# BUILDING BLOCKS FOR CURRENT-MODE IMPLEMENTATION OF VLSI FUZZY MICROCONTROLLERS

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# Building Blocks for Current-Mode Implementation of VLSI Fuzzy Microcontrollers

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Abstract-- A fuzzy microcontroller is presented implementing a simplified inference mechanism. Fuzzification, rule composition and defuzzification are carried out by means of (basically) analog current-mode CMOS circuits operating in strong inversion. Also a voltage interface is provided with the external world. Combining analog and digital techniques allow a programming capability.

#### I. INTRODUCTION

The application of inference techniques based on fuzzy logic to real-time control problems requires specialized hardware realizations tailored to the fuzzy paradigm. Most fuzzy microcontrollers presently used in industrial applications correspond to digital implementations. A main reason for this is the many advantages derived from sound design techniques, flexible programmability, and easy connection to digital processing environments. However, resorting to analog techniques might give better results since fuzzy logic is intrinsically more alike the multivalued and continuous world than to the digital one. This may allow to design circuits with a better ratio "silicon area/inference speed", eliminating as well the need for A/D and D/A interfacing.

Adapting fuzzy control concepts to fit microelectronics constraints, both in terms of architecture and circuitry, has been a major issue in this field. There have been reported fuzzy controllers implemented by massively parallel structures for both evaluating the control rule contributions and handling the fuzzy information employed by the consequents [1]. The huge size of parallel implementations can be substantially reduced when a series architecture is used, as the one proposed by the authors in [2], since there is possible to establish a trade-off between silicon area and operation speed.

A different issue is related to simplifying the algorithms employed for the inference process. When we evaluate the controller output, if we do not disregard the contribution of the pertenence functions overlapping zones, and if, in addition, these functions are symmetrical, a center of gravity calculation is equivalent to compute the center of the maximum values for the different functions. From a mathematical viewpoint, this is equivalent to substitute the pertenence

functions representing the rule consequent linguistic label by a singleton membership function located in the point where the original function reaches a maximum. This simplified inference procedure is much more adequate for controller hardware implementations [3].

Concerning circuit design methodologies, current-mode techniques are specially suited for a direct implementation of the arithmetic operations (addition and subtraction) needed by the basic fuzzy operators. Working in currentmode, dynamic range problems can be handled very flexibly, in a manner which does not depend upon bias voltage values; also, a high operation speed can be attained. Another important feature that worth considering is the controller interfacing capability with existing devices. In this sense, although some sensors (actuators) provide (accept) currents, most applications require voltages as the control variables. Another essential issue to guarantee a broad application spectrum for a controller is its programming capability, in such a way that it can be adapted to solve many problems without demanding complex adjusting procedures.

The aim of this communication is to describe a hardware realization for a fuzzy controller implementing a simplified inference mechanism. Although the processes of fuzzification, rule composition and defuzzification are performed by current-mode circuits, this system provides voltage-to-current interfacing at its inputs and current-to-voltage at its outputs. Programming functionalities are added by combining analog and digital techniques, giving rise to a versatile microcontroller.

### II. ARCHITECTURE DESCRIPTION

The fuzzy microcontroller we are about to describe is based on rules:

If  $x_1$  is  $A_i$  and/or  $x_2$  is  $B_i$  and/or ... Then z is  $C_i$  where  $x_i$  are input variables, z is the output variable,  $A_i$ ,  $B_i$ , ... are linguistic labels represented by pertenence functions, and  $C_i$  are discrete values associated to the consequents. The contribution from a given control rule  $(z_i)$  is calculated by multiplying the consequent  $C_i$  by the rule activation degree,  $h_i$ . The latter, in turn, is a function of the inputs

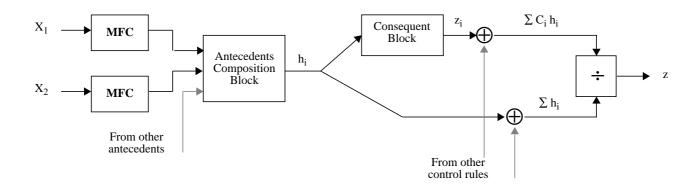


Fig.1.- Controller Architecture.

pertenence degree and of the connectives among the different antecedents. Hence, the controller output can be calculated by the expression:

$$z = \sum C_i h_i / \sum h_i \tag{1}$$

Figure 1 represents a block diagram for an architecture implementing the described inference algorithm. Circuit structures for each block in Figure 1 will be detailed in the next Sections.

#### III. MEMBERSHIP FUNCTION CIRCUITS

A simple manner to implement a Membership Function Circuit is shown in Figure 2. Inputs are voltages and outputs are currents. The input part is a voltage-to-current converter designed by means of a circuit described in [4]. We use PMOS transistors for a positive slope of the voltage-current relationship, avoiding the substrate effect of transistor M2.

Figure 2-a depicts a circuit schematic for the MFC for a triangle-shaped function. Figure 2-b plots the simulated transfer characteristic for the circuit in Figure 2-a.

In this example we have assumed one V-I converter element within each MFC. Since the converter circuitry is so simple, an alternative is to use as many converters as rule antecedents exist, and then replicate the resulting current for the different rules. The former can be carried out at the pin interfacing circuitry, thus suggesting that pads for the

controller inputs can be designed to perform the voltage to current conversion.

#### IV. RULE EVALUATION CIRCUITRY

AND and OR fuzzy operators connecting the control rules are associated to MIN and MAX operations, respectively. Figure 3-a shows a rule evaluation circuit. The left part implements a MIN/MAX operator; the right part is a multiple-output current mirror followed by a set of switches, used to add digital programmability to the consequents, C<sub>i</sub>. Figure 3-b depicts experimental results for the MIN/MAX operator.

Taking into account that the number of antecedents is usually not too high, and that the simplified inference method requires neither MIN operators to relate antecedents and consequents nor MAX operators to relate all the rules among them, restricting to 2-input operators is not very limiting. Of course, alternatives can be found by adapting voltage-driven multiple-input MAX operators. A candidate is the circuit in [5] using an OTA with multiple outputs in a feedback loop (Figure 4-a). However, when this is the case, stability problems can arise, restricting the circuit applicability. Another alternative is offered by the circuit in [6] and [7], which can be simplified as shown in Figure 4-b where only one diode-connected transistor is used to discharge the common gate node with a reduced power consumption.

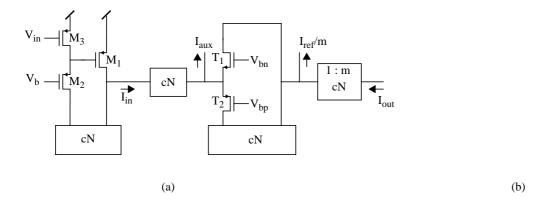
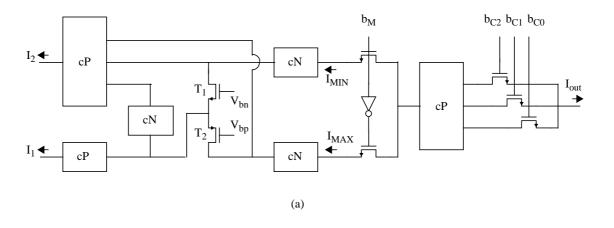


Fig.2.- a) Membership Function Circuit. b) Transfer Characteristic for the MFC.



(b)

Fig.3.- a) Rule Evaluation Circuit. b) Experimental Results for MAX and MIN operators.

#### V. DEFUZZIFIER BLOCK

Since defuzzifiers are based on division or normalization, it is customary to use circuits based on a global feedback loop where a high-gain element is embedded. However, these circuits are complex and usually prone to instability problems.

On the contrary, the defuzzifier we propose herein does require only transistors operating in strong inversion; the circuit output is a voltage and only local feedback loops are used. It is based on a variable transresistance element, and its circuit schematic is given in Figure 5-a. It is formed by three parts (from right to left): a voltage-controlled resistor [8], a current-controlled biasing circuit, and a current squar-

ing [9]. Disregarding the substrate effect ( $V_{T1}=V_{T2}=V_{T}$ ),  $V_{out}$  can be expressed by:

$$V_{out} = I_B / \beta_R (V_B - V_{SS} - 2V_T)$$
 (2)

The voltage supplied by the biasing circuit is:

$$V_{B} = V_{SS} + 2V_{T} + 2\sqrt{\frac{2I}{\beta}}$$
 (3)

And the squaring circuit output is:

$$I = I_A^2 / 8 I_{SS}$$
 (4)

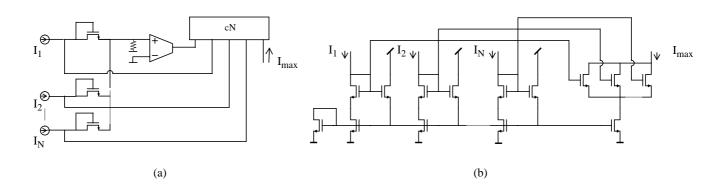


Fig.4.- Current-Mode Multiple-Inputs MAX Operators. a) With a Feedback Loop. b) Based on the Circuit proposed in [6] and [7].

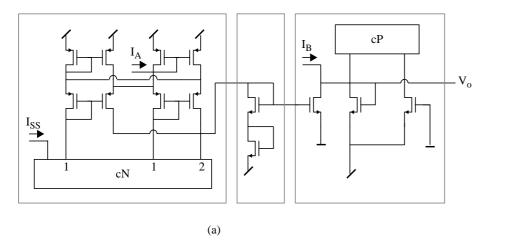


Fig.5.- a) Defuzzifier Circuit. b). Input-Output Characteristic for the Circuit in Figure 5-a. Fig.

After substituting (3) and (4) into (2):

$$V_{out} = \frac{\sqrt{\beta I_{SS}}}{\beta_R} \times \frac{I_B}{I_A}$$
 (5)

within an operating range  $0 \le V_{out} \le V_B - V_T$ . Since in our case  $I_B$  corresponds to  $\sum C_i$   $h_i$  and  $I_A$  corresponds to  $\sum h_i$ , the operating range can be expressed as:

$$\frac{\beta}{\beta_R} I_{SS} C_{max} + (\left| V_{SS} \right| - V_T) \sqrt{\beta I_{SS}} \le I_A \le 4I_{SS}$$
 (6)

This limitation is not very restrictive, specially because we are working with currents and thus we can scale them easily. Figure 5-b shows a simulation result obtained varying  $I_B$  with  $I_A$  as the parameter, taking values from -15  $\mu A$  to - 40  $\mu A$  in steps of 5  $\mu A$ . From the Figure it should be apparent the circuit linearity for this case.

## VI. CONCLUDING REMARKS

A set of circuits have been presented to implement a fuzzy controller handling voltage inputs and outputs but processing currents. This is a way to take advantage of the inherent high speed of current-mode circuitry still retaining voltages as the external controller variables. The different components have been sent to integration, but not all of them have been available yet; for that reason experimental results are given only for some of them.

The issue of dynamic range worth considering, since the input range is going from 3 to 4 volts, whilst the output range is from 0 to 1 volts. This must not be a problem because this controller is not intended for driving another controller, in addition, input buffering and level shifting can be added specifically tailored to every application where this controller is going to be used.

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