoring the confinement to a similar level to that seen with the carbon wall. Using N-seeding, stationary condition over 7 s have been achieved on JET at 2.5 MA/2.7 T and 21 MW input power with $\beta_N \sim 1.6$, $\langle n \rangle / n_{\text{GW}} \sim 0.85$, $Z_{\text{eff}} \sim 1.6$, $f_{\text{rad}} \sim 55\%$, with low divertor target power loads and partial detachment between ELMs, as

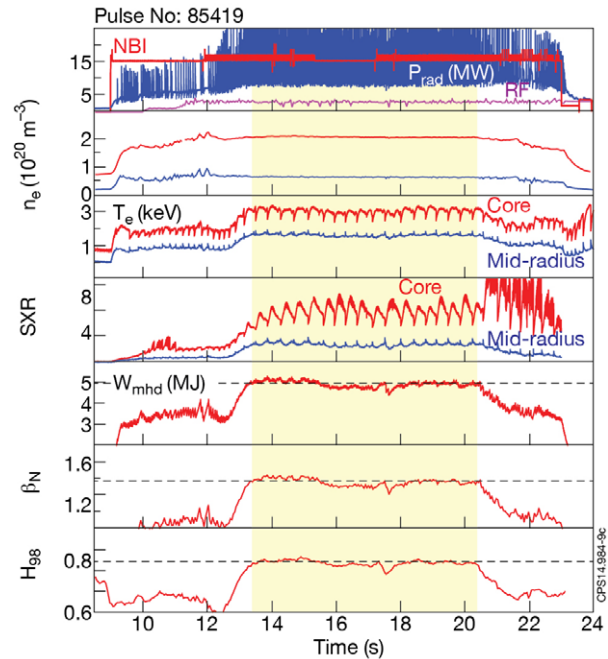


Figure 11. Time traces for long nitrogen-seeded pulse #85419 at 2.5 MA/2.7 T showing avoidance of tungsten core accumulation in a high triangularity nitrogen-seeded plasma with VT divertor configuration by adding around 3 MW of central ICRH heating power.

shown in figure 11 [68]. The performance of these plasmas is close to the desired ITER integrated plasma performance, in terms of Greenwald fraction, Z_{eff} , and divertor conditions, but the normalized energy confinement needs to be increased from $H_{98} \sim 0.85$ to $H_{98} = 1$ and the ELM energy losses need to be lowered from $\sim 4\%$ to less than 1% of the pedestal stored energy. Seeded plasma with partially detached divertor, $H_{98} \sim 1$ and $\beta_N \sim 1.8$ will be a target of the next experimental campaign in which a higher level of input power should be available ($P_{\text{aux}} > 25$ MW).

3.3. Progress towards maximum fusion performance

Hybrid scenarios at high β_N were further progressed towards lower collisionality values ($\nu^* \sim 0.04$), where better fusion performance is expected. In particular, a set of discharges with collisionalities low enough to match the upper range of the hybrid regimes in the JET carbon wall ($\nu^* \sim 0.04$) for low triangularity plasmas ($\delta \sim 0.15$) were achieved. These experiments used up to 25 MW of NBI auxiliary power with $I_p = 2$ MA and $q_{95} = 3.8$ using a configuration with the strike point on the outer horizontal tile for maximizing pumping, producing plasmas with H_{98} up to 1.4 and β_N up to 3.4. Values of β_N up to 2.3 were achieved at $B_T = 2.9$ T and $I_p = 2.5$ MA leading to a new neutron rate record of $2.3 \times 10^{16} \text{ s}^{-1}$ for the ILW. The normalised confinement $H_{98} = 1.15$ is consistent with the findings of the beta scan experiment and on the basis of the observed dependence of H_{98} on β_N , is expected to achieve higher values if the target $\beta_N = 2.5$ could be reached. The β_N value so far achieved is only limited by the available heating power. The duration (up to 3 s) of the high performance phase is limited by impurity

accumulation and MHD occurring during the accumulation process, requiring further optimization of divertor plasma conditions while maximizing core fusion performance.

The extrapolation of these discharges to a 50/50 DT fuel mix predicts that about 15 MW of fusion power could be produced. This target could be achieved in stationary conditions for about 5 s, rather than transiently as in the 1997 JET DT experiment, corresponding to a total produced fusion energy of 75 MJ, at 3.5 MA/3.45 T with 39 MW of auxiliary power. These projections do not account for the contribution of the alpha particle heating and the beneficial isotope dependence of confinement, giving some margin in the achievable performance. In addition, recent analyses [69] of the 1997 record DT discharges show that core condition exceeding breakeven ($Q = 1$ with Q evaluated from the power balance inside mid-radius) could have been already achieved in JET with core Q values of about 1.5. Similarly, the extrapolated JET-ILW discharges are expected to achieve a higher core Q value than that inferred by the global analysis. However, the scenario tailoring necessary to achieve divertor-compatible conditions represents a major area of required improvement for the next set of JET campaigns.

3.4. L–H transition studies

JET-ILW experiments show a minimum in the L–H threshold power as function of density, as seen on other machines and on JET-C with the MkII-GB divertor, and a reduction of the threshold by 30% in the high-density branch. Both observations are potentially favourable for H-mode access on ITER [70, 71]. Nitrogen injection increases the threshold to JET-C values, suggesting that the difference between JET-C and JET-ILW can be accounted for by the impurity composition. Experiments indicate that the density at which the minimum occurs depends on both impurity content and divertor configuration and was not accessible in JET-C with the current divertor. Changes to the magnetic configuration in the divertor lead to changes in P_{L-H} up to a factor 2. Fits of the edge density and temperature profiles show agreement with the assumption of a critical, diamagnetic driven, E_r well (as proxy for the shearing rate) for each of the divertor configurations, but cannot explain the difference in P_{L-H} between them. A transition that creates a strong inner–outer asymmetry in the divertor plasma conditions is observed with the same power scaling as the high-density branch of the L–H threshold and precedes the L–H transition at high density. This transition depends on the divertor configuration and hints at changes in the scrape-off layer directly affecting the transition.

3.5. Pedestal studies with the ILW

Pedestal studies have been carried out at JET with the main objective of addressing the physics responsible for the decrease in H-mode pedestal confinement observed in the initial phase of JET-ILW operation [61]. The effects of neutral recycling, plasma beta, plasma triangularity and nitrogen seeding on pedestal confinement and stability have been investigated, in the framework of the peeling–ballooning paradigm and making use of the EPED model [72]. It was found that low neutral recycling, achieved either by low deuterium gas injection rates or by divertor configurations with optimum

pumping, and high beta are necessary conditions for good pedestal (and core) confinement. Under such conditions the pedestals are consistent with the peeling–ballooning paradigm. In contrast, under conditions characterized by high neutral recycling, additional physics is required in the pedestal model to explain the onset of the ELM instability. The physics mechanism leading to the increase in electron temperature in the pedestal with nitrogen seeding in high triangularity JET-ILW H-modes is not yet understood. The changes in edge confinement following the change in wall composition from CFC to beryllium/tungsten suggest the importance of the role of neutral recycling, low- Z impurities and scrape-off-layer physics in pedestal stability, elements that are not currently included in pedestal models. These aspects need to be addressed before a full predictive capability of the pedestal height can be achieved.

4. Conclusions and perspectives

Four years of JET operation with the ILW have provided confidence that the use of this combination of materials will not pose major problems for the successful operation of ITER. The low retention properties have been confirmed by the post-mortem analysis and the melt layer experiment has shown that the consequence of melting can be tolerated for JET operation and that the JET results agree with the simulation codes that predict tolerable consequences also for ITER operation.

Significant progress has been made in expanding the domain in which good energy confinement is achieved by investigating magnetic configurations that allow a better pumping. Impurity seeding has been used to achieve steady regimes at high density and low Z_{eff} with detached divertor.

Overall JET demonstrated successful plasma operation in the beryllium/tungsten material combination, confirmed its advantageous behaviour with respect to material migration and fuel retention and provided a strong scientific basis for the ITER material selection.

The ILW exploitation will continue in 2015 with the main aim of progressively increasing the plasma performance. In parallel, the preparation of a DT experiment is ongoing. The experiment is presently foreseen to take place in 2017 and according to the ‘Reference Scenario’ for the JET exploitation [1] will be followed by the machine being put in a safe state for decommissioning.

Following the completion of the feasibility studies for new JET enhancements, the design and R&D activity for a set of internal resonant magnetic perturbation coils has been completed in collaboration with the Institute for Plasma Research in Gandhinagar. Its implementation on JET will require a decision on the ‘Alternative Scenario’ for the JET exploitation, consisting of the prolongation of JET up to 2022, tritium operation limited to a full-T experiment in 2017 and the DT experiment postponed to 2021.

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